# WEST HILLS COMMUNITY COLLEGE DISTRICT <br> WEST HILLS LEMOORE CAMPUS INSTRUCTIONAL CENTER PROJECT 



## WEST HILLS COLLEGE <br> 

Comments must be received by: January 22, 2021 (30 days after notice)

# INITIAL STUDY/MITIGATED NEGATIVE DECLARATION 

## WEST HILLS LEMOORE CAMPUS INSTRUCTIONAL CENTER PROJECT

Prepared for:<br>West Hills Community College District<br>275 Phelps Avenue<br>Coalinga, CA 93210

Contact Person: Richard Storti, Deputy Chancellor
Phone: (559) 934-2160


## WEST HILLS COLLEGE L E M O O R E

Consultant:


Bakersfield, CA 93309
Contact: Jaymie Brauer
Phone: (661) 616-2600

December 2020
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## Notice of Public Hearing and Intent to Adopt a Mitigated Negative Declaration

This is to advise that the West Hills Community College District has prepared a Mitigated Negative Declaration for the project identified below that is scheduled to be considered at the Board of Trustees regular meeting on Tuesday, February 16, 2021

PLEASE BE ADVISED that the Board of Trustees will consider adopting the Mitigated Negative Declaration at the meeting to be held on February 16, 2021. Presentations will be made at approximately 3:00 p.m. Action on items on the board agenda will occur after the presentations.

In response to the COVID-19 pandemic, the Governor of California has issued Executive Order N-25-20, Executive Order N-29-20, and Executive Order N-35-20 modifying the Brown Act in order to facilitate essential public meetings being held through remote methods, such as telephonically or electronically Consistent with the foregoing, this Board meeting is being held as a virtual meeting. The Board meeting can be viewed live on YouTube. Please go to the District's website for more information https://www.westhillscollege.com/

## Project Name

West Hills College Lemoore Campus Instructional Center Project

## Project Location

The project site is located on the West Hills Community College- Lemoore campus on the northwest corner of Pederson Avenue and College Avenue in the City of Lemoore, Kings County, CA. The project site is an approximately 27.1 acre portion of Assessor's Parcel Numbers 023-510-018, within Section 8, Township 19S, Range 20E, MMB\&M.

## Project Description

The District proposes to construct a 42,429-square-foot, two-story Instructional Center (IC) on an undeveloped but disturbed portion of the existing campus. The college has a current student enrollment of 4,600 students and the proposed expansion is anticipated to increase the overall student population by approximately 5 percent, or approximately 232 students. The IC will be used to expand education opportunities in the areas of allied health services, computer science and graphic arts.

Construction will include site clearing, rough and finished grading, trenching, backfill for underground facilities, and concrete for circulation surfaces. The two-story building will match existing campus standards and include steel framing, concrete floors, built up roofing over steel decking, and brick exterior finishes, metal roofing accents, and an elevator which will support future expansion. The project consists of lecture, laboratory, office and other rooms used for educational purposes.

Construction is expected to begin in January 2023 and end in April 2024. Construction equipment will include a crane, bulldozer, grader, bob cat, trencher, cement trucks, water trucks, trash trucks, equipment delivery trucks, and company work vehicles.

The document and documents referenced in the Initial Study/Mitigated Negative Declaration are available for review at District administrative office located at 275 Phelps Ave, Coalinga, CA 93210, or on the District website:
https://www.westhillscollege.com/district/administration/
As mandated by the California Environmental Quality Act (CEQA), the public review period for this document was 30 days (CEQA Section 15073 [b]). The public review period began on December 24, 2020 and ended on January 22, 2021. For further information, please contact Jaymie Brauer at 661-616-2600 or jaymie.brauer@qkinc.com.

## Notice of Completion \& Environmental Document Transmittal



| Local Action Type: |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\square$ General Plan Update |  | Specific Plan |  | Rezone |  | Annexation |
| $\square$ General Plan Amendment |  | Master Plan |  | Prezone |  | Redevelopment |
| $\square$ General Plan Element |  | Planned Unit Development |  | Use Permit |  | Coastal Permit |
| $\square$ Community Plan |  | Site Plan |  | Land Division (Subdivision, etc.) |  | Other: |

## Development Type:



## Project Issues Discussed in Document:

| $\square$ Aesthetic/Visual | $\square$ Fiscal | $\square$ Recreation/Parks | $\square$ Vegetation |
| :--- | :--- | :--- | :--- |
| $\square$ Agricultural Land | $\square$ Flood Plain/Flooding | $\square$ Schools/Universities | $\square$ Water Quality |
| $\square$ Air Quality | $\square$ Forest Land/Fire Hazard | $\square$ Septic Systems | $\square$ Water Supply/Groundwater |
| $\square$ Archeological/Historical | $\square$ Geologic/Seismic | $\square$ Sewer Capacity | $\square$ Wetland/Riparian |
| $\square$ Biological Resources | $\square$ Minerals | $\square$ Soil Erosion/Compaction/Grading | $\square$ Growth Inducement |
| $\square$ Coastal Zone | $\square$ Noise | $\square$ Solid Waste | $\square$ Land Use |
| $\square$ Drainage/Absorption | $\square$ Population/Housing Balance | $\square$ Toxic/Hazardous | $\square$ Cumulative Effects |
| $\square$ Economic/Jobs | $\square$ Public Services/Facilities | $\square$ Traffic/Circulation | $\square$ Other: |

## Present Land Use/Zoning/General Plan Designation:

## Community Facilities

## Project Description: (please use a separate page if necessary)

The District is proposing to construct a 42,000 square foot, two-story Instructional Center (IC) on an undeveloped but disturbed portion of the existing campus. The college has a current student enrollment of 4,600 students and the proposed expansion is anticipated to increase the overall student population by approximately 5 percent, approximately 232 students. The IC will be used to expand education opportunities in the areas of allied health services, computer science and graphic arts

[^0]
## Reviewing Agencies Checklist

Lead Agencies may recommend State Clearinghouse distribution by marking agencies below with and "X".
If you have already sent your document to the agency please denote that with an "S".

| x | Air Resources Board <br> Boating \& Waterways, Department of California Emergency Management Agency California Highway Patrol Caltrans District \# 6 <br> Caltrans Division of Aeronautics Caltrans Planning Central Valley Flood Protection Board Coachella Valley Mtns. Conservancy Coastal Commission Colorado River Board Conservation, Department of Corrections, Department of Delta Protection Commission Education, Department of Energy Commission <br> Fish \& Game Region \# 4 <br> Food \& Agriculture, Department of Forestry and Fire Protection, Department of General Services, Department of Health Services, Department of Housing \& Community Development Native American Heritage Commission |  | Office of Historic Preservation |
| :---: | :---: | :---: | :---: |
|  |  |  | Office of Public School Construction |
|  |  |  | Parks \& Recreation, Department of |
|  |  |  | Pesticide Regulation, Department of |
| x |  |  | Public Utilities Commission |
|  |  | x | Regional WQCB \# Central |
|  |  |  | Resources Agency |
|  |  |  | Resources Recycling and Recovery, Department of |
|  |  |  | S.F. Bay Conservation \& Development Comm. |
|  |  |  | San Gabriel \& Lower L.A. Rivers \& Mtns. Conservancy |
|  |  |  | San Joaquin River Conservancy |
|  |  |  | Santa Monica Mtns. Conservancy |
|  |  |  | State Lands Commission |
|  |  |  | SWRCB: Clean Water Grants |
|  |  | x | SWRCB: Water Quality |
|  |  |  | SWRCB: Water Rights |
| x |  |  | Tahoe Regional Planning Agency |
|  |  | x | Toxic Substances Control, Department of |
|  |  | x | Water Resources, Department of |
|  |  |  |  |
|  |  |  | Other: Division of the State Architecht |
|  |  |  | Other: |
| $x$ |  |  |  |

## Local Public Review Period (to be filled in by lead agency)

Starting Date December 24, 2020
Ending Date $\qquad$

## Lead Agency (Complete if applicable):

## Address:

$\qquad$
City/State/Zip:
Contact: $\qquad$
Applicant: $\qquad$
Address:
City/State/Zip:
Phone: $\qquad$
Phone: $\qquad$ /S/

Date: 12/24/2020
Signature of Lead Agency Representative: $\qquad$

Authority cited: Section 21083, Public Resources Code. Reference: Section 21161, Public Resources Code.

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Santa Rosa Rancheria Tachi
Yokut Tribe
Chairperson
P.O. Box 8

Lemoore, CA 93245

U S. Fish and Wildlife Service
2800 Cottage Way
Rm W-2605
Sacramento, CA 95825

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Chairperson
P.O. Box 410

Friant, CA 93626

Table Mountain Rancheria
Cultural Resources Director
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## Table of Contents

Mitigated Negative Declaration ..... 1
SECTION 1 - Introduction ..... 1-1
1.1-Overview ..... 1-1
1.2-CEQA Requirements ..... 1-1
1.3 - Impact Terminology ..... 1-1
1.4 - Document Organization and Contents ..... 1-2
1.5 - Incorporated by Reference. ..... 1-2
SECTION 2 - Project Description ..... 2-1
2.1 - Introduction ..... 2-1
2.2 - Project Location ..... 2-1
2.3 - Project Environment ..... 2-1
2.4 - Proposed Project ..... 2-1
SECTION 3 - Evaluation of Environmental Impacts ..... 3-1
3.1 - Environmental Checklist and Discussion ..... 3-1
3.2 - Environmental Factors Potentially Affected: ..... 3-3
3.3 - Determination ..... 3-3
3.4 - Evaluation of Environmental Impacts ..... 3-5
3.4.1 - Aesthetics ..... 3-7
3.4.2 - Agriculture and Forestry Resources ..... 3-10
3.4.3 - Air Quality ..... 3-15
3.4.4 - Biological Resources ..... 3-23
3.4.5 - Cultural Resources ..... 3-39
3.4.6 - Energy ..... 3-42
3.4.7 - Geology and Soils ..... 3-44
3.4.8 - Greenhouse Gas Emissions ..... 3-52
3.4.9 - Hazards and Hazardous Materials ..... 3-55
3.4.10 - Hydrology and Water Quality ..... 3-60
3.4.11 - Land Use and Planning ..... 3-68
3.4.12 - Mineral Resources ..... 3-70
3.4.13 - Noise ..... 3-72
3.4.14 - Population and Housing. ..... 3-76
3.4.15 - Public Services ..... 3-78
3.4.16 - Recreation ..... 3-82
3.4.17 - Transportation and Traffic ..... 3-84
3.4.18 - Tribal Cultural Resources ..... 3-90
3.4.19 - Utilities and Service Systems ..... 3-93
3.4.20 - Wildfire ..... 3-97
3.4.21 - Mandatory Findings of Significance ..... 3-100
West Hills Lemoore Campus Construction Project ..... December 2020
SECTION 4 - References ..... 4-1
SECTION 5 - List of Preparers ..... 5-1
5.1 - Lead Agency ..... 5-1
5.2 - Technical Assistance ..... 5-1
SECTION 6 - Mitigation Monitoring and Reporting Program ..... 6-1
List of Figures
Figure 2-1 Regional Location ..... 2-3
Figure 2-2 Project Site ..... 2-4
Figure 2-3 Surrounding Land Uses ..... 2-5
Figure 3.4.2-1 Farmland Mapping and Monitoring Program (FMMP) ..... 3-13
Figure 3.4.2-2 Williamson Act Contracts ..... 3-14
Figure 3.4.4-1 National Wetland Inventory and Hydrologic Information ..... 3-38
Figure 3.4.10-1 100-Year Floodplain ..... 3-67
List of Tables
Table 3.4.3-1 GAMAQI Thresholds of Significance for Criteria Pollutants ..... 3-16
Table 3.4.3-2 Small Project Analysis Level - Units for Educational ..... 3-17
Table 3.4.3-3 Small Project Analysis Level - Daily Trips for Educational Institutions ..... 3-17
Table 3.4.3-4 Construction Emissions ..... 3-19
Table 3.4.3-5 Total Project Operational Emissions ..... 3-19
Table 3.4.4-1 List of Plant and Wildlife Species Observed on the Project Site ..... 3-26
Table 3.4.8-1 Estimated Annual Greenhouse Gas Emissions ..... 3-53
Table 3.4.13-1 Vibration Generated by Construction Equipment ..... 3-73
Table 3.4.15-1 Fire Service Existing and Future Demand ..... 3-79
Table 3.4.15-2 Police Service Existing and Future Demand ..... 3-80
Table 3.4.17-1 Project Estimated Trips ..... 3-85
Table 3.4.17-2 Traffic Conditions Analysis ..... 3-86
Table 3.4.17-3 Traffic Conditions Analysis ..... 3-87
Table 3.4.20-1 Existing Wildfire Hazards ..... 3-98
List of Appendices
Appendix A: Small Project Analysis Level Assessment
Appendix B: Cultural Memorandum
Appendix C: Geotechnical Report
Appendix D: Traffic Study

## Mitigated Negative Declaration

As Lead Agency under the California Environmental Quality Act (CEQA), the West Hills Community College District reviewed the project described below to determine whether it could have a significant effect on the environment because of its development. In accordance with CEQA Guidelines Section 15382, "[s]ignificant effect on the environment" means a substantial, or potentially substantial, adverse change in any of the physical conditions within the area affected by the project, including land, air, water, minerals, flora, fauna, ambient noise, and objects of historic or aesthetic significance.

## Project Name

West Hills College Lemoore Campus Instructional Center Project

## Project Location

The project site is located on the West Hills Community College- Lemoore campus on the northwest corner of Pederson Avenue and College Avenue in the City of Lemoore, Kings County, CA. The project site is an approximately 27.1 acre portion of Assessor's Parcel Numbers 023-510-018, within Section 8, Township 19S, Range 20E, MMB\&M.

## Project Description

The District is proposing to construct a 42,429-square-foot, two-story Instructional Center (IC) on an undeveloped but disturbed portion of the existing campus. The college has a current student enrollment of 4,600 students and the proposed expansion is anticipated to increase the overall student population by approximately five percent or approximately 232 students. The IC will be used to expand education opportunities in the areas of allied health services, computer science and graphic arts.

Construction will include site clearing, rough and finished grading, trenching, backfill for underground facilities, and concrete for circulation surfaces. The two-story building will match existing campus standards and include steel framing, concrete floors, built up roofing over steel decking, and brick exterior finishes, metal roofing accents, and an elevator which will support future expansion. The project consists of lecture, laboratory, office and other rooms used for educational purposes.

The project will match the existing construction and space standards set by the District. Construction is expected to begin in January 2023 and end in April 2024. Construction equipment will include a crane, bulldozer, grader, bob cat, trencher, cement trucks, water trucks, trash trucks, equipment delivery trucks, and company work vehicles.

## Mailing Address and Phone Number of Contact Person

Richard Storti, Deputy Chancellor

West Hills Community College District

275 Phelps Avenue
Coalinga, CA 93210 (559) 934-2160
richardstorti@whccd.edu

## Findings

As Lead Agency, the District finds that the project will not have a significant effect on the environment. The Initial Study (IS) (see Section 3-Environmental Checklist) identified one or more potentially significant effects on the environment, but revisions to the project have been made before the release of this Mitigated Negative Declaration (MND) or mitigation measures would be implemented that reduce all potentially significant impacts to less-thansignificant levels. The District further finds that there is no substantial evidence that this project would have a significant effect on the environment.

## Mitigation Measures Included in the Project to Avoid Potentially Significant Effects

## Mitigation Measure(s)

MM BIO-1: Prior to ground disturbing activities, a qualified wildlife biologist shall conduct a biological clearance survey between 14 and 30 days prior to the onset of construction.

The clearance survey shall include walking transects to identify presence of San Joaquin kit fox, Swainson's hawk, and burrowing owl and any other special-status species and their sign. The pre-construction survey shall be walked by no greater than 30 -foot transects for 100 percent coverage of the project and a 250 -foot buffer, where feasible. If no evidence of special-status species is detected, no further action is required but measures BIO-4 through BIO-6 and BIO-8 shall be implemented.

MM BIO-2: The following avoidance and minimization measures shall be implemented during all phases of the project to reduce the potential for impact from the project. They are modified from the U.S. Fish and Wildlife Service Standardized Recommendations for Protection of the Endangered SJKF Prior to or During Ground Disturbance (USFWS 2011, Appendix F).
a. All food-related trash items such as wrappers, cans, bottles, and food scraps shall be disposed of in securely closed containers. All food-related trash items such as wrappers, cans, bottles, and food scraps shall be disposed of in securely closed containers and removed at least once a week from the construction or project site.
b. Construction-related vehicle traffic shall be restricted to established roads and predetermined ingress and egress corridors, staging, and parking areas. Vehicle speeds shall not exceed 20 miles per hour (mph) within the project site.
c. To prevent inadvertent entrapment of kit fox or other animals during construction, the contractor shall cover all excavated, steep-walled holes or trenches more than two feet deep at the close of each workday with plywood or similar materials. If holes or trenches cannot be covered, one or more escape ramps constructed of earthen fill
or wooden planks shall be installed in the trench. Before such holes or trenches are filled, the contractor shall thoroughly inspect them for entrapped animals. All construction-related pipes, culverts, or similar structures with a diameter of four inches or greater that are stored on the project site shall be thoroughly inspected for wildlife before the pipe is subsequently buried, capped, or otherwise used or moved in anyway. If at any time an entrapped or injured kit fox is discovered, work in the immediate area shall be temporarily halted and USFWS and CDFW shall be consulted.
d. Kit foxes are attracted to den-like structures such as pipes and may enter stored pipes and become trapped or injured. All construction pipes, culverts, or similar structures with a diameter of four inches or greater that are stored at a construction site for one or more overnight periods shall be thoroughly inspected for kit foxes before the pipe is subsequently buried, capped, or otherwise used or moved in any way. If a kit fox is discovered inside a pipe, that section of pipe shall not be moved until the USFWS and CDFW have been consulted. If necessary, and under the direct supervision of the biologist, the pipe may be moved only once to remove it from the path of construction activity, until the fox has escaped.
e. No pets, such as dogs or cats, shall be permitted on the project sites to prevent harassment, mortality of kit foxes, or destruction of dens.
f. Use of anti-coagulant rodenticides and herbicides in project sites shall be restricted. This is necessary to prevent primary or secondary poisoning of kit foxes and the depletion of prey populations on which they depend. All uses of such compounds shall observe label and other restrictions mandated by the U.S. Environmental Protection Agency, California Department of Food and Agriculture, and other State and Federal legislation, as well as additional project-related restrictions deemed necessary by the USFWS and CDFW. If rodent control must be conducted, zinc phosphide shall be used because of the proven lower risk to kit foxes.
g. A representative shall be appointed by the project proponent who will be the contact source for any employee or contractor who might inadvertently kill or injure a kit fox or who finds a dead, injured or entrapped kit fox. The representative shall be identified during the employee education program and their name and telephone number shall be provided to the USFWS.
h. The Sacramento Fish and Wildlife Office of USFWS and CDFW shall be notified in writing within three working days of the accidental death or injury to a SJKF during project-related activities. Notification must include the date, time, and location of the incident or of the finding of a dead or injured animal and any other pertinent information. The USFWS contact is the Chief of the Division of Endangered Species, at the addresses and telephone numbers below. The CDFW contact can be reached at (559) 243-4014 and R4CESA@wildlifeca.gov.
i. All sightings of the SJKF shall be reported to the California Natural Diversity Database (CNDDB). A copy of the reporting form and a topographic map clearly marked with the location of where the kit fox was observed shall also be provided to the Service at the address below.
j. Any project-related information required by the USFWS or questions concerning the above conditions, or their implementation may be directed in writing to the U.S. Fish and Wildlife Service at: Endangered Species Division, 2800 Cottage Way, Suite W

2605, Sacramento, California 95825-1846, phone: (916) 414-6620 or (916) 4146600.
k. New sightings of SJKF should be reported to the CNDDB.

MM BIO-3: Within 14 days prior to the start of project ground-disturbing activities, a preactivity survey with a 500 -foot buffer shall be conducted by a qualified biologist knowledgeable in the identification of these species and approved by the CDFW. If dens/burrows that could support any of these species are discovered during the pre-activity survey conducted under MM BIO-1, the avoidance buffers outlined below should be established. No work would occur within these buffers unless the biologist approves and monitors the activity.

## Burrowing Owl (active burrows)

- Non-breeding season: September 1 - January 31-160 feet
- Breeding season: February 1 - August 31 - 250 feet

San Joaquin Kit Fox

- Potential or Atypical den - 50 feet
- Known den - 100 feet
- Natal or pupping den - 500 feet, unless otherwise specified by CDFW

MM BIO-4: If all project activities are completed outside of the Swainson's hawk nesting season (February 15 through August 31), this mitigation measure may be disregarded.

Nesting surveys for the Swainson's hawks shall be conducted in accordance with the protocol outlined in the Recommended Timing and Methodology for Swainson's Hawk Nesting Surveys in California's Central Valley (CDFG 2000). If potential Swainson's hawk nests or nesting substrates are located within 0.5 miles of the project site, then those nests or substrates must be monitored for activity on a routine and repeating basis throughout the breeding season, or until Swainson's hawks or other raptor species are verified to be using them. The protocol recommends that the following visits be made to each nest or nesting site: one visit during January 1-March 20 to identify potential nest sites, three visits during March 20-April 5, three visits during April 5-April 20, and three visits during June 10-July 30. A fewer number of visits may be permissible if deemed adequate by the City after consultation with a qualified biologist. To meet the minimum level of protection for the species, surveys shall be completed for at least the two survey periods immediately prior to project-related ground disturbance activities. If Swainson's hawks are not found to nest within the survey area, then no further action is warranted.

MM BIO-5: If an active Swainson's hawk nest is discovered at any time within 0.5 miles of active construction, a qualified biologist shall complete an assessment of the potential for current construction activities to impact the nest. The assessment will consider the type of construction activities, the location of construction relative to the nest, the visibility of construction activities from the nest location, and other existing disturbances in the area that
are not related to construction activities of this project. Based on this assessment, the biologist shall determine if construction activities can proceed and the level of nest monitoring required. Construction activities shall not occur within 500 feet of an active nest but depending upon conditions at the site this distance may be reduced. Fulltime monitoring to evaluate the effects of construction activities on nesting Swainson's hawks may be required. The qualified biologist shall have the authority to stop work if it is determined that project construction is disturbing the nest. These buffers may need to increase depending on the sensitivity of the nest location, the sensitivity of the nesting Swainson's hawk to disturbances, and at the discretion of the qualified biologist.

MM BIO-6: If construction is planned outside the nesting period for raptors (other than burrowing owl) and migratory birds (February 15 to August 31), no mitigation shall be required. If construction is planned during the nesting season for migratory birds and raptors, a preconstruction survey to identify active bird nests shall be conducted by a qualified biologist to evaluate the site and a 250 -foot buffer for migratory birds and a 500foot buffer for raptors. If nesting birds are identified during the survey, active raptor nests shall be avoided by 500 feet and all other migratory bird nests shall be avoided by 250 feet. Avoidance buffers may be reduced if a qualified on-site monitor determines that encroachment into the buffer area is not affecting nest building, the rearing of young, or otherwise affecting the breeding behaviors of the resident birds. Because nesting birds can establish new nests or produce a second or even third clutch at any time during the nesting season, nesting bird surveys shall be repeated every 30 days as construction activities are occurring throughout the nesting season.

No construction or earth-moving activity shall occur within a non-disturbance buffer until it is determined by a qualified biologist that the young have fledged (left the nest) and have attained sufficient flight skills to avoid project construction areas. Once the migratory birds or raptors have completed nesting and young have fledged, disturbance buffers will no longer be needed and may be removed, and monitoring may cease.

MM BIO-7: A qualified biologist shall conduct a pre-construction survey on the project site and within 500 feet of its perimeter, where feasible, to identify the presence of the western burrowing owl. The survey shall be conducted between 14 and 30 days prior to the start of construction activities. If any burrowing owl burrows are observed during the preconstruction survey, avoidance measures shall be consistent with those included in the CDFW Staff Report on Burrowing Owl Mitigation (CDFG 2012). If occupied burrowing owl burrows are observed outside of the breeding season (September 1 through January 31) and within 250 feet of proposed construction activities, a passive relocation effort may be instituted in accordance with the guidelines established by the California Burrowing Owl Consortium (1993) and the California Department of Fish and Wildlife (2012). During the breeding season (February 1 through August 31), a 500-foot (minimum) buffer zone shall be maintained unless a qualified biologist verifies through noninvasive methods that either the birds have not begun egg laying and incubation or that juveniles from the occupied burrows are foraging independently and are capable of independent survival.

In addition, impacts to occupied burrowing owl burrows shall be avoided in accordance with the following table unless a qualified biologist approved by CDFW verifies through noninvasive methods that either: 1) the birds have not begun egg laying and incubation; or 2) that juveniles from the occupied burrows are foraging independently and are capable of independent survival.

| Location | Time of Year | Level of Disturbance |  |  |
| :--- | :--- | :--- | :--- | :--- |
|  |  | Low | Med | High |
| Nesting sites | April 1-Aug 15 | $200 \mathrm{~m}^{*}$ | 500 m | 500 m |
| Nesting sites | Aug 16-Oct 15 | 200 m | 200 m | 500 m |
| Nesting sites | Oct 16-Mar 31 | 50 m | 100 m | 500 m |

MM BIO-8: Prior to ground disturbance activities, or within one week of being deployed at the project site for newly hired workers, all construction workers at the project site shall attend a Construction Worker Environmental Awareness Training and Education Program, developed and presented by a qualified biologist.

The Construction Worker Environmental Awareness Training and Education Program shall be presented by the biologist and shall include information on the life history wildlife and plant species that may be encountered during construction activities, their legal protections, the definition of "take" under the Endangered Species Act, measures the project operator is implementing to protect the species, reporting requirements, specific measures that each worker must employ to avoid take of the species, and penalties for violation of the Act. Identification and information regarding special-status or other sensitive species with the potential to occur on the project site shall also be provided to construction personnel. The program shall include:

- An acknowledgement form signed by each worker indicating that environmental training has been completed.
- A copy of the training transcript and/or training video/CD, as well as a list of the names of all personnel who attended the training and copies of the signed acknowledgement forms shall be maintain on site for the duration of construction activities.

MM CUL-1: If prehistoric or historic-era cultural materials are encountered during construction activities, all work in the immediate vicinity of the find shall halt until a qualified archaeologist can evaluate the find and make recommendations. Cultural resource materials may include prehistoric resources such as flaked and ground stone tools and debris, shell, bone, ceramics, and fire-affected rock as well as historic resources such as glass, metal, wood, brick, or structural remnants. If the qualified archaeologist determines that the discovery represents a potentially significant cultural resource, additional investigations may be required to mitigate adverse impacts from project implementation. These additional studies may include avoidance, testing, and evaluation or data recovery excavation. Implementation of the mitigation measure below would ensure that the proposed project would not cause a substantial adverse change in the significance of a historical resource.

MM CUL-2: If human remains are discovered during construction or operational activities, further excavation or disturbance shall be prohibited pursuant to Section 7050.5 of the California Health and Safety Code. The specific protocol, guidelines, and channels of communication outlined by the Native American Heritage Commission, in accordance with Section 7050.5 of the Health and Safety Code, Section 5097.98 of the Public Resources Code (Chapter 1492, Statutes of 1982, Senate Bill 297), and Senate Bill 447 (Chapter 44, Statutes of 1987), shall be followed. Section 7050.5(c) shall guide the potential Native American involvement, in the event of discovery of human remains, at the direction of the county coroner.

MM GEO-1: Prior to the ground disturbance activities, a qualified engineer shall be obtained. The project engineer, structural engineer, civil engineer, general contractor, the earthwork contractor shall meet to discuss the grading plan and grading requirements as outlined in the final Geotechnical Report.

MM GEO-2: Prior to issuing of grading or building permits, the project applicant shall submit to the City: (1) the approved Storm Water Pollution Prevention Plan (SWPPP) and (2) the Notice of Intent (NOI) to comply with the General National Pollutant Discharge Elimination System (NPDES) from the Central Valley Regional Water Quality Control Board. The requirements of the SWPPP and NPDES shall be incorporated into design specifications and construction contracts. Recommended Best Management Practices for the construction phase may include the following:

- Stockpiling and disposing of demolition debris, concrete, and soil properly;
- Protecting existing storm drain inlets and stabilizing disturbed areas;
- Implementing erosion controls;
- Properly managing construction materials; and
- Managing waste, aggressively controlling litter, and implementing sediment controls.

Evidence of the approved SWPPP shall be submitted to the Lead Agency.
MM GEO-3: If any paleontological resources are encountered during ground disturbance activities, all work within 25 feet of the find shall halt until a qualified paleontologist as defined by the Society of Vertebrate Paleontology Standard Procedures for the Assessment and Mitigation of Adverse Impacts to Paleontological Resources (2010), can evaluate the find and make recommendations regarding treatment. Paleontological resource materials may include resources such as fossils, plant impressions, or animal tracks preserved in rock. The qualified paleontologist shall contact the Natural History Museum of Los Angeles County or other appropriate facility regarding any discoveries of paleontological resources.

If the qualified paleontologist determines that the discovery represents a potentially significant paleontological resource, additional investigations and fossil recovery may be required to mitigate adverse impacts from project implementation. If avoidance is not feasible, the paleontological resources shall be evaluated for their significance. If the resources are not significant, avoidance is not necessary. If the resources are significant, they shall be avoided to ensure no adverse effects, or such effects must be mitigated. Construction
in that area shall not resume until the resource appropriate measures are recommended or the materials are determined to be less than significant. If the resource is significant and fossil recovery is the identified form of treatment, then the fossil shall be deposited in an accredited and permanent scientific institution. Copies of all correspondence and reports shall be submitted to the Lead Agency.

MM HYD-1: The District shall limit grading to the minimum area necessary for construction and operation of the project. Final grading plans shall include best management practices to limit on-site and off-site erosion.

MM TRA-1: Intersection and roadway improvements needed by the year 2040 to maintain or improve the operational level of service of the street system in the vicinity include:

- Signal at Bust St \& Semas Dr
- Signal at Bust St \& Belle Haven Dr
- Signal at Bust St \& SR 41 SB Ramps
- Signal at Bust St \& SR 41 NB Ramps
- Signal at Bust St \& S. 19th $1 / 2$ Ave


## SECTION 1 - Introduction

## 1.1-Overview

The District is proposing to construct a 42,000-square-foot, two-story Instructional Center (IC) on an undeveloped but disturbed portion of the existing campus. The proposed expansion is anticipated to increase the overall student population by approximately five percent. The IC will be used to expand education opportunities in the areas of allied health services, computer science and graphic arts.

## 1.2-CEQA Requirements

The West Hills Community College District is the Lead Agency for this project pursuant to the CEQA Guidelines (Public Resources Code Section 15000 et seq.). The Environmental Checklist (CEQA Guidelines Appendix G) or Initial Study (IS) (see Section 3 - Initial Study) provides analysis that examines the potential environmental effects of the construction and operation of the project. Section 15063 of the CEQA Guidelines requires the Lead Agency to prepare an IS to determine whether a discretionary project will have a significant effect on the environment. A Mitigated Negative Declaration (MND) is appropriate when an IS has been prepared and a determination can be made that no significant environmental effects will occur because revisions to the project have been made or mitigation measures will be implemented that reduce all potentially significant impacts to less-than-significant levels. The content of an MND is the same as a Negative Declaration, with the addition of identified mitigation measures and a Mitigation Monitoring and Reporting Program (MMRP) (see Section 6 - Mitigation Monitoring and Reporting Program).

Based on the IS, the Lead Agency has determined that the environmental review for the proposed application can be completed with an MND.

## 1.3 - Impact Terminology

The following terminology is used to describe the level of significance of project environmental impacts.

- A finding of "no impact" is appropriate if the analysis concludes that the project would not affect a topic area in any way.
- An impact is considered "less than significant" if the analysis concludes that it would cause no substantial adverse change to the environment and requires no mitigation.
- An impact is considered "less than significant with mitigation incorporated" if the analysis concludes that it would cause no substantial adverse change to the environment with the inclusion of environmental commitments that have been agreed to by the proponent.
- An impact is considered "potentially significant" if the analysis concludes that it could have a substantial adverse effect on the environment.


## 1.4 - Document Organization and Contents

The content and format of this IS/MND is designed to meet the requirements of CEQA. The report contains the following sections:

- Section 1 - Introduction: This section provides an overview of CEQA requirements, intended uses of the IS/MND, document organization, and a list of regulations that have been incorporated by reference.
- Section 2- Project Description: This section describes the project and provides data on the site's location.
- Section 3 - Environmental Checklist: This section contains the evaluation of 21 different environmental resource factors contained in Appendix G of the CEQA Guidelines. Each environmental resource factor is analyzed to determine whether the proposed project would have an impact. One of four findings is made which include: no impact, less-than-significant impact, less than significant with mitigation, or significant and unavoidable. If the evaluation results in a finding of significant and unavoidable for any of the 21 environmental resource factors, then an Environmental Impact Report will be required.
- Section 4-References: This section contains a full list of references that were used in the preparation of this IS/MND.
- Section 5- Preparers
- Section 6- Mitigation Monitoring and Reporting Program (RESERVED)


## 1.5-Incorporated by Reference

The following documents and/or regulations are incorporated into this IS/MND by reference:

- West Hill Master Facilities Plan 2018-2022
- City of Lemoore General Plan
- City of Lemoore 2015 Urban Water Management Plan
- City of Lemoore Master Storm Drain Plan
- 2015 Kings County Emergency Operations Plan
- Kings County General Plan (2010)
- California Title 24 Code of Regulations (2019)


## SECTION 2 - Project Description

## 2.1 - Introduction

The District is proposing to construct a new Instructional Center (IC) on an undeveloped but disturbed portion of the existing campus. The proposed expansion is anticipated to increase the overall student population by approximately five percent. The IC will be used to expand education opportunities in the areas of allied health services, computer science and graphic arts.

## 2.2 - Project Location

The proposed site is in Sections 8, Township 19 South, Range 20 East, Mount Diablo Base and Meridian, within the incorporated City of Lemoore, County of Kings, California. The project site is located on the northwest corner of Pederson Street and College Avenue, and is an approximately 27.1 acre portion of Assessor's Parcel Numbers 023-510-018, within Section 8, Township 19S, Range 20E, MMB\&M. The regional location is depicted on Figure 2-1 and the project site location is depicted on Figure 2-2.

The project is within the Lemoore General Plan, which designates the project site as Community Facilities (Figure 2-3). Additionally, the project site is zoned Public Services and Community Facilities (CF). However, as a special district, the project does not fall under the jurisdiction of the Kings County Zoning Ordinance or General Plan, and therefore is not subject to land use regulations

## 2.3 - Project Environment

West Hills College Lemoore was constructed in 2002 and serves a student population of approximately 6,500 students (West Hills College Lemoore, 2018). Fire service would be served by the Lemoore Fire Department located at 610 Fox Street in Lemoore. Police service would be served by the City of Lemoore Police Department located at 657 Fox Street in Lemoore. Sanitation/garbage collection will be provided by a local waste hauler. Water and sewer service will be provided by City of Lemoore.

## 2.4-Proposed Project

The District proposes to construct a 42,429-square-foot, two-story Instructional Center (IC) on an undeveloped but disturbed portion of the existing campus. The college has a current student enrollment of 4,600 students and the proposed expansion is anticipated to increase the overall student population by approximately five percent, or approximately 232 students. The IC will be used to expand education opportunities in the areas of allied health services, computer science and graphic arts.

Construction will include site clearing, rough and finished grading, trenching, backfill for underground facilities, and concrete for circulation surfaces. The two-story building will match existing campus standard and include steel framing, concrete floors, built up roofing
over steel decking, and brick exterior finishes, metal roofing accents, and an elevator which will support future expansion. The project consists of lecture, laboratory, office and other rooms used for educational purposes.

The project will match the existing construction and space standards set by the District. Construction is expected to begin in January 2023 and end in April 2024. Construction equipment will include a crane, bulldozer, grader, bob cat, trencher, cement trucks, water trucks, trash trucks, equipment delivery trucks, and company work vehicles.



Figure 2-2

## Project Site



## SECTION 3 - Evaluation of Environmental Impacts

## 3.1 - Environmental Checklist and Discussion

## 1. Project Title:

West Hills College Lemoore Campus Instructional Center Project
2. Lead Agency Name and Address:

West Hills Community College District
275 Phelps Avenue
Coalinga, CA 93210
3. Contact Person and Phone Number:

Richard Storti, Deputy Chancellor
Phone: (559) 934-2160
4. Project Location:

The project site is located on the northwest corner of Pederson Street and College Avenue in the City of Lemoore, Kings County, CA. The project site includes Assessor's Parcel Number (APN) 023-510-018, which totals approximately 27.1 acres in area.
5. Project Sponsor's Name and Address:

Richard Storti, Deputy Chancellor
Phone: (559) 934-2160
6. General Plan Designation:

Community Facilities
7. Zoning:

Public Services and Community Facilities (CF)
8. Description of Project:

See Section 2.4 - Proposed Project.
9. Surrounding Land Uses and Setting:

See Section 2.3 - Surrounding Land Uses and Figure 2-3.

## 10. Other Public Agencies Whose Approval May be Required:

- San Joaquin Valley Air Pollution Control District (SJVAPCD)
- Regional Water Quality Control Board - Central (RWQCB)
- State Water Resource Control Board (SWRCB)
- Division of the State Architect (DSA)

11. Have California Native American tribes traditionally and culturally affiliated with the project area requested consultation pursuant to Public Resources Code Section 21080.3.1? If so, has consultation begun?

On November 24, 2020, the Native American Heritage Commission (NAHC) conducted a search of its Sacred Lands File to identify previously recorded sacred sites or cultural resources of special importance to tribes and provide contact information for local Native American representatives who may have information about the project area. The NAHC responded on December 18, 2020, with its findings and attached a list of Native American tribes and individuals culturally affiliated with the project area. On December 10, 2020, an outreach letter was mailed or emailed to each of the contacts identified by the NAHC (Appendix C). The outreach letter and follow-up calls are considered best practices within cultural resource management. To date, no response has been received from the tribes.

NOTE: Conducting consultation early in the CEQA process allows tribal governments, lead agencies, and project proponents to discuss the level of environmental review, identify and address potential adverse impacts to tribal cultural resources, and reduce the potential for delay and conflict in the environmental review process. (See Public Resources Code Section 21083.3.2.) Information may also be available from the California Native American Heritage Commission’s Sacred Lands File per Public Resources Code Section 5097.96 and the California Historical Resources Information System administered by the California Office of Historic Preservation. Please also note that Public Resources Code Section 21082.3(c) contains provisions specific to confidentiality.

## 3.2 - Environmental Factors Potentially Affected:

The environmental factors checked below would be potentially affected by this project, involving at least one impact that is a "Potentially Significant Impact" as indicated by the checklist on the following pages.

| $\square$ | Aesthetics | $\square$ | Agriculture and Forest <br> Resources | $\square$ | Air Quality |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\square$ | Biological Resources | $\square$ | Cultural Resources | $\square$ | Geology/Soils |
| $\square$ | Greenhouse Gas | $\square$ | Hazards \& Hazardous | $\square$ | Hydrology/Water |
|  | Emissions |  | Materials |  |  |
| $\square$ | Land Use/Planning | $\square$ | Mineral Resources | $\square$ | Noise |
| $\square$ | Population/Housing | $\square$ | Public Services | $\square$ | Recreation |
| $\square$ | Transportation/Traffic | $\square$ | Utilities/Service | $\square$ | Findings of |
| $\square$ |  | Systems |  | Significance |  |

## 3.3 - Determination

On the basis of this initial evaluation:
$\square$ I find that the proposed project COULD NOT have a significant effect on the environment, and a NEGATIVE DECLARATION will be prepared.
$\boxtimes \quad$ I find that although the proposed project could have a significant effect on the environment, there will not be a significant effect in this case because revisions in the project have been made by or agreed to by the project proponent. A MITIGATED NEGATIVE DECLARATION will be prepared.
$\square$ I find that the proposed project MAY have a significant effect on the environment, and an ENVIRONMENTAL IMPACT REPORT is required.
$\square$ I find that the proposed project MAY have a "potentially significant impact" or "potentially significant unless mitigated" impact on the environment, but at least one effect (a) has been adequately analyzed in an earlier document pursuant to applicable legal standards, and (b) has been addressed by mitigation measures based on the earlier analysis as described on attached sheets. An ENVIRONMENT IMPACT REPORT is required, but it must analyze only the effects that remain to be addressed.
$\square$ I find that although the proposed project could have a significant effect on the environment, because all potentially significant effects (a) have been analyzed adequately in an earlier EIR or NEGATIVE DECLARATION pursuant to applicable
standards, and (b) have been avoided or mitigated pursuant to that earlier EIR or NEGATIVE DECLARATION, including revisions or mitigation measures that are imposed upon the proposed project, nothing further is required.

RichardStorti
Richard Storti, Deputy Chancellor

12/24/2020
Date

## 3.4-Evaluation of Environmental Impacts

1. A brief explanation is required for all answers except "No Impact" answers that are adequately supported by the information sources a lead agency cites in the parentheses following each question. A "No Impact" answer is adequately supported if the referenced information sources show that the impact simply does not apply to projects like the one involved (e.g., the project falls outside a fault rupture zone). A "No Impact" answer should be explained where it is based on project-specific factors as well as general standards (e.g., the project will not expose sensitive receptors to pollutants, based on a projectspecific screening analysis).
2. All answers must take account of the whole action involved, including offsite as well as onsite, cumulative as well as project-level, indirect as well as direct, and construction as well as operational impacts.
3. Once the lead agency has determined that a particular physical impact may occur, then the checklist answers must indicate whether the impact is potentially significant, less than significant with mitigation, or less than significant. "Potentially Significant Impact" is appropriate if there is substantial evidence that an effect may be significant. If there are one or more "Potentially Significant Impact" entries when the determination is made, an EIR is required.
4. "Negative Declaration: "Less Than Significant With Mitigation Incorporated" applies where the incorporation of mitigation measures has reduced an effect from "Potentially Significant Impact" to a "Less-Than-Significant Impact." The lead agency must describe the mitigation measures, and briefly explain how they reduce the effect to a less-thansignificant level (mitigation measures from "Earlier Analyses," as described in (5) below, may be cross-referenced).
5. Earlier analyses may be used where, pursuant to the tiering, program EIR, or other CEQA process, an effect has been adequately analyzed in an earlier EIR or negative declaration. Section 15063(c)(3)(D). In this case, a brief discussion should identify the following:
a. Earlier Analysis Used. Identify and state where they are available for review;
b. Impacts Adequately Addressed. Identify which effects from the above checklist were within the scope of and adequately analyzed in an earlier document pursuant to applicable legal standards, and state whether such effects were addressed by mitigation measures based on the earlier analysis; and
c. Mitigation Measures. For effects that are "Less than Significant with Mitigation Measures Incorporated," describe the mitigation measures which were incorporated or refined from the earlier document and the extent to which they address sitespecific conditions for the project.
6. Lead agencies are encouraged to incorporate into the checklist references to information sources for potential impacts (e.g., general plans, zoning ordinances). Reference to a
previously prepared or outside document should, where appropriate, include a reference to the page or pages where the statement is substantiated.
7. Supporting Information Sources: A source list should be attached, and other sources used, or individuals contacted should be cited in the discussion.
8. This is only a suggested form, and lead agencies are free to use different formats; however, lead agencies should normally address the questions from this checklist that are relevant to a project's environmental effects in whatever format is selected.
9. The explanation of each issue should identify:
a. The significance criteria or threshold, if any, used to evaluate each question; and
b. The mitigation measure identified, if any, to reduce the impact to less than significant.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.1-Aesthetics

Would the project:
a. Have a substantial adverse effect on a scenic vista?
b. Substantially damage scenic resources, including, but not limited to, trees, rock outcroppings, and historic buildings within a state scenic highway?
c. In non-urbanized area, substantially degrade the existing visual character or quality of public views of the site and its surroundings? If the project is in an urbanized area, would the project conflict with applicable zoning and other regulations governing scenic quality?
d. Create a new source of substantial light or glare that would adversely affect day or nighttime views in the area?

## Discussion

Impact \#3.4.1a - Would the project have a substantial adverse effect on a scenic vista?
As seen in Figure 2-1, the project site consists of a partially undeveloped land and is surrounded by the developed existing school campus to the north, east, and south. The project site is located on the northwest corner of Pederson Street and College Avenue Lemoore, Kings County, CA.

There are no natural features or landmark buildings within the vicinity of the project site (City of Lemoore, 2008). The project is not located in an area that would result in substantial adverse effects on any scenic vistas, therefore, causing no negative impacts. Any construction-related related impacts to the visual character of the site and its surroundings would be temporary, therefore, there would be no impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.1b - Would the project substantially damage scenic resources, including, but not limited to, trees, rock outcroppings, and historic buildings within a state scenic highway?

There are no listed State scenic highways within or near the City of Lemoore, nor are there scenic highways in Kings County (California Department of Transportation, 2020). The closest eligible scenic highway is SR 41, southwest of SR 33, which is approximately 35 miles southwest of the project site. Further, the project does not include the removal of trees determined to be scenic or of scenic value, the destruction of rock outcroppings or degradation of any historic building. The project will not result in development that is substantially different than surrounding land uses. Therefore, impacts to scenic resources would be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.1c - In non-urbanized area, substantially degrade the existing visual character or quality of public views of the site and its surroundings? If the project is in an urbanized area, would the project conflict with applicable zoning and other regulations governing scenic quality?

The entirety of the project will be within the existing and developed campus. The project's appearance will be similar in character to the existing buildings and would not degrade the visual character of the site or its surroundings. Therefore, the project would not result in a substantial impact to the visual quality of the area.

See also discussion of Impact \#3.4.1a, above.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.1d - Would the project create a new source of substantial light or glare that would adversely affect day or nighttime views in the area?

Construction of the proposed project would be temporary and generally occur during daytime hours, typically from 7:00 a.m. to 6:00 p.m. All lighting would be directed downward and shielded to focus illumination on the desired work areas only and prevent light spillage onto adjacent properties. Because lighting used to illuminate work areas would be shielded, focused downward, and turned off by 6:00 p.m., the potential for lighting to affect any residents adversely is minimal. Increased truck traffic and the transport of construction materials to the project site would temporarily increase glare conditions during construction. However, this increase in glare would be minimal. Construction activity would focus on specific areas on the sites, and any sources of glare would not be stationary for a prolonged period of time. Therefore, construction of the proposed project would not create a new source of substantial glare that would affect daytime views in the area.

Upon completion of the construction, the project will not create a new source of light and glare beyond what is already existing on the campus. Any light and glare impacts related to the construction of the proposed project would be temporary, therefore, the project would have a less-than-significant impact.

## Mitigation Measure(s)

No mitigation is required.

## LEVEL OF SIGNIFICANCE

Impacts would be less than significant.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.2 - Agriculture and Forestry Resources

In determining whether impacts to agricultural resources are significant environmental effects, lead agencies may refer to the California Agricultural Land Evaluation and Site Assessment Model (1997) prepared by the California Department of Conservation as an optional model to use in assessing impacts on agriculture and farmland. In determining whether impacts to forest resources, including timberland, are significant environmental effects, lead agencies may refer to information compiled by the California Department of Forestry and Fire Protection regarding the state's inventory of forest land, including the Forest and Range Assessment Project and the Forest Legacy Assessment Project; and forest carbon measurement methodology provided in Forest Protocols adopted by the California Air Resources Board. Would the project:
a. Convert Prime Farmland, Unique Farmland, or Farmland of Statewide Importance (Farmland), as shown on the maps prepared pursuant to the Farmland Mapping and Monitoring Program of the California Resources Agency, to nonagricultural use?
b. Conflict with existing zoning for agricultural use or a Williamson Act contract?
c. Conflict with existing zoning for, or cause rezoning of, forest land (as defined in Public Resources Code Section 12220 (g)), timberland (as defined by Public Resources Code Section 4526), or timberland zoned Timberland Production (as defined by Government Code Section 51104(g))?
d. Result in the loss of forest land or conversion of forest land to non-forest use?
e. Involve other changes in the existing environment which, due to their location or nature, could result in conversion of Farmland, to nonagricultural use or conversion of forest land to non-forest use?

## Discussion

Impact \#3.4.2a - Would the project convert Prime Farmland, Unique Farmland, or Farmland of Statewide Importance (Farmland), as shown on the maps prepared pursuant to the Farmland Mapping and Monitoring Program of the California Resources Agency, to nonagricultural use?

The proposed project will not convert any Prime Farmland, Unique Farmland, or Farmland of Statewide Importance. According to the Department of Conservation's Farmland Mapping
and Monitoring Program (FMMP), the project site is classified as "Urban and Built-Up Land" (Figure 3.4.2-1), which is defined as:

- Urban and Built-Up Land - Land occupied by structures with a building density of at least one unit to 1.5 acres, or approximately six structures to a 10 -acre parcel. This land is used for residential, industrial, commercial, construction, institutional, public administration, railroad and other transportation yards, cemeteries, airports, golf courses, sanitary landfills, sewage treatment, water control structures, and other developed purposes.

The site also is not currently used for farming and is not zoned for agricultural use. Considering these factors, the proposed project will have no impact on conversion of agricultural resources.

## Mitigation Measure(s)

No mitigation is required.

## LEVEL OF SIGNIFICANCE

There would be no impact.
Impact \#3.4.2b - Would the project conflict with existing zoning for agricultural use or a Williamson Act contract?

See response to Impact \#3.4.2a.
According to the City of Lemoore's Zoning Ordinance, the project site's zoning classification is Public Services and Community Facilities. The project site is not subject to a Williamson Act contract and would not conflict with any current Williamson Act contracted land in the vicinity. Therefore, the project will not conflict with existing zoning for agricultural use or a Williamson Act contract.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.2c - Would the project conflict with existing zoning for, or cause rezoning of, forest land (as defined in Public Resources Code Section 12220(g)), timberland (as defined by Public Resources Code Section 4526), or timberland zoned Timberland Production (as defined by Government Code Section 51104(g))?

According to the City of Lemoore Zoning Map, the project site and the adjacent properties are not zoned for forest land or timberland. The site will remain as Community Facilities land use designation. The project will have no impact on land designated for forest land or timberland use.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.2d - Would the project result in the loss of forest land or conversion of forest land to non-forest use?

See discussion of Impact \#3.4.2c, above.
The proposed project will have no impact.
Mitigation Measure(s)
No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.2e - Would the project involve other changes in the existing environment which, due to their location or nature, could result in conversion of Farmland, to nonagricultural use or conversion of forest land to non-forest use?

See discussion of Impact \#3.4.2c, above.
The proposed project will have no impact.
Mitigation Measure(s)
No mitigation is required.
Level of Significance
There would be no impact.



|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.3 - AIR QuALITY

Where available, the significance criteria established by the applicable air quality management or air pollution control district may be relied upon to make the following determinations. Would the project:
a. Conflict with or obstruct implementation of the applicable air quality plan?


## Discussion

The analysis below is based on a Small Project Analysis Level Assessment (SPAL) prepared for the Project (Trinity Consultants, 2020). The SPAL is included in this document as Appendix A.

## Impact \#3.4.3a - Would the project conflict with or obstruct implementation of the applicable air quality plan?

The project is located within the San Joaquin Valley Air Basin (SJVAB), which and under the jurisdiction of the San Joaquin Valley Air Pollution Control District (SJVAPCD). The SJVAB is designated nonattainment of State and federal health-based air quality standards for ozone and $\mathrm{PM}_{2.5}$. The SJVAB is designated nonattainment of State $\mathrm{PM}_{10}$. To meet Federal Clean Air Act (CAA) requirements, the SJVAPCD has multiple air quality attainment plan (AQAP) documents, including:

- 2016 Ozone Plan;
- 2007 PM ${ }_{10}$ Maintenance Plan and Request for Redesignation; and
- 2016 PM2.5 Plan.

The SJVAPCD's Guidance for Assessing and Mitigating Air Quality Impacts (GAMAQI) thresholds are designed to implement the general criteria for air quality emissions as
required in the CEQA Guidelines, Appendix G, Paragraph III (Title 14 of the California Code of Regulations $\S 15064.7$ ) and CEQA (California Public Resources Code Sections 21000 et. al). SJVAPCD's specific CEQA air quality thresholds are presented in Table 3.4.3-1.

Table 3.4.3-1
GAMAQI Thresholds of Significance for Criteria Pollutants

| Criteria Pollutant | Threshold (tons/year) |
| :---: | :---: |
| CO | 100 |
| ROG | 10 |
| NOx | 10 |
| SOx | 27 |
| PM $_{10}$ | 15 |
| PM $_{2.5}$ | 15 |
| (Sale |  |

(San Joaquin Air Pollution Control District, 2015)
The project's anticipated construction duration for the proposed project is approximately 15 months. Stationary sources that comply or that would comply with Air District Rules and Regulations are generally not considered to have a significant air quality impact.

During construction, the proposed project would be subject to Regulation VIII (Fugitive PM ${ }_{10}$ Prohibition) of the SJVAPCD. The purpose of Regulation VIII is to reduce ambient concentrations of fine particulate matter ( $\mathrm{PM}_{10}$ ) by requiring actions to prevent, reduce or mitigate anthropogenic fugitive dust emissions. Regulation VIII would require fugitive dust emission controls at the construction site such as water application, dust suppressants, reduced vehicle speeds on unpaved roads (SJVAPCD, 2017).

The SJVAPCD Small Project Analysis Level (SPAL) process established review parameters to determine whether a project qualifies as a "small project." A project that is found to be "less than" the established parameters, according to the SPAL review parameters, has "no possibility of exceeding criteria pollutant emissions thresholds."

As shown in Table 3.4.3-2, the proposed project would not exceed the established SPAL limits for an educational project. The project would construct a 42,429 -square-foot Instructional Center compared to the allowable project size for junior college project, which is 74,400 square feet. Based on the above information, this project qualifies for a limited air quality analysis applying the SPAL guidance to determine air quality impacts.

Table 3.4.3-2
Small Project Analysis Level - Units for Educational

| Land Use Category -Educational | Project Size (square feet) |
| :---: | :---: |
| Elementary | 156,000 |
| Junior High School | 168,000 |
| High School | 153,600 |
| Junior College (2 year) | 74,400 |
| University/College (4 year) | 1,200 students |
| Library | 38,400 |
| Place of Worship | 141,000 |
| Proposed Project - Junior College | 42,000 |
| SPAL Exceeded? | No |

Source: (Trinity Consultants, 2020)
Table 3.4.3-3
Small Project Analysis Level - Daily Trips for Educational Institutions

| Land Use Category -Educational | Average Daily Trips <br> (non-HHD) | Average <br> Daily Trips <br> (HHD)* |
| :---: | :---: | :---: |
| Elementary |  |  |
| Junior High School |  | 15 |
| High School | 1,000 |  |
| Junior College (2 year) |  | 15 |
| University/College (4 year) |  | No |
| Library |  |  |
| Place of Worship | 997 | No |
| Proposed Project - Junior College |  |  |
| SPAL Exceeded? |  |  |

Source: (Trinity Consultants, 2020)
As shown in Table 3.4.3-3, the proposed project would not exceed the established SPAL limits for a "Junior College" educational project. The project would include 997 additional daily trips for all vehicle types except HHD and 15 additional daily trips for HHD vehicles. The SPAL threshold for HHD trips is based on a 50-mile trip length. The HHD trips for the proposed project are based on a 47.6-mile trip length. Construction and operation of the proposed project would not exceed any established SJVAPCD thresholds; therefore, impacts would be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.3b - Would the project result in a cumulatively considerable net increase of any criteria pollutant for which the project region is nonattainment under an applicable federal or State ambient air quality standard (including releasing emissions which exceed quantitative thresholds for ozone precursors)?

The nonattainment pollutants for the SJVAPCD are ozone, $\mathrm{PM}_{10}$ and $\mathrm{PM}_{2.5}$. Therefore, the pollutants of concern for this impact are ozone precursors, and regional $\mathrm{PM}_{10}$, and $\mathrm{PM}_{2} .5$. As discussed above, the thresholds of significance used for determination of emission significance are shown in Table 3.4.3-1 above. The proposed project would create NOx and $\mathrm{PM}_{10}$ emissions during construction, which would contribute to the current nonattainment status of these pollutants within the SJVAB. As noted in Impact \#3.4.3a, the project's emissions during temporary construction activities would not exceed thresholds.

Operation of the project would also create additional criteria pollutants, particularly as a result of increased mobile emissions in the project area. However, these impacts also would not exceed thresholds.

Because project construction at the project site would not result in significant emissions for which the SJVAPCD and surrounding air districts are in nonattainment, construction emissions would not result in a cumulatively considerable net increase. Further, as the proposed project would not result in significant operational emissions of criteria pollutants, the proposed project would not contribute to a long-term cumulative increase in criteria pollutants.

## Construction

Construction is expected to begin in January 2023 and end in April 2024. Project construction emissions of NOx and $\mathrm{PM}_{10}$ were calculated using default CalEEMod factors for construction of a new 42,000-square-foot, two-story Instruction Center on an undeveloped but disturbed portion of the existing campus (see Appendix A).

The primary source of NOx is off-road diesel construction equipment and on-road diesel emissions during hauling activities. The primary source of $\mathrm{PM}_{10}$ is from site preparation and grading activities. Table 3.4.3-4 shows construction emission levels do not exceed the SJVAPCD localized emission screening thresholds and would therefore have a less-thansignificant impact from localized criteria pollutant emissions.

Table 3.4.3-4 Construction Emissions

| Emissions Source | ROG | NOx | CO | SOx | PM $_{10}$ | PM $_{2.5}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | (tons/year) |  |  |
| 2023 Construction Emissions | 0.10 | 0.91 | 1.01 | 0.0002 | 0.08 | 0.05 |  |
| 2024 Construction Emissions | 0.31 | 0.20 | 0.25 | 0 | 0.02 | 0.01 |  |
| SJVAPCD Construction Emissions Thresholds | 10 | 10 | 100 | 27 | 15 | 15 |  |
| Is Threshold Exceeded? | No | No | No | No | No | No |  |

Notes: $\mathrm{NO}_{\mathrm{X}}=$ nitrogen oxides, $\mathrm{PM}_{10}=$ particulate matter
Source: (Trinity Consultants, 2020)
As seen in Table 3.4.3-4, emissions from the project are below the SJVAPCD's thresholds.

## Operation

Operational emissions occur over the lifetime of the project generated from mobile, energy, and area sources as well as from water use and waste generation emissions. Operational emissions are presented in Table 3.4.3-5. The results of the analysis show that emissions are below the annual emission thresholds for each pollutant.

Table 3.4.3-5
Total Project Operational Emissions

| Emissions Source | ROG | NOx | C0 | S0x | $\mathrm{PM}_{10}$ | PM 2.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (tons/year) |  |  |  |  |  |
| Unmitigated |  |  |  |  |  |  |
| Operational Emissions | 0.38 | 2.38 | 2.00 | 0.01 | 0.87 | 0.24 |
| SJVAPCD Operational Emissions Thresholds -non-permitted sources | 10 | 10 | 100 | 27 | 15 | 15 |
| Is Threshold Exceeded Before Mitigation? | No | No | No | No | No | No |
| Mitigated |  |  |  |  |  |  |
| Operational Emissions | 0.38 | 2.34 | 1.91 | 0.01 | 0.81 | 0.22 |
| SJVAPCD Operational Emissions Thresholds -non-permitted sources | 10 | 10 | 100 | 27 | 15 | 15 |
| Is Threshold Exceeded? | No | No | No | No | No | No |

Notes: $\mathrm{NO}_{\mathrm{x}}=$ nitrogen oxides, $\mathrm{PM}_{10}=$ particulate matter
Source: (Trinity Consultants, 2020)

The long-term operational emissions associated with the proposed project would be less than SJVAPCD significance threshold levels and would, therefore, not pose a significant impact to criteria air pollutants. This finding is consistent with the SPAL screening thresholds. The project would not exceed SJVAPCD daily operational screening thresholds and would result in less-than-significant localized impacts.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.3c - Would the project expose sensitive receptors to substantial pollutant concentrations?

The proposed project is located near the southwest corner of Bush Street and College Avenue. Sensitive receptors are defined as areas where young children, chronically ill individuals, the elderly, or people who are more sensitive than the general population reside. Schools, hospitals, nursing homes and daycare centers are locations where sensitive receptors would likely reside. There are currently sensitive receptors at the existing Lemoore University Elementary Charter and Lemoore Middle College High School located on the proposed project site. There are no other known schools, hospitals, or nursing homes within a one-mile radius of the project.

Based on the predicted operational emissions and activity types, the proposed Project is not expected to affect any on-site or off-site sensitive receptors and is not expected to have any adverse impacts on any known sensitive receptor.

The proposed project once constructed is not expected to result in the generation of odors or other hazardous air pollutants. However, during construction of the project, construction activities and equipment may generate emission from construction equipment exhaust. These impacts are localized and temporary in nature and therefore are considered less than significant. The project would not expose sensitive receptors to substantial concentrations of localized $\mathrm{PM}_{10}$, carbon monoxide, diesel particulate matter, hazardous air pollutants, or naturally occurring asbestos, as discussed below.

## Hazardous Pollutants or Odors

The GAMAQI guidelines introduce two types of projects that should be assessed when considering hazardous air pollutants (HAPs) which includes: (1) placing a toxic land use in an area where it may have an adverse health impact on an existing sensitive land use and (2) placing a sensitive land use in an area where an adverse health impact may occur from an existing toxic land use. Some examples of projects that may include HAPs are:

- Agricultural products processing;
- Bulk material handling;
- Chemical blending, mixing, manufacturing, storage, etc.;
- Combustion equipment (boilers, engines, heaters, incinerators, etc.);
- Metals etching, melting, plating, refining, etc.;
- Plastics \& fiberglass forming and manufacturing;
- Petroleum production, manufacturing, storage, and distribution; and
- Rock \& mineral mining and processing.

The proposed project is located on a site that is currently undeveloped but disturbed land. During the construction period some odors could result from vehicles and equipment using diesel fuels. However, vehicles and equipment using diesel fuels at the proposed project would have to comply with the California Air Resources Board (CARB) guidelines, which limit idling time to five minutes with the Airborne Toxic Control Measure (ATCM). All construction would be temporary. The project is not expected to expose sensitive receptors to substantial pollutant concentrations. Therefore, impacts will be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.3d - Would the project result in emissions (such as those leading to odors) adversely affecting a substantial number of people?

Sensitive receptors include locations where young children, chronically ill individuals, the elderly, or people who are more sensitive than the general population reside, such as schools, hospitals, nursing homes, and daycare centers. The Lemoore Elementary Charter School is located in close proximity to the project site. Although emissions from construction-related vehicles are anticipated during temporary construction activities, the proposed project is not expected to affect these sensitive receptors. Construction equipment will be used during limited times and of short duration and is not anticipated to generate significant amounts of emissions.

As discussed in Impact \#3.4.3c, above. The residential nature of this project is not expected to result in the generation of odors or hazardous air pollutants that would affect a substantial number of people. The emissions associated with the construction of the project would be temporary in nature and are not anticipated to result in the generation of a substantial amount of hazardous air pollutants. Therefore, the project will have a less-than-significant impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.

|  | Less than <br> Significant |  |  |
| :---: | :---: | :---: | :---: |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.4-Biological Resources

Would the project:
a. Have a substantial adverse effect, either directly or through habitat modifications, on any species identified as a candidate, sensitive, or special-status species in local or regional plans, policies, or regulations or by the California Department of Fish and Wildlife or U.S. Fish and Wildlife Service?
b. Have a substantial adverse effect on any riparian habitat or other sensitive natural community identified in local or regional plans, policies, regulations, or by the California Department of Fish and Wildlife or U.S. Fish and Wildlife Service?
c. Have a substantial adverse effect on State or federally protected wetlands (including, but not limited to, marsh, vernal pool, coastal, etc.) through direct removal, filling, hydrological interruption, or other means?
d. Interfere substantially with the movement of any native resident or migratory fish or wildlife species, or with established native resident or migratory wildlife corridors, or impede the use of native wildlife nursery sites?
e. Conflict with any local policies or ordinances protecting biological resources, such as a tree preservation policy or ordinance?
f. Conflict with the provisions of an adopted habitat conservation plan, natural community conservation plan, or other approved local, regional, or state habitat conservation plan?

## Discussion

The biological resources evaluation is based upon a review of available literature and databases and existing site conditions evaluated during a reconnaissance survey. These studies evaluated the potential for sensitive biological resources to occur on and in the vicinity of the project, and any impacts that could potentially occur.

Reviews of the California Department of Fish and Wildlife's California Natural Diversity Database (California Department of Fish and Wildlife, 2020), the California Native Plant Society's Rare Plant Program Inventory (California Native Plant Society, 2020), and the United States Fish and Wildlife Service's Information for Planning and Consultation online tool (US Fish and Wildlife Service, 2020) were conducted to identify special-status plant and wildlife species with the potential to occur within the project and in the vicinity of the project (the Lemoore 7.5" USGS quadrangle, within which the project is situated, and the surrounding eight quads). Information regarding the presence of Critical Habitat in the project vicinity was obtained from the United States Fish and Wildlife Service’s Critical Habitat Mapper database (USFWS, 2020b). The results of the database inquiries were reviewed to evaluate the potential for occurrence of special-status species and other sensitive biological resources known to occur on or near the project site prior to conducting the biological reconnaissance survey.

On December 1, 2020, QK biologist Shannon Gleason conducted a biological reconnaissance survey of the project and accessible areas within 250 feet (Survey Area). Meandering pedestrian transects were walked through the Survey Area to achieve 100 percent visual coverage, with the aid of binoculars. The purpose of the survey was to determine the presence and extent of existing plant communities and any sensitive habitats, the presence and potential for occurrence of special-status plant and animal species, and to identify any other sensitive biological resources within the Survey Area. Protocol surveys for specific special-status wildlife species were not conducted. Locations of sensitive biological resources were documented using the ArcGIS Collector application installed on an iPad. Photographs were taken to document the existing landscape and sensitive biological resources; detailed notes on observed plant and wildlife species and site conditions were taken while conducting the survey.

## General Site Conditions

The project area is within the footprint of the West Hills College Lemoore campus, which was constructed in 2002. Prior to the development of the campus, the land on which it is situated was used for agriculture. The campus is located in the San Joaquin Valley, most of which has been developed for agricultural and urban use. The West Hills College Lemoore campus has been developed with numerous permanent buildings and semi-permanent modular buildings, parking lots, manicured lawns, sidewalks, and soccer fields. There is a freshwater pond just west of the southwest corner of the campus (outside of the Survey Area) that is surrounded by native habitat. The project site is located between existing buildings. There is a small pile of concrete rubble and some short open-ended pipes in the Survey Area buffer west of the project site. Southwest of the project there are two small seatrains and another open-ended pipe.

Some of the campus has not yet been developed and supports non-native grassland habitat, which consists mainly of ruderal plant species such as red brome (Bromus madritensis ssp. rubens), annual burweed (Ambrosia acanthicarpa), and Russian thistle (Salsola tragus). Seepweed (Saueda nigra) was also found in this natural habitat where the ground was slightly depressed. The natural habitat is found in some of the Survey Area buffer west and
south of the project site. Plant species found in the developed areas of the campus include Bermuda grass (Cynodon dactylon), common groundsel (Senecio vulgaris), oleander (Nerium oleander), and various ornamental species.

A gravel road bisects the project site into two halves. The northern half of the project site is covered by a Bermuda grass lawn. The southern half is vegetated by red brome, Bermuda grass, pigweed amaranth (Amaranthus albus), and Russian thistle, all of which was dead and dry at the time of the survey, and appears to be routinely cut to control growth.

The wildlife species observed during the survey were typical of urban and grassland habitats. Most of the bird species observed were detected on the west side of the Survey Area where there is undeveloped habitat. A desert cottontail (Sylvilagus audubonii) was also observed in this area. Several gopher (Thomomys bottae) mounds were observed south of the project site. There were very few small mammal burrows in the Survey Area; a few were observed in the southeastern corner of the project site where there is compacted soil, and these were in very poor condition and did not appear active. There are modular buildings in the southeastern corner of the Survey Area, and there are multiple gaps under these buildings that would allow wildlife to enter the crawlspace underneath the buildings.

There were 17 plant species, six bird species, and two mammal species identified during the reconnaissance survey, either through direct observation or by the presence of diagnostic signs (Table 3.4.4-1). None of these species are listed under the federal or California Endangered Species Acts.

## Impact Analysis

This section describes the results of the database searches and, using conditions present on the project as determined by the reconnaissance survey, provides an analysis of project impacts on each of six biological evaluation criteria. Each of the biological evaluation criteria were determined to be in one of three categories: less-than-significant impacts with mitigation incorporated, less-than-significant impacts, and no impacts. Each of the evaluation criteria are discussed below and mitigation measures are provided as warranted to, when implemented, reduce impacts to below significant levels.

Impact \#3.4.4a - Would the project have a substantial adverse effect, either directly or through habitat modifications, on any species identified as a candidate, sensitive, or specialstatus species in local or regional plans, policies, or regulations or by the California Department of Fish and Wildlife or the U.S. Fish and Wildlife Service?

The literature search indicated that there is potential for several special-status species to be present on or in the vicinity of the project. An evaluation of each of the potential specialstatus species, which included habitat requirements, likelihood of required habitat to occur within the project area, and a comparison to the CNDDB records was conducted. The results of this evaluation concluded that nine plant, one natural community, and12 wildlife species with special status have a reasonable potential to occur on or near the project.

Table 3.4.4-1
List of Plant and Wildlife Species Observed on the Project Site

| Scientific name | Common name |
| :---: | :---: |
| Amaranthus albus | pigweed amaranth |
| Ambrosia acanthicarpa | annual burweed |
| Bromus madritensis ssp. rubens | red brome |
| Chenopodium sp. | goosefoot |
| Cynodon dactylon | Bermuda grass |
| Erigeron canadensis | horseweed |
| Heterotheca grandiflora | telegraph weed |
| Malva parviflora | cheeseweed |
| Nerium oleander | oleander |
| Phalaris sp. | canarygrass |
| Salsola tragus | Russian thistle |
| Senecio vulgaris | common groundsel |
| Sorghum halepense | johnsongrass |
| Suaeda nigra | seepweed |
| Taraxicum officinale | common dandelion |
| Trifolium hirtum | rose clover |
| Washingtonia filifera | California fan palm |
| Warious ornamental |  |
| Anthus rubescens | American pipit |
| Charadrius vociferus | killdeer |
| Corvus corax | common raven |
| Eremophila alpestris | horned lark |
| Mimus polyglottos | northern mockingbird |
| Sturnella neglecta | western meadowlark |
| Sylvilagus audubonii | desert cottontail |
| Thomomys bottae | Botta's pocket gopher* |

*Indicates that only sign of the species (e.g., scat, tracks, burrows) was observed.

## Special-Status Species

## Special-Status Plant Species

Based on the survey and database queries, there are seven special-status plant species that have the potential to occur within the subject quadrangle and eight surrounding quadrangles: brittlescale (Atriplex depressa), recurved larkspur (Delphinium recurvatum), vernal barley (Hordeum intercedens), alkali sink goldfields (Lasthenia chrysantha), Panoche peppergrass (Lepidium jaredii ssp. album), mud nama (Nama stenocarpa), and California alkali grass (Puccinellia simplex). There are CNDDB records for 6 of these species within the 9 -quad query; there is no record for vernal barley.

The project site is within the current college campus footprint, which was historically disturbed by agricultural practices. None of the sensitive-plant species were observed during the survey, although the survey was not conducted during the blooming periods of any of the species. The project site currently consists of non-native Bermuda grass lawn and non-native grassland, both of which are routinely maintained and would not support any of the specialstatus species listed above. The non-native grassland in the Survey Area buffer west of the project is not routinely maintained and could potentially support brittlescale, recurved larkspur, vernal barley, Panoche peppergrass, and California alkali grass; it does not provide suitable habitat for alkali sink goldfields or mud nama. However, all project activities will be restricted to previously disturbed and routinely maintained areas that would not support these species. Thus, no protective measures for special-status plant species are warranted.

## Sensitive Wildlife Species

Based on the database queries there were 22 special-status wildlife species that were identified as having a potential to occur within the subject quadrangle and eight surrounding quadrangles. Nineteen of these species were eliminated from consideration due to the lack of suitable habitat. California red-legged frog (Rana draytonii), delta smelt (Hypomesus transpacificus), giant garter snake (Thamnophis gigas), western pond turtle (Emys marmorata), vernal pool fairy shrimp (Branchinecta lynchi), vernal pool tadpole shrimp (Lepidurus packardi), western ridged mussel (Gonidea angulata), and western spadefoot (Spea hammondii) are dependent upon water bodies and/or vernal pools, which are not present within the Survey Area. There were no CNDDB records for California red-legged frog, delta smelt, vernal pool fairy shrimp, or vernal pool tadpole shrimp in the 9-quad database query. Hoary bat (Lasiurus cinereus) roosts in dense foliage of medium to large trees, typically in forests, which were not present on or near the project. There are no elderberry shrubs (Sambucussp.) in the Survey Area so valley elderberry longhorn beetle (Desmocerus californicus dimorphus) would not be present. San Joaquin tiger beetle (Cicindela tranquebarica joaquinensis) is highly associated with sandy soils, which are not present in the Survey Area. There is no suitable nesting or foraging habitat for black-crowned night heron (Nycticorax nycticorax), tricolored blackbird (Agelaius tricolor), western snowy plover (Charadrius alexandrinus nivosus), or yellow-headed blackbird (Xanthocephalus xanthocephalus), which require wetlands, marshes, dry lakes, or sandy beaches. There are no burrows suitable for blunt-nosed leopard lizard (Gambelia sila) or California glossy snake (Arizona elegans occidentalis) and the non-native grassland habitat in the Survey Area is only marginally acceptable for these species. No kangaroo rat burrows were observed during the survey and the non-native grassland habitat is only marginally acceptable for Fresno kangaroo rat (Dipodomys nitratoides exilis) and Tipton kangaroo rat (D. n. nitratoides). American badger ( Taxidea taxus) did not result from the 9-quad queries and is now a very uncommon species to encounter in agricultural and residential areas of the California Central Valley; there is no suitable habitat for the species in the project area.

The remaining three species resulting from the database queries have the potential to occur within the project site and vicinity: burrowing owl (Athene cunicularia), Swainson's hawk (Buteo swainsonsi), and San Joaquin kit fox (Vulpes macrotis mutica). Nesting birds
protected by the federal Migratory Bird Treaty Act (MBTA) may also be present during the breeding season.

## San Joaquin Kit Fox

San Joaquin kit fox, a federally Endangered and State Threatened species, has potential to occur in the habitat surrounding the project, but is unlikely to be present within the project footprint. The nearest CNDDB record for the species is from 2002 and approximately 2.1 miles northwest of the project, documenting one San Joaquin kit fox that was observed in a fallow agricultural field during a spotlighting effort (EONDX 66434). The non-native grassland present in the Survey Area buffer provides moderate quality habitat, although there were very few small mammal burrows and the natural prey base is likely limited. However, San Joaquin kit foxes are known to adapt well to urban and residential areas and scavenge anthropogenic foods, which may be available at the college campus. No natural kit fox dens or any sign of the species were observed during the survey. Some of the modular buildings in the southeast corner of the Survey Area buffer have gaps underneath them and kit foxes could potentially den under these buildings. Multiple open-ended PVC pipes were found in the buffer which could provide temporary shelter to kit foxes.

San Joaquin kit foxes are known to be in the region and to adapt well to human presence, so the species could be present on or near the project as a transient or become an established resident at any time. Because the project supports only marginal habitat and is a small area, development of the project area would not result in a significant loss of habitat for the species. If the species were to be present during construction activities individual San Joaquin kit foxes could be injured or killed, or normal reproductive or foraging behaviors could be affected.

## Swainson's Hawk

Swainson's hawk (Buteo swainsoni) is a State Threatened species and has potential to occur in the habitat around the project, but it unlikely to be present within the project footprint. Swainson's hawks forage in agricultural fields, shrublands, and grasslands, and typically nest in scattered trees or small groves. The project is surrounding by suitable foraging habitat, but the trees present on the college campus provide only marginal nesting habitat. No suitable nests were observed on the project site or surrounding area. The nearest CNDDB occurrence is 4.6 miles northwest of the project, where one or a pair of Swainson's hawks was exhibiting breeding behavior in March 2016 (EONDX 115241).

The project footprint contains very marginal habitat for Swainson's hawk and there is a limited prey base for the species in the Survey Area. The planted trees at the college campus provide marginal nesting habitat. No trees will be removed as a result of the project. Because the project supports only marginal foraging habitat and is a small area, development of the project area would not result in a significant loss of habitat for the species. Swainson's hawk is unlikely to be nesting on the college campus, and there are no suitable nesting trees within 0.5 miles of the campus. However, if the species were to be nesting within 0.5 miles of the
project during construction activities, normal reproductive or foraging behaviors could be affected.

## Burrowing Owl

Burrowing owl (Athene cunicularia), a CDFW Species of Special Concern, has a very low potential to occur within the project, but may be found in the surrounding habitat. The nearest CNDDB record is approximately 4.7 miles southwest of the project, where a nesting burrowing owl was observed at the Lemoore Naval Air Station when routine surveys were conducted in 2000. This species is unlikely to occur within the project area but may be found in the surrounding habitat. Burrowing owls could potentially occupy the gaps beneath modular homes

Because the project supports only marginal habitat for burrowing owl and is a small area, development of the project area would not result in a significant loss of habitat for the species. If the species were to be present during construction activities individual burrowing owls could be injured or killed, or normal reproductive or foraging behaviors could be affected.

## Nesting Migratory Birds

Migratory bird species are protected under the federal MBTA. No active or inactive bird nests were observed during the survey, which was conducted outside of the typical avian breeding season (February 1 - September 30). The project and surrounding vicinity provide suitable nesting habitat for a variety of bird species which may nest in tree branches and cavities, shrubs, man-made structures, and directly on the ground. If nesting migratory birds are in the vicinity of the project during construction activities, individual birds could be injured or killed, or normal reproductive or foraging behaviors could be affected.

## Conclusion

The project footprint occurs within the existing West Hills College Lemoore campus, which has been repeatedly disturbed and built upon since the college campus was built in 1981. The project and surrounding areas support mainly non-native grasses and other ruderal or ornamental species.

No special-status plant or wildlife species or their sign were observed during the survey.
It is very unlikely that any special-status plant species occur in the project area or in the vicinity due to historic agricultural development and the current vegetation maintenance regimen. No minimization, avoidance, or mitigation measures related to special status plants is warranted.

There is the potential for some special-status or protected wildlife species to be impacted by project activities. Mitigation Measures MM BIO-1 through MM BIO-8, as provided below, would protect, avoid, and minimize impacts to special-status wildlife species. When
implemented, these measures would reduce impacts to these species to levels that are less than significant.

Through implementation of the mitigation measures listed below, impacts of the proposed project would not have a substantial adverse effect, either directly or through habitat modifications, on any species identified as a candidate, sensitive, or special status species in local or regional plans, policies, or regulations, or by the California Department of Fish and Wildlife or the U.S. Fish and Wildlife Service. Therefore, the project will have a less-thansignificant impact with incorporation of mitigation measures.

## Mitigation Measure(s)

MM BIO-1: Prior to ground disturbing activities, a qualified wildlife biologist shall conduct a biological clearance survey between 14 and 30 days prior to the onset of construction.

The clearance survey shall include walking transects to identify presence of San Joaquin kit fox, Swainson's hawk, and burrowing owl and any other special-status species and their sign. The pre-construction survey shall be walked by no greater than 30 -foot transects for 100 percent coverage of the project and a 250 -foot buffer, where feasible. If no evidence of special-status species is detected, no further action is required but measures BIO-4 through BIO-6 and BIO-8 shall be implemented.

MM BIO-2: The following avoidance and minimization measures shall be implemented during all phases of the project to reduce the potential for impact from the project. They are modified from the U.S. Fish and Wildlife Service Standardized Recommendations for Protection of the Endangered SJKF Prior to or During Ground Disturbance (USFWS 2011, Appendix F).
a. All food-related trash items such as wrappers, cans, bottles, and food scraps shall be disposed of in securely closed containers. All food-related trash items such as wrappers, cans, bottles, and food scraps shall be disposed of in securely closed containers and removed at least once a week from the construction or project site.
b. Construction-related vehicle traffic shall be restricted to established roads and predetermined ingress and egress corridors, staging, and parking areas. Vehicle speeds shall not exceed 20 miles per hour ( mph ) within the project site.
c. To prevent inadvertent entrapment of kit fox or other animals during construction, the contractor shall cover all excavated, steep-walled holes or trenches more than two feet deep at the close of each workday with plywood or similar materials. If holes or trenches cannot be covered, one or more escape ramps constructed of earthen fill or wooden planks shall be installed in the trench. Before such holes or trenches are filled, the contractor shall thoroughly inspect them for entrapped animals. All construction-related pipes, culverts, or similar structures with a diameter of four inches or greater that are stored on the project site shall be thoroughly inspected for wildlife before the pipe is subsequently buried, capped, or otherwise used or moved in anyway. If at any time an entrapped or injured kit fox is discovered, work in the immediate area shall be temporarily halted and USFWS and CDFW shall be consulted.
d. Kit foxes are attracted to den-like structures such as pipes and may enter stored pipes and become trapped or injured. All construction pipes, culverts, or similar structures with a diameter of four inches or greater that are stored at a construction site for one or more overnight periods shall be thoroughly inspected for kit foxes before the pipe is subsequently buried, capped, or otherwise used or moved in any way. If a kit fox is discovered inside a pipe, that section of pipe shall not be moved until the USFWS and CDFW have been consulted. If necessary, and under the direct supervision of the biologist, the pipe may be moved only once to remove it from the path of construction activity, until the fox has escaped.
e. No pets, such as dogs or cats, shall be permitted on the project sites to prevent harassment, mortality of kit foxes, or destruction of dens.
f. Use of anti-coagulant rodenticides and herbicides in project sites shall be restricted. This is necessary to prevent primary or secondary poisoning of kit foxes and the depletion of prey populations on which they depend. All uses of such compounds shall observe label and other restrictions mandated by the U.S. Environmental Protection Agency, California Department of Food and Agriculture, and other State and Federal legislation, as well as additional project-related restrictions deemed necessary by the USFWS and CDFW. If rodent control must be conducted, zinc phosphide shall be used because of the proven lower risk to kit foxes.
g. A representative shall be appointed by the project proponent who will be the contact source for any employee or contractor who might inadvertently kill or injure a kit fox or who finds a dead, injured or entrapped kit fox. The representative shall be identified during the employee education program and their name and telephone number shall be provided to the USFWS.
h. The Sacramento Fish and Wildlife Office of USFWS and CDFW shall be notified in writing within three working days of the accidental death or injury to a SJKF during project-related activities. Notification must include the date, time, and location of the incident or of the finding of a dead or injured animal and any other pertinent information. The USFWS contact is the Chief of the Division of Endangered Species, at the addresses and telephone numbers below. The CDFW contact can be reached at (559) 243-4014 and R4CESA@wildlifeca.gov.
i. All sightings of the SJKF shall be reported to the California Natural Diversity Database (CNDDB). A copy of the reporting form and a topographic map clearly marked with the location of where the kit fox was observed shall also be provided to the Service at the address below.
j. Any project-related information required by the USFWS or questions concerning the above conditions, or their implementation may be directed in writing to the U.S. Fish and Wildlife Service at: Endangered Species Division, 2800 Cottage Way, Suite W 2605, Sacramento, California 95825-1846, phone: (916) 414-6620 or (916) 4146600.
k. New sightings of SJKF should be reported to the CNDDB.

MM BIO-3: Within 14 days prior to the start of project ground-disturbing activities, a preactivity survey with a 500 -foot buffer shall be conducted by a qualified biologist knowledgeable in the identification of these species and approved by the CDFW. If
dens/burrows that could support any of these species are discovered during the pre-activity survey conducted under MM BIO-1, the avoidance buffers outlined below should be established. No work would occur within these buffers unless the biologist approves and monitors the activity.

Burrowing Owl (active burrows)

- Non-breeding season: September 1 - January 31-160 feet
- Breeding season: February 1 - August 31-250 feet

San Joaquin Kit Fox

- Potential or Atypical den - 50 feet
- Known den - 100 feet
- Natal or pupping den - 500 feet, unless otherwise specified by CDFW

MM BIO-4: If all project activities are completed outside of the Swainson's hawk nesting season (February 15 through August 31), this mitigation measure may be disregarded.

Nesting surveys for the Swainson's hawks shall be conducted in accordance with the protocol outlined in the Recommended Timing and Methodology for Swainson's Hawk Nesting Surveys in California's Central Valley (CDFG 2000). If potential Swainson's hawk nests or nesting substrates are located within 0.5 miles of the project site, then those nests or substrates must be monitored for activity on a routine and repeating basis throughout the breeding season, or until Swainson's hawks or other raptor species are verified to be using them. The protocol recommends that the following visits be made to each nest or nesting site: one visit during January 1-March 20 to identify potential nest sites, three visits during March 20-April 5, three visits during April 5-April 20, and three visits during June 10-July 30. A fewer number of visits may be permissible if deemed adequate by the City after consultation with a qualified biologist. To meet the minimum level of protection for the species, surveys shall be completed for at least the two survey periods immediately prior to project-related ground disturbance activities. If Swainson's hawks are not found to nest within the survey area, then no further action is warranted.

MM BIO-5: If an active Swainson's hawk nest is discovered at any time within 0.5 miles of active construction, a qualified biologist shall complete an assessment of the potential for current construction activities to impact the nest. The assessment will consider the type of construction activities, the location of construction relative to the nest, the visibility of construction activities from the nest location, and other existing disturbances in the area that are not related to construction activities of this project. Based on this assessment, the biologist shall determine if construction activities can proceed and the level of nest monitoring required. Construction activities shall not occur within 500 feet of an active nest but depending upon conditions at the site this distance may be reduced. Fulltime monitoring to evaluate the effects of construction activities on nesting Swainson's hawks may be required. The qualified biologist shall have the authority to stop work if it is determined that project construction is disturbing the nest. These buffers may need to increase depending on
the sensitivity of the nest location, the sensitivity of the nesting Swainson's hawk to disturbances, and at the discretion of the qualified biologist.

MM BIO-6: If construction is planned outside the nesting period for raptors (other than burrowing owl) and migratory birds (February 15 to August 31), no mitigation shall be required. If construction is planned during the nesting season for migratory birds and raptors, a preconstruction survey to identify active bird nests shall be conducted by a qualified biologist to evaluate the site and a 250 -foot buffer for migratory birds and a $500-$ foot buffer for raptors. If nesting birds are identified during the survey, active raptor nests shall be avoided by 500 feet and all other migratory bird nests shall be avoided by 250 feet. Avoidance buffers may be reduced if a qualified on-site monitor determines that encroachment into the buffer area is not affecting nest building, the rearing of young, or otherwise affecting the breeding behaviors of the resident birds. Because nesting birds can establish new nests or produce a second or even third clutch at any time during the nesting season, nesting bird surveys shall be repeated every 30 days as construction activities are occurring throughout the nesting season.

No construction or earth-moving activity shall occur within a non-disturbance buffer until it is determined by a qualified biologist that the young have fledged (left the nest) and have attained sufficient flight skills to avoid project construction areas. Once the migratory birds or raptors have completed nesting and young have fledged, disturbance buffers will no longer be needed and may be removed, and monitoring may cease.

MM BIO-7: A qualified biologist shall conduct a pre-construction survey on the project site and within 500 feet of its perimeter, where feasible, to identify the presence of the western burrowing owl. The survey shall be conducted between 14 and 30 days prior to the start of construction activities. If any burrowing owl burrows are observed during the preconstruction survey, avoidance measures shall be consistent with those included in the CDFW Staff Report on Burrowing Owl Mitigation (CDFG 2012). If occupied burrowing owl burrows are observed outside of the breeding season (September 1 through January 31) and within 250 feet of proposed construction activities, a passive relocation effort may be instituted in accordance with the guidelines established by the California Burrowing 0wl Consortium (1993) and the California Department of Fish and Wildlife (2012). During the breeding season (February 1 through August 31), a 500-foot (minimum) buffer zone shall be maintained unless a qualified biologist verifies through noninvasive methods that either the birds have not begun egg laying and incubation or that juveniles from the occupied burrows are foraging independently and are capable of independent survival.

In addition, impacts to occupied burrowing owl burrows shall be avoided in accordance with the following table unless a qualified biologist approved by CDFW verifies through noninvasive methods that either: 1) the birds have not begun egg laying and incubation; or 2) that juveniles from the occupied burrows are foraging independently and are capable of independent survival.

| Location | Time of Year | Level of Disturbance |  |  |
| :--- | :--- | :--- | :--- | :--- |
|  |  | Low | Med | High |
| Nesting sites | April 1-Aug 15 | $200 \mathrm{~m}^{*}$ | 500 m | 500 m |
| Nesting sites | Aug 16-Oct 15 | 200 m | 200 m | 500 m |
| Nesting sites | Oct 16-Mar 31 | 50 m | 100 m | 500 m |

MM BIO-8: Prior to ground disturbance activities, or within one week of being deployed at the project site for newly hired workers, all construction workers at the project site shall attend a Construction Worker Environmental Awareness Training and Education Program, developed and presented by a qualified biologist.

The Construction Worker Environmental Awareness Training and Education Program shall be presented by the biologist and shall include information on the life history wildlife and plant species that may be encountered during construction activities, their legal protections, the definition of "take" under the Endangered Species Act, measures the project operator is implementing to protect the species, reporting requirements, specific measures that each worker must employ to avoid take of the species, and penalties for violation of the Act. Identification and information regarding special-status or other sensitive species with the potential to occur on the project site shall also be provided to construction personnel. The program shall include:

- An acknowledgement form signed by each worker indicating that environmental training has been completed.
- A copy of the training transcript and/or training video/CD, as well as a list of the names of all personnel who attended the training and copies of the signed acknowledgement forms shall be maintain on site for the duration of construction activities.


## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.4b - Would the project have a substantial adverse effect on any riparian habitat or other sensitive natural community identified in local or regional plans, policies, regulations, or by the California Department of Fish and Wildlife or U.S. Fish and Wildlife Service?

There is one CNDDB occurrence of Valley Sink Scrub, approximately 3.2 miles south of the project (EONDX 16344). This sensitive natural community or any other sensitive natural community was not observed during the survey. The project is not located within a river or an area that encompasses a river or potential floodplain and does not contain nor is near any riparian habitat. The proposed project would not have a substantial adverse effect on any riparian habitat or other sensitive natural community. Therefore, the project's impacts would be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.4c - Would the project have a substantial adverse effect on State or federally protected wetlands (including, but not limited to, marsh, vernal pool, coastal, etc.) through direct removal, filling, hydrological interruption, or other means?

The United States Army Corps of Engineers (USACE) has regulatory authority over the Clean Water Act (CWA), as provided for by the EPA. The USACE has established specific criteria for the determination of wetlands based upon the presence of wetland hydrology, hydric soils, and hydrophilic vegetation. There are no federally protected wetlands or vernal pools that occur within the project.

Wetlands, streams, reservoirs, sloughs, and ponds typically meet the criteria for federal jurisdiction under Section 404 of the CWA and state jurisdiction under the Porter-Cologne Water Quality Control Act. Streams and ponds typically meet the criteria for State jurisdiction under Section 1602 of the California Fish and Game Code. There is a freshwater pond 0.3 miles southwest of the project area, but it will not be impacted by project activities.

Although there is a historic water feature identified as a "riverine" by the National Wetland Inventory (see Figure 3.4.4-1), that feature no longer exists on the project site. The development of the campus has eliminated it. As noted during the biological survey, there are no features on or near the project that would meet the criteria for either federal or State jurisdiction. Accordingly, there are no wetlands or Waters of the U.S. occurring on the project site. There would be no impact to federally protected wetlands or waterways as a result of the proposed project. Therefore, the project would have no impact.

## Mitigation Measure(s)

No mitigation is required.

## LEVEL OF SIGNIFICANCE

There would be no impact.
Impact \#3.4.4d - Would the project interfere substantially with the movement of any native resident or migratory fish or wildlife species, or with established native resident or migratory wildlife corridors, or impede the use of native wildlife nursery sites?

Wildlife migratory corridors are described as a narrow stretch of land that connects two open pieces of habitat that would otherwise be unconnected. These routes provide shelter and sufficient food supplies to support wildlife species during migration. Movement
corridors generally consist of riparian, woodlands, or forested habitats that span contiguous acres of undisturbed habitat and are important elements of resident species' home ranges.

The project falls within the Pacific Flyway, a significant migratory route encompassing the west coast of North America, but the project represents a very small land acreage within this territory and does not support any significant migratory stopover habitat. The proposed project and surrounding area does not occur within a known terrestrial migration route, significant wildlife corridor, or linkage area as identified by the Essential Habitat Connectivity Project (Spencer, W.D., et al, 2010). The survey conducted for the project did not provide evidence of a wildlife nursery or important migratory habitat being present on the project site. Migratory birds and raptors could use habitat on and near the project for foraging and/or as stopover sites during migrations or movement between local areas.

The project will not restrict, eliminate, or significantly alter a wildlife movement corridor, wildlife core area, or Essential Habitat Connectivity area, either during construction or after the project has been constructed. Project construction will not substantially interfere with wildlife movements or reduce breeding opportunities.

The proposed project would not interfere with the movement of any native resident or migratory fish or wildlife species or with established native resident or migratory wildlife corridors or impede the use of native wildlife nursery sites. Therefore, the project's impacts would be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.4e - Would the Project conflict with any local policies or ordinances protecting biological resources, such as a tree preservation policy or ordinance?

There are no adopted local policies or ordinances protecting biological that would apply to this project site. Therefore, implementation of the proposed project would have no conflict related to an adopted local policies or ordinances protecting biological.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.

Impact \#3.4.4f - Would the project conflict with the provisions of an adopted habitat conservation plan, natural community conservation plan, or other approved local, regional, or State habitat conservation plan?

The project is not located within any Natural Community Conservation Plan or any other local, regional, or State Conservation Plan. With mitigation, the proposed project would not conflict with the provisions of an adopted Habitat Conservation Plan, Natural Community Conservation Plan, or other approved local, regional, or State Habitat Conservation Plan.

Mitigation Measure(s)
No mitigation is required.

## Level of Significance

Impacts would be less than significant.


|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.5 - Cultural Resources

Would the project:
a. Cause a substantial adverse change in the
significance of a historical resource as defined in CEQA Guidelines Section 15064.5?
b. Cause a substantial adverse change in the
significance of an archaeological resource pursuant to CEQA Guidelines Section 15064.5?
c. Disturb any human remains, including those interred outside of formal cemeteries?

The analysis below is based on a Cultural Resources Technical Memorandum prepared for the project ( $\mathrm{QK}, 2020$ ) and found in Appendix B of this document.

Impact \#3.4.5a - Would the project cause a substantial adverse change in the significance of a historical resource as defined in CEQA Guidelines Section 15064.5?

The City of Lemoore 2030 General Plan states there are currently no buildings or structures listed in the National Register of Historic Places or as California Historic Landmarks. However, there are 37 sites listed as having local historic significance located within the downtown district (City of Lemoore , 2008).

A records search was conducted at the Southern San Joaquin Valley Information Center (SSJVIC) at California State University, Bakersfield to identify previously recorded resources and prior surveys within the project area and surrounding half-mile area. The records search covered an area within one-half mile of the project and included a review of the National Register of Historic Places, California Points of Historical Interest, California Registry of Historic Resources, California Historical Landmarks, California State Historic Resources Inventory, and a review of cultural resource reports on file.
The records search indicated that the subject property had never been surveyed for cultural resources and it is not known if any exist there. Only one cultural resource, a segment of the historic route of the Southern Pacific Railroad (now the San Joaquin Valley Railroad) (P-16000122), has been identified within a half mile of the proposed project. However, the project will not impact this resource.

Based on the results of cultural records search findings and the lack of archaeological resources previously identified within a half-mile radius of the proposed project, the potential to encounter subsurface cultural resources is minimal. Additionally, the project
construction would be conducted within the developed and previously disturbed roadways and road easements. The potential to uncover subsurface historical or archaeological deposits is would be considered unlikely.

However, there is still a possibility that historical or archaeological materials may be exposed during construction. Grading and trenching, as well as other ground-disturbing actions have the potential to damage or destroy these previously unidentified and potentially significant cultural resources within the project area, including historical or archaeological resources. Disturbance of any deposits that have the potential to provide significant cultural data would be considered a significant impact. To reduce the potential impacts of the project on cultural resources, the following measures are recommended. With implementation of CUL-1, impacts under cultural resources would be less than significant.

## Mitigation Measure(s)

MM CUL-1: If prehistoric or historic-era cultural materials are encountered during construction activities, all work in the immediate vicinity of the find shall halt until a qualified archaeologist can evaluate the find and make recommendations. Cultural resource materials may include prehistoric resources such as flaked and ground stone tools and debris, shell, bone, ceramics, and fire-affected rock as well as historic resources such as glass, metal, wood, brick, or structural remnants. If the qualified archaeologist determines that the discovery represents a potentially significant cultural resource, additional investigations may be required to mitigate adverse impacts from project implementation. These additional studies may include avoidance, testing, and evaluation or data recovery excavation. Implementation of the mitigation measure below would ensure that the proposed project would not cause a substantial adverse change in the significance of a historical resource.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.5b - Would the project cause a substantial adverse change in the significance of an archaeological resource pursuant to CEQA Guidelines Section 15064.5?

See discussion of Impact \#3.4.5a, above.

## Mitigation Measure(s)

Implement MM CUL-1.
Level of Significance
Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.5c - Would the project disturb any human remains, including those interred outside of formal cemeteries?

Human remains are not known to exist within the project area. However, construction would involve earth-disturbing activities, and it is still possible that human remains may be discovered, possibly in association with archaeological sites. MM CUL-2 has been included in the unlikely event that human remains are found during ground-disturbing activities. Impacts would be less than significant with implementation of mitigation.

## Mitigation Measure(s)

MM CUL-2: If human remains are discovered during construction or operational activities, further excavation or disturbance shall be prohibited pursuant to Section 7050.5 of the California Health and Safety Code. The specific protocol, guidelines, and channels of communication outlined by the Native American Heritage Commission, in accordance with Section 7050.5 of the Health and Safety Code, Section 5097.98 of the Public Resources Code (Chapter 1492, Statutes of 1982, Senate Bill 297), and Senate Bill 447 (Chapter 44, Statutes of 1987), shall be followed. Section 7050.5(c) shall guide the potential Native American involvement, in the event of discovery of human remains, at the direction of the county coroner.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.6-Energy

Would the project:
a. Result in a potentially significant environmental impact due to wasteful, inefficient, or unnecessary consumption of energy resources, during project construction or operation?
b. Conflict with or obstruct a State or local plan for renewable energy or energy efficiency?

## Discussion

Impact \#3.4.6a - Would the project result in a potentially significant environmental impact due to wasteful, inefficient, or unnecessary consumption of energy resources, during project construction or operation?

## Construction

Energy demand during the construction phase would result from the transportation of materials, construction equipment, and construction worker vehicle trips. Construction equipment includes a crane, bulldozer, grader, bob cat, trencher, cement trucks, water trucks, trash trucks, equipment delivery trucks, and company work vehicles. The project would comply with the SJVAPCD requirements regarding the limitation of vehicle idling, and the use of fuel-efficient vehicles and equipment, to the extent feasible. Energy saving strategies will be implemented where possible to further reduce the project's energy consumption, during the construction phase. Strategies being implemented include those recommended by the California Air Resources Board (CARB) that may reduce both the project's energy consumption, including diesel anti-idling measures, light-duty vehicle technology, usage of alternative fuels such as biodiesel blends and ethanol, and heavy-duty vehicle design measures to reduce energy consumption.

The project will not use natural gas during the construction phase. Compliance with standard regional and local regulations, the project would minimize fuel consumption during construction. By complying with standard regional and local regulations, the project would minimize fuel consumption during construction. Construction related fuel consumption is not expected to result in inefficient, wasteful, or unnecessary energy use. Thus, constructionrelated fuel consumption at the project would not result in inefficient, wasteful, or unnecessary energy use.

## Post-Construction

With the project, it is expected that the annual electricity usage for the campus would increase by approximately six percent. The project will comply with all applicable standards and building codes included in the 2019 California Green Building Standards Code. Therefore, the project would have a less-than-significant impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.6b - Would the project conflict with or obstruct a State or local plan for renewable energy or energy efficiency?

See Impact \#3.4.6a, above.
The project must comply with Title 24 , Chapter 4 of the California Green Building Standards Code for residential development and Part 6, of the California Energy Code (CEC) the California Code of Regulations (CCR), Title 20 with adoptions of the California Energy Commission (California Building Standards Commission, 2019). It is the District's intention to exceed Title 24 requirements for energy efficiency, using the most effective equipment available to minimize energy consumption.

Energy saving strategies will be implemented where feasible to reduce the project's energy consumption during the construction and post-construction phases. Strategies being implemented include those recommended by the California Air Resources Board (CARB) that may reduce both the project's construction energy consumption, including diesel antiidling measures, light-duty vehicle technology, usage of alternative fuels such as biodiesel blends and ethanol, and heavy-duty vehicle design measures to reduce energy consumption. The continued use of solar-generated energy along with the energy efficiency components outlined above will assist California in meeting greenhouse gas (GHG) emissions reduction goal by 2020 and 2030 as required by the California Global Warming Solutions Act (AB 32), as amended by SB 32 in 2016.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.

### 3.4.7-Geology and Soils

Would the project:
a. Directly or indirectly cause potential substantial adverse effects, including the risk of loss, injury, or death involving:
i. Rupture of a known earthquake fault, as delineated on the most recent AlquistPriolo Earthquake Fault Zoning Map issued by the State Geologist for the area or based on other substantial evidence of a known fault? Refer to Division of Mines and Geology Special Publication 42.
ii. Strong seismic ground shaking?
iii. Seismic-related ground failure, including Liquefaction?
iv. Landslides?
b. Result in substantial soil erosion or the loss of topsoil?
c. Be located on a geologic unit or soil that is unstable, or that would become unstable as a result of the project, and potentially result in on or offsite landslide, lateral spreading, subsidence, liquefaction, or collapse?
d. Be located on expansive soil, as defined in Table 18-1-B of the Uniform Building Code (1994), creating substantial risks to life or property?
e. Have soils incapable of adequately supporting the use of septic tanks or alternative wastewater disposal systems in areas where sewers are not available for the disposal of wastewater?
f. Directly or indirectly destroy a unique paleontological resource or site or unique geologic feature?

## Discussion

The analysis below is based on the Geotechnical Engineering Investigation completed for the student center on the campus adjacent to the project site by BSK Associates (BSK Associates, 2011), found in Appendix C in this document.

Impact \#3.4.7a(i) - Would the project expose people or structures to potential substantial adverse effects, including the risk of loss, injury, or death involving rupture of a known earthquake fault, as delineated on the most recent Alquist-Priolo Earthquake Fault Zoning Map issued by the State Geologist for the area or based on other substantial evidence of a known fault?

According to the City of Lemoore 2030 General Plan, there are no known major fault systems within Lemoore (City of Lemoore, 2008). The project site is not located within an AlquistPriolo Earthquake Fault Zone and the closest Fault-Rupture Hazard Zone is associated with the Nunez Fault located approximately 35 miles west of the campus (BSK Associates, 2011). By adhering to the most recent California Building Standard Codes and other applicable local codes, the project will have a less-than-significant impact related to earthquakes and seismic events.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.7a(ii) - Would the project expose people or structures to potential substantial adverse effects, including the risk of loss, injury, or death involving strong seismic ground shaking?

See response to Impact \#3.4.7a.
Secondary hazards from earthquakes include ground shaking/rupture, seiche, landslides, liquefaction, and subsidence. Since there are no known faults within the immediate area, ground shaking/rupture from surface faulting should not be a potential problem. Seiche and landslides are not potential hazards in the area. Lastly, deep subsidence problems may be low to moderate according to the conclusions of the Five County Seismic Safety Element. However, the site is not located in an area susceptible to subsidence due to petroleum or groundwater withdrawal (BSK Associates, 2011).

According to the Seismic Safety Map contained within the Health and Safety Element of the 2035 Kings County General Plan (Figure HS-2, page HS-10), the project site is located within an area designated as Zone V1 or Valley Zone 1, which is identified as the area of least expected seismic shaking by the Kings County Seismic Zone Description in the 2035 General Plan (County of Kings, 2010). The potential for ground shaking is discussed in terms of the
percent probability of exceeding peak ground acceleration (\% g) in the next 50 years (County of Kings, 2010).

The project is required to design the new facilities and associated infrastructure to withstand substantial ground shaking in accordance with all applicable State law and applicable codes included in the CBC Title 24 for earthquake construction standards and building standards code including those relating to soil characteristics (California Building Standards Commission, 2019). Based on previous projects, a final Geotechnical Report prepared by a licensed engineer to determine the preparation of the project site prior to construction and design the building to withstand seismic events The project will adhere to all applicable local and State regulations to reduce any potentially significant impacts to structures resulting from strong seismic ground shaking at the project site. With implementation of MM GEO-1 and all applicable local and State codes, project impacts would be less than significant with mitigation.

## Mitigation Measure(s)

MM GEO-1: Prior to the ground disturbance activities, a qualified engineer shall be obtained. The project engineer, structural engineer, civil engineer, general contractor, the earthwork contractor shall meet to discuss the grading plan and grading requirements as outlined in the final Geotechnical Report.

## Level of Significance

Impacts would be less than significant with mitigation.
Impact \#3.4.7a(iii) - Would the project expose people or structures to potential substantial adverse effects, including the risk of loss, injury, or death involving seismic-related ground failure, including liquefaction?

See discussion of Impact \#3.4.7a(i) and a(ii), above.
The potential magnitude/geographic extent of expansive liquefaction erosion was deemed 'negligible' and its significance 'low' throughout the City (City of Lemoore, 2012). Liquefaction is possible in local areas during a strong earthquake or other seismic ground shaking, where unconsolidated sediments coincide with a high-water table.

Structures constructed as part of the project would be required by State law to be constructed in accordance with all applicable IBC and CBC earthquake construction standards, including those relating to soil characteristics. Adherence to all applicable regulations would avoid any potential impacts to structures resulting from liquefaction at the project site.

Test boring indicated that free groundwater was encountered at depths of approximately seven feet bgs during subsurface investigation. The analysis conducted to determine safety against liquefaction determined the site to have a value of less than 1.0 , which is acceptable
for most structures and it was determined the overall potential for liquefaction to occur at the site is low (BSK Associates, 2011).

Structures constructed as part of the project would be required by State law to be constructed in accordance with all applicable IBC CBC, Title 24 construction standards. Adherence to all applicable regulations and implementation of MM GEO-1 would reduce potential impacts to structures resulting from seismically related ground failure to less-thansignificant levels.

## Mitigation Measure(s)

Implementation of MM GEO-1.

## LEVEL OF SIGNIFICANCE

Impacts would be less than significant with mitigation.
Impact \#3.4.6a(iv) - Would the project expose people or structures to potential substantial adverse effects, including the risk of loss, injury, or death involving landslides?

The site and surrounding areas are essentially flat. As such, there is no potential for rock fall and landslides to impact the project in the event of a major earthquake, as the area has no dramatic elevation changes (BSK Associates, 2011). Secondary hazards from earthquakes include ground shaking/rupture, seiche, landslides, liquefaction, and subsidence. Since there are no known faults within the immediate area, ground shaking/rupture from surface faulting should not be a potential problem. Additionally, there is not a potential for seiche and landslides. Lastly, deep subsidence problems may be low to moderate according to the conclusions of the Five County Seismic Safety Element. However, the project is not in an area susceptible to subsidence (BSK Associates, 2011).

The area surrounding the project site currently is developed. The site's topography would not change substantially as a result of project development since the site is essentially flat in nature from previous activities with no surrounding slopes and it is not considered to be prone to landslides. The project would not expose people or structures to potential substantial adverse effects from landslides. Therefore, there would be a less-than-significant impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant

Impact \#3.4.7b - Would the project result in substantial soil erosion or the loss of topsoil?
The type of soil found within the project site is Goldsberg loam. The construction of the project is not expected to subject the site to any extreme erosion problems.

Construction activities associated with the proposed project will disturb surface vegetation and soils during construction and would expose these disturbed areas to erosion by wind and water. To reduce the potential for soil erosion and loss of topsoil, the project would comply with the State Water Resources Control Board's (SWRCB) National Pollutant Discharge Elimination System (NPDES) General Permit (No. 2012-0006-DWQ) during construction. Under the NPDES, the preparation and implementation of a Stormwater Pollution Prevention Plan (SWPPP) are required for construction activities that would disturb an area of one acre or more. A SWPPP must identify potential sources of erosion or sedimentation as well as identify and implement Best Management Practices (BMPs) that ensure reduce erosion. Typical BMPs intended to control erosion include sandbags, retention basins, silt fencing, street sweeping, etc.

Mitigation Measure MM GEO-2 requires the approval of a SWPPP to comply with the NPDES General Construction Permit. The project will comply with all the grading requirements as outlined in Title 24 and Appendix J of the California Building Code (UpCodes, 2016). The project is not expected to result in substantial soil erosion or the loss of topsoil with the incorporation of Mitigation Measure MM GEO-1.

Once constructed, the project will have both impermeable surfaces as well as permeable surfaces. Impermeable surfaces would include roadways, driveways and building sites. Permeable surfaces would include any landscaped areas and open space. Overall, development of the project would not result in conditions where substantial surface soils would be exposed to wind and water erosion.

## Mitigation Measure(s)

MM GEO-2: Prior to issuing of grading or building permits, the project applicant shall submit to the City: (1) the approved Storm Water Pollution Prevention Plan (SWPPP) and (2) the Notice of Intent (NOI) to comply with the General National Pollutant Discharge Elimination System (NPDES) from the Central Valley Regional Water Quality Control Board. The requirements of the SWPPP and NPDES shall be incorporated into design specifications and construction contracts. Recommended Best Management Practices for the construction phase may include the following:

- Stockpiling and disposing of demolition debris, concrete, and soil properly;
- Protecting existing storm drain inlets and stabilizing disturbed areas;
- Implementing erosion controls;
- Properly managing construction materials; and
- Managing waste, aggressively controlling litter, and implementing sediment controls.

Evidence of the approved SWPPP shall be submitted to the Lead Agency.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.7c - Would the project be located on a geologic unit or soil that is unstable, or that would become unstable as a result of the project, and potentially result in on or offsite landslide, lateral spreading, subsidence, liquefaction, or collapse?

As previously discussed, the site soils are considered stable in that there is not a potential of on or offsite landslides, lateral spreading, subsidence or collapse. As discussed in Impact \#3.4.7a(iii), the project site soils have a low overall potential for significant liquefaction to occur at the site. All structures would be subject to all IBC and CBC earthquake construction standards, including those relating to soil characteristics. In order to reduce impacts related to unstable soils, MM GEO-1 requires a registered engineering geologist or soils engineer to provide recommendations to provide sufficient specification for project structures. With implementation of MM GEO-1, impacts would be less than significant.

## Mitigation Measure(s)

Implementation of MM GEO-1.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.7d - Would the project be located on expansive soil, as defined in Table 18-1-B of the Uniform Building Code (1994), creating substantial risks to life or property?

See Impact 3.4 .7 b and c .
Expansive clay soils are subject to shrinking and swelling due to changes in moisture content over the seasons. These changes can cause damage or failure of foundations, utilities, and pavements. During periods of high moisture content, expansive soils under foundations can heave and result in structures lifting. In dry periods, the same soils can collapse and result in settlement of structures.

The subject site and soil conditions consists of silty sands, silty clays, clayey silts, and sandy silts. Based on the results of the consolidation tests, the on-site soils below two feet are considered to have a low potential for hydrocompaction. The upper five feet of the on-site soils are considered to have medium expansion potential (BSK Associates, 2011). Any recommendations based on the results of the evaluation would be performed according to standard geotechnical engineering practices and meet all local and State codes and regulations. With implementation of MM GEO-1 impacts related to expansive soils would be less than significant.

## Mitigation Measure(s)

Implementation of GEO-1.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.7e - Would the project have soils incapable of adequately supporting the use of septic tanks or alternative wastewater disposal systems in areas where sewers are not available for the disposal of wastewater?

## Refer to Section 3.4.19-Utilities and Service Systems.

The proposed project does not include the development or use of septic tanks or alternative wastewater disposal systems as the project would connect to the City's existing sewer system.

## Mitigation Measures

None are required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.7f - Would the project directly or indirectly destroy a unique paleontological resource or site or unique geologic feature?

The project does not intend to use undisturbed land; all construction will be conducted within the footprint of the existing campus. According to the Kings County General Plan EIR, there is only one site in the County considered to be sensitive for paleontological resources (Kings County, 2010b). There are no unique geological features or known fossil-bearing sediments in the vicinity of the project site. However, there remains the possibility for previously unknown, buried paleontological resources or unique geological sites to be uncovered during subsurface construction activities. Therefore, this would be a potentially significant impact. However, MM GEO-3, requires that if unknown paleontological resources are discovered during construction activities, work within a 25 -foot buffer would cease until a qualified paleontologist determined the appropriate course of action. With implementation of MM GEO-3, the project will have a less-than-significant impact.

## Mitigation Measure(s)

MM GEO-3: If any paleontological resources are encountered during ground disturbance activities, all work within 25 feet of the find shall halt until a qualified paleontologist as defined by the Society of Vertebrate Paleontology Standard Procedures for the Assessment and Mitigation of Adverse Impacts to Paleontological Resources (2010), can evaluate the find
and make recommendations regarding treatment. Paleontological resource materials may include resources such as fossils, plant impressions, or animal tracks preserved in rock. The qualified paleontologist shall contact the Natural History Museum of Los Angeles County or other appropriate facility regarding any discoveries of paleontological resources.

If the qualified paleontologist determines that the discovery represents a potentially significant paleontological resource, additional investigations and fossil recovery may be required to mitigate adverse impacts from project implementation. If avoidance is not feasible, the paleontological resources shall be evaluated for their significance. If the resources are not significant, avoidance is not necessary. If the resources are significant, they shall be avoided to ensure no adverse effects, or such effects must be mitigated. Construction in that area shall not resume until the resource appropriate measures are recommended or the materials are determined to be less than significant. If the resource is significant and fossil recovery is the identified form of treatment, then the fossil shall be deposited in an accredited and permanent scientific institution. Copies of all correspondence and reports shall be submitted to the Lead Agency.

## Level of Significance

Impacts would be less than significant. with mitigation incorporated.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.8 - Greenhouse Gas Emissions

Would the project:
a. Generate greenhouse gas emissions, either directly or indirectly, that may have a significant impact on the environment?
b. Conflict with any applicable plan, policy, or regulation adopted for the purpose of reducing the emissions of greenhouse gases?

## Discussion

The analysis in this section is based on the Small Project Analysis Level Assessment prepared for the project (Trinity Consultants, 2020), which can be found in Appendix A of this document.

There have been significant legislative and regulatory activities that directly and indirectly affect climate change and GHGs in California. The primary climate change legislation in California is AB 32, the California Global Warming Solutions Act of 2006. AB 32 focuses on reducing GHG emissions in California. GHGs, as defined under AB 32, include carbon dioxide, methane, nitrous oxide, hydrofluorocarbons, perfluorocarbons, sulfur hexafluoride, and Nitrogen trifluoride. AB 32 requires that GHGs emitted in California be reduced to 1990 levels by the year 2020. The California Air Resources Board is the State agency charged with monitoring and regulating sources of emissions of GHGs that cause global warming in order to reduce emissions of GHGs. SB 32 was signed by the Governor in 2016, which would require the State Board to ensure that statewide greenhouse gas emissions are reduced to 40 percent below the 1990 level by 2030.

Although construction of the proposed project would result in temporary emissions of GHGs, the project as a whole is not expected to generate greenhouse gas emissions, either directly or indirectly that may have a significant impact on the environment. The project GHG emissions are primarily from mobile source activities.

The SJVAPCD Small Project Analysis Level (SPAL) process established review parameters to determine whether a project qualifies as a "small project." A project that is found to be "less than" the established parameters, according to the SPAL review parameters, has "no possibility of exceeding criteria pollutant emissions thresholds."

As shown in Table 3.4.3-3, the proposed project would not exceed the established SPAL limits for an educational project. The project would construct a new 42,429-square-foot,
two-story Instructional Center, which is less than the SPAL threshold for a Junior College (2 year) of 74,400 square feet. Based on the above information, this project qualifies for a limited GHG analysis applying the SPAL guidance to determine air quality impacts.

Impact \#3.4.8a - Would the project generate greenhouse gas emissions, either directly or indirectly, that may have a significant impact on the environment?

See Impact \#3.4.6a, above.
Construction and operation of this project will result in temporary Greenhouse Gases (GHG) emissions. The project as a whole is not expected to generate GHGs either directly or indirectly that may have a significant impact on the environment. The project's greenhouse gas (GHG) emissions are primarily from mobile source activities and are shown in Table 3.4.8-1.

Table 3.4.8-1
Estimated Annual Greenhouse Gas Emissions

|  | CO2 Emissions <br> metric tons | CH4 Emissions <br> metric tons | $\mathrm{N}_{2}$ O Emissions <br> metric tons | CO2e Emissions <br> metric tons |
| :---: | :---: | :---: | :---: | :---: |
| 2024 Project | $1,298.58$ | 0.82 | 0.004 | $1,320.16$ |
| Operations | $1,928.57$ | 1.44 | 0.004 | $1,965.82$ |
| 2005 BAU |  |  |  | $32.8 \%$ |
| BAU less <br> Project <br> Emissions |  |  |  |  |

Source: (Trinity Consultants, 2020)
The SJVAPCD does not have thresholds or guidance regarding the significance of construction related emissions. Overall, the impacts to occur during the construction phase would be short-term and temporary in nature. As there are no current significance thresholds to quantify construction emissions and because construction-related impacts are considered temporary they are therefore, generally considered less than significant. In addition, construction of the proposed project would still have to comply with the SJVAPCD's regulation and requirements as discussed in the air quality section.

The project will not generate long-term emissions over the life of the project. Therefore, the project is considered less than significant for GHG emission impacts.

## Mitigation Measures

No mitigation is required.
Level of Significance
Impacts would be less than significant

Impact \#3.4.8b - Would the project conflict with any applicable plan, policy, or regulation adopted for the purpose of reducing the emissions of greenhouse gases?

See response to Impact \#3.4.8a.
The amount of $\mathrm{CO}_{2}$ that would be generated by the project is so small in relation to the California $\mathrm{CO}_{2}$ equivalent estimates for 2020 ( 596 million metric tons $\mathrm{CO}_{2} \mathrm{e}$ ) that it's not possible for the contribution of the project to be cumulatively considerable. Additionally, the project's GHG emissions are less than the 2005 business as usual emissions for the project by 645.66 metric tons $\mathrm{CO}_{2} \mathrm{e}$, which is a 32.8 percent reduction. Therefore, the project would not generate a cumulatively considerable GHG impact nor would it conflict with any applicable plan, policy or regulation adopted for the purpose of reducing the emissions of GHGs. The project will also not conflict with any elements of the California Air Resources Board's 2008 Climate Change Scoping Plan. Therefore, this potential impact is less than significant.

## Mitigation Measures

No mitigation required.

## Level of Significance

Impacts would be less than significant.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.9-Hazards and Hazardous

 MaterialsWould the project:
a. Create a significant hazard to the public or the environment through the routine transport, use, or disposal of hazardous materials?
b. Create a significant hazard to the public or the environment through reasonably foreseeable upset and accident conditions involving the release of hazardous materials into the environment?
c. Emit hazardous emissions or involve handling hazardous or acutely hazardous materials, substances, or waste within onequarter mile of an existing or proposed school?
d. Be located on a site that is included on a list of hazardous materials sites compiled pursuant to Government Code Section 65962.5 and, as a result, would it create a significant hazard to the public or the environment?
e. For a project located within an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project result in a safety hazard for people residing or working in the project area?
f. Impair implementation of, or physically interfere with, an adopted emergency response plan or emergency evacuation plan?
g. Expose people or structures, either directly or indirectly, to a significant risk of loss, injury, or death involving wildland fires??

## Discussion

Impact \#3.4.9a - Would the project create a significant hazard to the public or the environment through the routine transport, use, or disposal of hazardous materials?

The building and operation of the proposed project would not involve the transport, use, and storage of large quantities of hazardous materials. Although construction of the site would involve the transport and use of minor quantities of hazardous materials, such materials would be limited to fuels, oils, lubricants, hydraulic fluids, paints and solvents utilized at the project site for construction purposes. Moreover, use of such materials would be temporary in nature and would cease upon completion of the project. Some solid hazardous waste, such as welding materials and dried paint, may also be generated during construction. These materials would be transported to the project site during construction, and any hazardous materials that are produced as a result of the construction of the project would be collected and transported away from the site. During construction of the project, material safety data sheets for all applicable materials present at the site would be made readily available to onsite personnel. During construction activities, non-hazardous construction debris would be generated and disposed of in local landfills. Sanitary waste would be managed using portable toilets located at a reasonably accessible onsite location.

The project site is located within an existing school campus. The use of hazardous materials will be limited in quantities and duration, and if spilled, would be very localized. The proposed project would not emit hazardous emissions or involve handling hazardous or acutely hazardous materials substances. The transport use and storage of hazardous materials would be required to comply with all applicable State and federal regulations, such as requirements that spills would be cleaned immediately, and all wastes and spills control materials would be properly disposed of at approved disposal facilities.

Mitigation Measure MM GEO-2 requires the preparation of a Storm Water Pollution Prevention Plan (SWPPP), which includes a list of BMPs to be implemented on the site both during construction to minimize potential impacts from accidental spills. Compliance with the SWPPP and all local, State, and federal regulations regarding hazardous materials, impacts associated with the use or accidental spill of hazardous materials would be less than significant.

## Mitigation Measure(s)

Implementation of MM GEO-2.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.9b - Would the project create a significant hazard to the public or the environment through reasonably foreseeable upset and accident conditions involving the release of hazardous materials into the environment?

See Impact \#3.4.8a, above.
There are no active Geologic Energy Management Division (CalGEM) identified oil or gas fields in the project vicinity and there are no known existing or historical oil wells on the project site (CalGEM, 2020). As such, it is not expected that any wells would be impacted by the project.

The completed project will not create significant hazards to the public or the environment through a reasonably foreseeable upset and accident conditions involving the release of hazardous materials into the environment. Therefore, the project will have a less-than-significant impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.9c - Would the project emit hazardous emissions or involve handling hazardous or acutely hazardous materials, substances, or waste within one-quarter mile of an existing or proposed school?

The closest school is Lemoore Elementary Charter School, which is on the campus and approximately 930 feet west of the project. However, construction of the project would require the use of minimal hazardous materials and require implementation of BMPs when handling any hazardous materials, substances, or waste. Operation of the project would not emit any involve handling of any hazardous materials near the elementary school campus site. Therefore, impacts would be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.9d - Would the project be located on a site that is included on a list of hazardous materials sites compiled pursuant to Government Code Section 65962.5 and, as a result, would it create a significant hazard to the public or the environment?

An online search was conducted of Cortese List to identify locations on or near the project site. The search indicated that there are no hazardous or toxic sites in the vicinity (within one mile) of the project site (Cal EPA, 2020). Currently, there are no hazardous wastes landfill sites within Lemoore. The Kings Waste \& Recycling Authority maintains a permanent
household hazardous waste facility in the City of Hanford. Lemoore residents can make use of this facility through free household hazardous waste disposal services available at collection sites in the City. The City collects e-waste, battery, and used oil for disposal (City of Lemoore, 2008).

According to EnviroStor, there are no hazardous waste and substances sites in the vicinity of the project site. The proposed project site is not located on a site that is included on a list of hazardous materials sites compiled pursuant to Government Code Section 65962.5 and would therefore not create a significant hazard to the public or the environment.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.9e - For a project located within an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project result in a safety hazard or excessive noise for people residing or working in the project area?

There are no public airports within two miles of the project site. The Lemoore NAS runways are located approximately five miles to the south west of the project site. The closest public airport is the Hanford Municipal Airport, located approximately 13 miles east of the project. The project is not within an airport land use compatibility plan area. Therefore, the Project would not result in a safety hazard as a result of proximity to a public or private use airport and would have no impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.9f -Would the project impair implementation of, or physically interfere with, an adopted emergency response plan or emergency evacuation plan?

The Kings County Emergency Operations Plan (EOP) establishes emergency procedures and policies and identifies responsible parties for emergency response in the County, and includes the incorporated City of Lemoore (Kings County, 2015). The EOP includes policies that would prevent new development from interfering with emergency response of evacuation plans. The proposed project would not impair implementation of or physically interfere with the West Hills Community College Emergency Response Plan.

The project would also comply with the appropriate local and State requirements regarding emergency response plans and access. The proposed project would not inhibit the ability of local roadways to continue to accommodate emergency response and evacuation activities. The proposed project would not interfere with the City or the District's adopted emergency response plan; therefore, there would be no impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.9g - Would the project expose people or structures, either directly or indirectly, to a significant risk of loss, injury, or death involving wildland fires?

The proposed project site is in an unzoned area of the Kings County Fire Hazard Severity Zone Map Local Responsibility Area (LRA) (Cal Fire, 2006). The project site is not within a wildland area nor is there within the vicinity of the project site. Construction activities and the project is not expected to increase the risk of wildfires on and adjacent to the project site.

The Lemoore City Volunteer Fire Department, located approximately 2.5 miles away, would provide fire protection services to the project.

The project will comply with all applicable State and local building standards as required by local fire codes. The project would not expose people or structures to a significant risk of loss, injury, or death involving wildland fires. Therefore, there would be no impact.

## Mitigation Measure(S)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.

### 3.4.10-Hydrology and Water QUALITY

Would the project:
a. Violate any water quality standards or waste discharge requirements or otherwise substantially degrade surface water quality?
b. Substantially decrease groundwater supplies or interfere substantially with groundwater recharge such that the project may impede sustainable groundwater management of the basin?
c. Substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river or through the addition of impervious surfaces, in a manner which would:
i. Result in substantial erosion or siltation on or offsite?
ii. Substantially increase the rate of amount of surface runoff in a manner which would result flooding on or offsite?
iii. Create or contribute runoff water which would exceed the capacity of existing or planned stormwater drainage systems or provide substantial additional sources of polluted runoff?
iv. Impede or redirect flood flows?
d. In flood hazard, tsunami, or seiche zones, risk release of pollutants due to project inundation?
e Conflict with or obstruct implementation of a water quality control plan or sustainable groundwater management plan?

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

## Less than <br> Significant

with Less-than-
Mitigation Significant Incorporated Impact

No
Impact

## Discussion

Impact \#3.4.10a - Would the project violate any water quality standards or waste discharge requirements or otherwise substantially degrade surface or groundwater quality?

Project construction would cause ground disturbance that could result in soil erosion or siltation and subsequent water quality degradation offsite, which is a potentially significant impact. Construction-related activities would also involve the use of materials such as vehicle fuels, lubricating fluids, solvents, and other materials that could result in polluted runoff, which is also a potentially significant impact. Construction activities involving soil disturbance, excavation, cutting/filling, stockpiling and grading activities could result in increased erosion and sedimentation to surface waters. However, the potential consequences of any spill or release of these types of materials are generally minimal due to the localized, short-term nature of such releases. The volume of any spills would likely be relatively small because the volume in any single vehicle or container would generally be anticipated to be less than 50 gallons.

As noted in Impact \#3.4.9b, accidental spills or disposal of potentially harmful materials used during construction could possibly wash into and pollute surface water runoff. Mitigation Measure MM GEO-2 requires the preparation and implementation of a SWPPP to comply with the Construction General Permit requirements.

In order to reduce potential impacts to water quality during construction activities, Mitigation Measures MM GEO-1 as well as MM HYD-1 would be required. MM HYD-1 limits the amount of ground disturbance during grading activities to a minimum and implement BMPs to reduce the potential for soil erosion or water runoff during a rain event. With mitigation, the proposed project would not violate any water quality standards or waste discharge requirements. Once constructed, the project would drain water into the existing City sewer system and would not degrade surface or groundwater quality.

## Mitigation Measure(s)

MM HYD-1: The District shall limit grading to the minimum area necessary for construction of the project. Final grading plans shall include best management practices to limit on-site and off-site erosion.

Implementation of Mitigation Measure MM GEO-1.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.10b - Substantially decrease groundwater supplies or interfere substantially with groundwater recharge such that the project may impede sustainable groundwater management of the basin?

The water purveyor for the project is the City of Lemoore. The City has adopted an Urban Water Management Plan (UWMP) in 2017 (City of Lemoore, 2017). This document is a planning tool that was created to help generally guide the actions of urban water suppliers in successfully preparing for potential water supply disruptions and issues. It provides a framework for long-term water planning and informs the public of a supplier's plans for long-term resource planning that ensures adequate water supplies for existing and future demands.

The City currently utilizes local groundwater as its sole source of municipal water supply. The City's municipal water system extracts its water supply from underground aquifers via six active groundwater wells within the city limits. The City maintains four ground-level storage reservoirs within the distribution system, with a total capacity of 4.4 million gallons (MG) (City of Lemoore, 2017). The groundwater basin underlying the City is the Tulare Lake Basin as defined in the Department of Water Resources Bulletin 118 for construction and operation would come from the City of Lemoore's existing water system.

Per the City's 2015 UWMP, the City's existing system has a total supply capacity of $21,674,000$ gallons per day with an average day demand of $8,769,000$ gallons (City of Lemoore, 2017). As the project site is currently designated for community facilities, the General Plan has adequately analyzed the water needed to meet the water demand.

The existing college campus uses approximately 3,000 HCF (Hundred Cubic Feet) or 0.068 acre feet of water monthly (City of Lemoore, 2020). The proposed project will minimally increase the student population by five percent or 232 students. Since students commute and do not live on campus, this increase would not substantially increase water demand. Nor would implementation of the project deplete aquifer supplies or interfere substantially with groundwater recharge or significantly alter local groundwater supplies. Therefore, the project will have a less-than-significant impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

## Impacts would be less than significant.

Impact \#3.4.10c(i) - Would the project substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river, in a manner that would result in substantial erosion or siltation onsite or offsite?

The rate and amount of surface runoff is determined by multiple factors, including the following: topography, the amount and intensity of precipitation, the amount of evaporation that occurs in the watershed and the amount of precipitation and water that infiltrates to the groundwater. The proposed project would alter the existing drainage pattern of the site, which would have the potential to result in erosion, siltation, or flooding on or offsite.

However, there are no streams or rivers located on the project site. The disturbance of soils onsite during construction could cause erosion, resulting in temporary construction impacts. In addition, the placement of permanent structures onsite could affect drainage in the longterm. Impacts from construction and operation are discussed below.

As discussed in Impact \#3.4.10a. above, potential impacts on water quality arising from erosion and sedimentation are expected to be localized and temporary during construction. Construction-related erosion and sedimentation impacts as a result of soil disturbance would be less than significant after implementation of an SWPPP (see Mitigation Measure MM GEO-2) and BMPs required by the NPDES. No drainages or other water bodies are present on the project site, and therefore, the proposed project would not change the course of any such drainages.

Existing drainage pattern of the site and area would be affected by project development because of the increase in impervious surfaces at the site. The project design includes natural features such as landscaping and vegetation that would allow for the percolation of stormwater. However, there will be an addition in impervious surfaces that could increase the potential for stormwater runoff and soil erosion. The project would connect to existing City stormwater sewer infrastructure. The project will comply with all applicable local building codes and regulations in order to minimize impacts during construction and postconstruction of the project. With implementation of MM GEO-2, impacts that would result in substantial erosion or siltation on or offsite is less than significant.

## Mitigation Measure(s)

Implementation of MM GEO-2.

## Level of Significance

## Impacts would be less than significant with mitigation incorporated.

Impact \#3.4.10c(ii) - Would the project substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river, or substantially increase the rate or amount of surface runoff in a manner that would result in flooding onsite or offsite?

See also Impact \#3.4.10c(i), above. The project site is flat, and grading would be minimal. The topography of the site would not change because of grading activities, and it does not contain any water features, streams or rivers. The project would not substantially alter the existing drainage pattern of the site or area in a manner that would result in substantial erosion or siltation on- or off-site with the implementation of recommended Mitigation Measures MM GEO-2, which require an approved SWPPP and the use of BMP, and MM HYD1, which minimizes the amount of disturbed dirt where feasible during construction. Once operational, there would be no impact. Therefore, the project would have a less-thansignificant impact with the incorporation of mitigation.

Mitigation Measure(s)
Implement MM GEO-2 and MM HYD-1.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.10c(iii) - Would the project substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river or through the addition of impervious surfaces, in a manner which would create or contribute runoff water which would exceed the capacity of existing or planned stormwater drainage systems or provide substantial additional sources of polluted runoff?

Please see Impact \#3.4.10c(i)-c(ii), above, there are no water features, including a river or stream, on or near the project. Existing drainage pattern of the site and area would be affected by project development during grading as well as the construction of impervious surfaces such as the proposed buildings. Therefore, the project would have a less-thansignificant impact.

With implementation recommended Mitigation Measures MM GEO-1, which require an approved SWPPP and the use of BMP, MM HYD-1, which minimizes the amount of disturbed dirt where feasible during construction, the project would not substantially increase the rate or amount of surface runoff in a manner that would result in flooding on- or off-site, contribute runoff water which would exceed the capacity of existing or planned stormwater drainage systems, nor provide additional sources of polluted runoff during construction or operations. Therefore, with mitigation, the project would have a less-than-significant impact.

## Mitigation Measure(s)

Implementation of Mitigation Measures MM GEO-1and MM HYD-1.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.10c(iv) - Would the project substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river or through the addition of impervious surfaces, in a manner which would impede or redirect flood flows?

As discussed above in Impact \#3.4.10a through c(iii), construction activities could potentially degrade water quality through the occurrence of erosion or siltation at the project site.

Construction of the project would include soil-disturbing activities that could result in erosion and siltation, as well as the use of harmful and potentially hazardous materials
required to operate vehicles and equipment. The transport of disturbed soils or the accidental release of potentially hazardous materials could result in water quality degradation. The project would be required comply with the NPDES Construction General Permit. A SWPPP would be prepared to specify BMPs to prevent construction pollutants as required by MM GEO-2. The proposed project would not otherwise substantially degrade water quality.

As discussed above, the existing drainage pattern of the site and area would be affected by project development. However, the project will connect to the existing stormwater sewer system, and therefore potential impacts resulting from the impeding or redirection of flood flows would be less than significant. Therefore, the project will have a less-than-significant impact with mitigation incorporated.

## Mitigation Measure(s)

Implementation MM GEO-2.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.10d - Would the project, in flood hazard, tsunami, or seiche zones, risk release of pollutants due to project inundation?

The project site is not located near the ocean or a steep topographic feature (i.e., mountain, hill, bluff, etc.). Additionally, there is no body of water within the vicinity of the project site. The proposed project's inland location makes the risk of tsunami highly unlikely. The probability of a seiche occurring in the City of Lemoore is considered negligible. Furthermore, given the geologic context at the proposed project site and the absence of pollutants, if such an event were to occur, the likelihood of it exposing project structures or people to a significant risk is considered low.

As shown in Figure 3.4.10-1, the project is not located within a FEMA 100-year floodplain. According to FEMA, the site is located in an area of minimal flood hazard. As such, the project would not place housing within a 100-year flood hazard area as mapped on a federal flood hazard boundary or flood insurance rate map or other flood hazard delineation map.

## Mitigation Measure(S)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.10e - Conflict with or obstruct implementation of a water quality control plan or sustainable groundwater management plan?

As discussed in Impact \#3.4.10b, the water demand from this project would not result in a significant impact due to depleted groundwater resources or interference with groundwater recharge. Per the City's 2015 UWMP, the City's existing system has a total supply capacity of $21,674,000$ gallons per day with an average day demand of $8,769,000$ gallons (City of Lemoore, 2017). The existing college uses 22,158 gallons of water monthly, which represents a minimal portion of the water available from the City.

As the project site has a land use designation for Community Facilities, the General Plan has adequately analyzed the water needed to meet the increased water demand. The proposed project will not substantially deplete aquifer supplies or interfere substantially with groundwater recharge or significantly alter local groundwater supplies. Therefore, the project will have a less-than-significant impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.


Figure 3.4.10-1 100-Year Floodplain


### 3.4.11-Land Use and Planning

Would the project:


## Discussion

Impact \#3.4.11a - Would the project physically divide an established community?
The project is within the existing West Hills College Lemoore campus. The proposed project will be implemented within the existing footprint of the campus and would not physically divide an established community. Therefore, the project would have no impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.11b - Would the project cause a significant environmental impact due to a conflict with any land use plan, policy, or regulation adopted for the purpose of avoiding or mitigating an environmental effect?

The project is within the Lemoore General Plan, which has land use designation of Community Facilities. However, Government Code Section 53091 does not require a school district to comply with County land use designations or zoning requirements. The project will build a new building within the existing campus footprint. The proposed project would not conflict with any applicable land use plan, policy, or regulation of an agency with jurisdiction over the project (including, but not limited to the general plan, specific plan, local coastal program, or zoning ordinance) adopted for the purpose of avoiding or mitigating an environmental effect. Therefore, the project would have no impact.

## Mitigation Measure(S)

No mitigation is required.
Level of Significance
There would be no impact.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.12 - Mineral Resources

Would the project:
a. Result in the loss of availability of a known mineral resource that would be of value to the region and the residents of the State?
b. Result in the loss of availability of a locally important mineral resource recovery site delineated on a local general plan, specific plan, or other land use plan?

## Discussion

Impact \#3.4.12a - Would the project result in the loss of availability of a known mineral resource that would be of value to the region and the residents of the State?

The City of Lemoore and the surrounding area have no mapped mineral resources, and no regulated mine facilities (City of Lemoore, 2008). Additionally, per the California Department of Conservation - Geologic Energy Management Division (CalGEM, formerly the Division of Oil, Gas, and Geothermal Resources [DOGGR]), there are no active, inactive, or capped oil wells located within the project site, and it is not within a DOGGR-recognized oilfield. Therefore, there would be no impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

There would be no impact.
Impact \#3.4.12b - Would the project result in the loss of availability of a locally important mineral resource recovery site delineated on a local general plan, specific plan, or other land use plan?

The project site is not designated for mineral and petroleum resources activities by the City of Lemoore General Plan. The project site and surrounding lands are zoned for residential, mixed-use, and community facilities. No mining occurs in the project area or in the nearby vicinity. The closest active oil and gas field is located in the unincorporated community of Westhaven, approximately 10 miles southwest of the project site. There are no mineral extraction activities that will be conducted in the future as a result of the project. The project
would not result in the loss of availability of a locally important mineral resource recovery site delineated on a local general plan, specific plan, or other land use plan and would therefore have no impact.

## Mitigation Measures

No mitigation is required.

## LEVEL OF SIGNIFICANCE

There would be no impact.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.13 - NoISE

Would the project result in:
a. Exposure of persons to, or generate, noise levels in excess of standards established in a local general plan or noise ordinance or applicable standards of other agencies?
b. Exposure of persons to or generate excessive groundborne vibration or groundborne noise levels?
c. For a project located within the vicinity of a private airstrip, would the project expose people residing or working in the project area to excessive noise levels?

## Discussion

Impact \#3.4.13a - Would the project result in exposure of persons to, or generate, noise levels in excess of standards established in a local general plan or noise ordinance or applicable standards of other agencies?

The City of Lemoore 2030 General Plan Section 8.6-Noise provides a land use compatibility for community noise environment thresholds for schools of acceptable up to 70 dB (City of Lemoore, 2008). Construction and operation of the project will not exceed this standard.

Construction-related noise levels and activities will be temporary and intermittent. The proposed project will generate noise from the following construction equipment: crane, bulldozer, grader, bob cat, trencher, cement truck, water truck, trash truck, equipment delivery truck, and company vehicles. Additionally, traffic and the various other noises generally associated with construction activities will be temporary and only take place during daylight hours. In addition, the construction-related noise will be intermittent and cease once the proposed project is completed. Consequently, sensitive receptors located at the school site will not be exposed to noise levels that violate applicable noise standards. Impacts to sensitive receptors onsite are considered less than significant.

Once constructed, the project would not significantly increase traffic on local roadways and will not generate other types of noise. Activities that would take place within the new facilities would be similar to noise currently generated around the school site.

As indicated above, the project's noise impacts are anticipated to generate noise levels below standards established and comply with local codes and regulations. Any permanent increase in ambient noise levels in the project vicinity and temporary or periodic increases in ambient noise levels in the project vicinity would not be considered significant.

## Mitigation Measure(s)

No mitigation is required.

## LeVel of Significance

Impacts would be less than significant.
Impact \#3.4.13b - Would the project result in exposure of persons to or generate excessive groundborne vibration or groundborne noise levels?

Construction activities in general can have the potential to create groundborne vibrations. However, based on the soil types found in the general project vicinity, it is unlikely that any blasting or pile-driving would be required in connection with construction of the project.

The Federal Transit Administration (FTA) has published standard vibration velocities for construction equipment operations (Federal Highway Administration (FHWA), U.S. Department of Transportation, 2017). In general, the FTA architectural damage criterion for continuous vibrations (i.e., 0.2 inch/second) appears to be conservative even for sustained pile driving. Building damage can be cosmetic or structural. Ordinary buildings that are not particularly fragile would not experience any cosmetic damage (e.g., plaster cracks) at distances beyond 30 feet. This distance can vary substantially depending on the soil composition and underground geological layer between vibration source and receiver. In addition, not all buildings respond similarly to vibration generated by construction equipment. The typical vibration produced by construction equipment is illustrated in Table 3.4.13-1.

As indicated in Table 3.4.13-1, below, based on the FTA data, vibration velocities from typical heavy construction equipment that would be used during project construction range from 0.003 to 0.210 inch-per-second peak particle velocity (PPV) at 25 feet from the source of activity.

Table 3.4.13-1
Vibration Generated by Construction Equipment

| Equipment | Reference peak particle <br> velocity at 25 feet <br> (inches/second) | Approximate peak particle <br> velocity at 100 feet <br> (inches/second) |
| :---: | :---: | :---: |
| Large bulldozer | 0.089 | 0.011 |
| Loaded trucks | 0.076 | 0.010 |
| Small bulldozer | 0.003 | 0.0004 |


| Vibratory <br> compactor/roller | 0.210 | 0.026 |
| :---: | :---: | :---: |

Notes:
1 - Federal Transit Administration, Transit Noise and Vibration Impact Assessment Guidelines, May 2006. Table 12-2. 2 - Calculated using the following formula:
PPV equip $=$ PPVref $x(25 / D) 1.5$
where: PPV (equip) = the peak particle velocity in in/sec of the equipment adjusted for the distance PPV (ref) = the reference vibration level in in/sec from Table 12-2 of the FTA Transit Noise and Vibration Impact Assessment Guidelines
$\mathrm{D}=$ the distance from the equipment to the receiver
Construction will be of short duration and not required jackhammers or pile driving. Therefore, the potential for groundborne vibrations impacts during the construction of the project is considered less than significant. Once operational, the project would not have any activities that would create groundborne vibrations. The proposed project would not result in exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.13c - For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

To minimize noise conflicts, the City has taken steps to ensure appropriate noise mitigation measures are in place before allowing development, including measures such as the noise level reduction (NLR) criteria in Air Installations Compatible Use Zones (AICUZ)instructions aircraft noise policies.

The City Zoning Ordinance established a Naval Air Station Lemoore (NASL) overlay zone as provided in this article will apply to those properties as designated on the zoning map, generally west of State Route 41 and south of the city limits, which fall in the military influence area (MIA) (Ord. 2013-05, 2-6-2014) (City of Lemoore, 2020). The project is within the Overlay III area, which experiences aircraft noise less than 65 decibels ( $<65 \mathrm{~dB}$ CNEL). Development located within Overlay III of the NASL overlay zone are required to be constructed so as to attain an indoor noise level of 45 decibels ( 45 dB CNEL). The project shall be constructed in accordance with noise attenuation standards of the City adopted building code AICUZ. Impacts would be less than significant.

## Mitigation Measures

No mitigation is required.

## Level of Significance

Impacts would be less than significant.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less- than |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.14 - Population and Housing

Would the project:
a. Induce substantial population growth in an area, either directly (for example, by proposing new homes and businesses) or indirectly (for example, through extension of roads or other infrastructure)?
b. Displace substantial numbers of existing housing, necessitating the construction of replacement housing elsewhere?

## Discussion

Impact \#3.4.14a - Would the project induce substantial population growth in an area, either directly (for example, by proposing new homes and businesses) or indirectly (for example, through extension of roads or other infrastructure)?

The project includes a new Instructional Center could slight population growth in the area because is anticipated to increase the student population by five percent. However, the potential for population growth is not substantial relative to the total population of the City of Lemoore. According the California Department of Finance estimate, the City's population was 26,257 in 2019. The City anticipates a 3.1 percent annual increase in population, with an estimated population of 34,719 in 2025 and 47,115 by 2035 (City of Lemoore, 2017). Therefore, the impacts would be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.14b - Would the project displace substantial numbers of existing housing, necessitating the construction of replacement housing elsewhere?

The proposed project would not require demolition of any housing, as the project site is currently undeveloped. Therefore, there would be no need to construct replacement housing elsewhere. There would be no impact.

## Mitigation Measure(S)

No mitigation is required.
Level of Significance
There would be no impact.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.15 - Public Services

Would the project:
a. Result in substantial adverse physical impacts associated with the provision of new or physically altered governmental facilities, need for new or physically altered governmental facilities, the construction of which could cause significant environmental impacts, in order to maintain acceptable service ratios, response times, or to other performance objectives for any of the public services:

| i. | Fire protection? | $\square$ | $\square$ | $\boxtimes$ | $\square$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| ii. | Police protection? | $\square$ | $\square$ | $\boxtimes$ | $\square$ |
| iii. | Schools? | $\square$ | $\square$ | $\boxtimes$ | $\square$ |
| iv. | Parks? | $\square$ | $\square$ | $\boxtimes$ | $\square$ |
| v. | Other public facilities? | $\square$ | $\square$ | $\boxtimes$ | $\square$ |

## Discussion

Impact \#3.4.15a(i) - Would the project result in substantial adverse physical impacts associated with the provision of new or physically altered governmental facilities, need for new or physically altered governmental facilities, the construction of which could cause significant environmental impacts, in order to maintain acceptable service ratios, response times, or to other performance objectives for any of the public services - fire protection?

The Lemoore Volunteer Fire Department (LVFD) has operated as an all-volunteer department since 1921. The LVFD includes one Chief, two Assistant Chiefs, four Crew Captains, seven Engineers, eleven Emergency Medical Technicians, one paid part-time Secretary, and one paid full-time maintenance worker. The department covers an area of approximately nine square miles, with Mutual Aid Agreements with Kings County Fire, Hanford City Fire and the Naval Air Station Lemoore.

Table 3.4.15-1
Fire Service Existing and Future Demand

|  | Existing (2006) | Demand Buildout (2030) |
| :---: | :---: | :---: |
| Staffing | 35 volunteers | 72 volunteers |
| Facilities | 2 | 3 |

(City of Lemoore , 2008)
Construction and operation of the proposed project would not be expected to result in an increase in demand of fire protection services leading to the construction of new or physically altered facilities. Fire suppression support is provided by the City of Lemoore Volunteer Fire Department (LVFD), which has two fire stations and the closest station to the project site is located at 210 Fox Street, approximately 2.5 miles east of the project site.

The project will increase the local school population by approximately 232 students. The project will not result in significant environmental impacts related to acceptable service ratios, response times, or to other performance objectives fire protection services.

The City of Lemoore will ensure that construction activities would be in accordance with local and State fire codes. Fire protection services are adequately planned for within the City's General Plan through policies to ensure the City maintains Fire Department performance and response standards by allocating the appropriate resources. The project applicant is responsible for constructing any infrastructure needed to serve the project and pay the appropriate impact fees, which would reduce impacts to fire protection to less-thansignificant levels.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.15a(ii) - Would the project result in substantial adverse physical impacts associated with the provision of new or physically altered governmental facilities, need for new or physically altered governmental facilities, the construction of which could cause significant environmental impacts, in order to maintain acceptable service ratios, response times, or to other performance objectives for any of the public services - police protection?

The Police Department has a staff of 31 sworn peace officers and seven civilian staff members. There are 30 vehicles assigned to the department.

The Police Department currently operates at a ratio of 1.33 officers per thousand residents, which is lower than the Western U.S. average of 1.5 officers per thousand residents reported by the Federal Bureau of Investigation. Average response times in 2006 averaged between 2.1 to 6.1 minutes depending on the priority type. Response times and the ability of the Police

Department to provide acceptable levels of service are contingent on increasing staffing levels, sworn and civilian, consistent with resident population increase and the population of visitors, merchants, schools, and shoppers with the department's service area.

Table 3.4.15-2
Police Service Existing and Future Demand

|  | Existing (2006) | Demand Buildout (2030) |
| :---: | :---: | :---: |
| Sworn Officers | 31 | 64 |
| Population | 23,390 | 48,250 |

(City of Lemoore , 2008)
The City's police station is located at 657 Fox Street, approximately three miles northeast of the project site. The project will increase the local population by approximately 232 students. The project will not result in significant environmental impacts related to acceptable service ratios, response times, or to other performance objectives police protection services. Therefore, impacts on police protection services would therefore be considered less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level Of Significance

Impacts would be less than significant.
Impact \#3.4.15a(iii) - Would the project result in substantial adverse physical impacts associated with the provision of new or physically altered governmental facilities, need for new or physically altered governmental facilities, the construction of which could cause significant environmental impacts, in order to maintain acceptable service ratios, response

The project is not anticipated to result in the need for additional schools in the area. Therefore, impacts would be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.15a(iv) - Would the project result in substantial adverse physical impacts associated with the provision of new or physically altered governmental facilities, need for new or physically altered governmental facilities, the construction of which could cause
significant environmental impacts, in order to maintain acceptable service ratios, response times, or to other performance objectives for any of the public services - parks?

The nearest park to the site is two miles east. The project is not anticipated to result in a significantly greater usage of the parks in the project vicinity. Therefore, impacts would be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.15a(v) - Would the project result in substantial adverse physical impacts associated with the provision of new or physically altered governmental facilities, need for new or physically altered governmental facilities, the construction of which could cause significant environmental impacts, in order to maintain acceptable service ratios, response times, or to other performance objectives for any of the public services - other public facilities?

Community facilities are the network of public and private institutions that support the civic and social needs of the population. They offer a variety of recreational, artistic, and educational programs and special events. New community facilities are not specifically sited on the General Plan Land Use Diagram. Small-scale facilities are appropriately sited as integral parts of neighborhoods and communities, while existing larger-scale facilities are generally depicted as public/semi-public land use, as appropriate (City of Lemoore , 2008).

The proposed project does not include any impacts to other public facilities such as libraries, hospitals or emergency medical facilities. The proposed project would comply with the goals, policies, and implementation measures of the General Plan.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.16-Recreation

Would the project:
a. Increase the use of existing neighborhood and regional parks or other recreational facilities such that substantial physical deterioration of the facility would occur or be accelerated?
b. Include recreational facilities or require the construction or expansion of recreational facilities that might have an adverse physical effect on the environment?

## Discussion

Impact \#3.4.16a - Would the project Increase the use of existing neighborhood and regional parks or other recreational facilities such that substantial physical deterioration of the facility would occur or be accelerated?

The proposed project would not increase the use of existing neighborhood and regional parks or other recreational facilities such that substantial physical deterioration of the facility would occur or be accelerated or require the construction or expansion of recreational facilities, which might have an adverse physical effect on the environment. Therefore, the project would have a less-than-significant impact.

## Mitigation Measure(S)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.16b - Would the project include recreational facilities or require the construction or expansion of recreational facilities that might have an adverse physical effect on the environment?

See Impact \#3.4.15a, above.

## Mitigation Measure(s)

No mitigation is required.
Level of Significance
Impacts would be less than significant.

|  | Less than <br> Significant |  |  |
| :---: | :---: | :---: | :---: |
| Potentially | with <br> Significant | Less-than- <br> Mitigation | Significant |
| Impact | Incorporated | Impact | Impact |

### 3.4.17-Transportation and Traffic

Would the project:
a. Conflict with a program, plan, ordinance or policy addressing the circulation system, including transit, roadway, bicycle and pedestrian facilities?
b. Conflict or be inconsistent with CEQA Guidelines Section 15064.3, subdivision (b)?
c. Substantially increase hazards due to a geometric design feature (e.g., sharp curves or dangerous intersections) or incompatible uses (e.g., farm equipment)?
d. Result in inadequate emergency access?

## Discussion

A Traffic Study was prepared for this project (Ruettgers \& Schuler Civil Engineers, 2020), and is included in Appendix D.

Impact \#3.4.17a - Would the project conflict with a program, plan, ordinance or policy addressing the circulation system, including transit, roadway, bicycle and pedestrian facilities?

The project trip generation and design hour volumes shown in Table 3.4.17-1 were estimated using the Institute of Transportation Engineers (ITE) Trip Generation Manual, 10th Edition. Rates and directional splits for ITE Land Use Code 540 (Junior/Community College: Students, Weekday, Peak Hour of Adjacent Street Traffic) were used to estimate project trip generation based on a total of 232 students. The AM and PM peak hours of adjacent street traffic was determined to be between 7:00 a.m. and 8:00 a.m., and between 4:30 p.m. and 5:30 p.m., based on a review of historical count data.

Table 3.4.17-1
Project Estimated Trips

| General Information |  |  | Daily Trips |  | AM Peak Hour Trips |  |  | PM Peak Hour Trips |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ITE <br> Code | Development Type | Variable | $\begin{aligned} & \text { ADT } \\ & \text { RATE } \end{aligned}$ | ADT | Rate | In \% Split/ Trips | Out <br> \% Split/ Trips | Rate | $\begin{gathered} \text { In } \\ \text { \% Split/ } \\ \text { Trips } \end{gathered}$ |  |
| 540 | Junior/Community College | $232$ <br> Students | eq | 1012 | eq | $\begin{gathered} 81 \% \\ 92 \end{gathered}$ | $\begin{gathered} 19 \% \\ 22 \\ \hline \end{gathered}$ | eq | $\begin{gathered} 56 \% \\ 51 \end{gathered}$ | $\begin{gathered} 44 \% \\ 40 \\ \hline \end{gathered}$ |

## Transit

The Kings Area Rural Transit (KART) operates two transit routes in the study area. Route 12, KART Transit Center to Skyline and Union, has stops at Bush and Belle Haven and West Hills College (WHC). The route operates Monday through Friday with three a.m. and two p.m. stops starting around 8:10 a.m. and stopping at 5:00 p.m. Route 20, KART Transit Center to WHC, likewise has stops at Bush and Belle Haven and WHC. This route operates Monday through Friday from approximately 6:10 a.m. to 10:40 a.m. with 30-minute headways.

## Bike

A Class 1 bike path is located along the south side of Bush Street between College Avenue and Belle Haven Drive. Class 1, shared use paths, are non-motorized facilities, paved or unpaved, physically separated from motorized vehicular traffic by an open space or barrier. Additional bike facilities are planned for Bush Street east and west of the current bike path, College Avenue, Semas Avenue (new alignment), Pederson Street, $191 / 2$ Avenue, the Union Pacific Railroad alignment, and the trail and gas pipeline easement that runs through the project site.

## Roadways

The City of Lemoore does not have an adopted level of service standard, however, per the General Plan most traffic studies are using a LOS "D" as their standard for traffic impact study purposes. Caltrans endeavors to maintain a target LOS at the transition between LOS "C" and LOS "D" on State highway facilities.

As shown in Table 3.4.17-2, Bush Street and State Route 41 Southbound Ramps operates below an acceptable level of service in the existing year prior to the addition of project traffic. All other intersections within the scope of the study are anticipated to operate at an acceptable level of service prior to and with the addition of project traffic.

In 2024, Bush Street and Semas Drive is anticipated to operate below an acceptable level of service prior to the addition of project traffic. With the addition of project traffic, Bush Street and S. $191 / 2$ Avenue is anticipated to operate below an acceptable level of service. All other
intersections within the scope of the study are anticipated to operate at an acceptable level of service prior to and with the addition of project traffic.

Table 3.4.17-2
Traffic Conditions Analysis

| Street | 2020 Directional LOS |  | 2024 Directional LOS |  | 2040 Directional LOS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | East AM/PM | West AM/PM | East AM/PM | West AM/PM | East AM/PM | West AM/PM |
| Bush St: College Ave to Semas Dr | A/B | C/B | B/B | B/B | C/C | C/C |
| Bush St: <br> Semas Dr to Belle Haven Dr | B/B | B/B | B/B | B/B | C/B | C/B |
| Bush St: <br> Belle Haven Dr to SR 41 SB | B/B | B/B | B/B | B/B | C/B | C/B |
| $\begin{gathered} \text { Bush St: } \\ \text { SR } 41 \text { SB to SR } 41 \text { NB } \end{gathered}$ | A/A | A/A | A/A | A/A | A/A | B/A |
| Bush St: <br> SR 41 NB to N $191 ⁄ 2$ Ave | A/A | A/A | A/A | A/A | A/A | B/A |
| Street | 2020+Project Directional LOS |  | 2024+Project Directional LOS |  | 2040+Project Directional LOS |  |
| Bush St: College Ave to Semas Dr | B/C | B/B | B/B | B/B | C/C | C/C |
| Bush St: <br> Semas Dr to Belle Haven Dr | B/B | B/B | B/B | B/B | C/B | C/B |
| Bush St: <br> Belle Haven Dr to SR 41 SB | B/B | B/B | B/B | C/B | C/C | C/C |
| Bush St: <br> SR 41 SB to SR 41 NB | A/A | A/A | A/A | A/A | A/A | B/A |
| Bush St: <br> SR 41 NB to N $191 ⁄ 2$ Ave | A/A | A/A | A/A | A/A | A/A | B/A |

In 2040, Bush Street and Belle Haven Drive and Bush Street and State Route 41 Northbound Ramps are anticipated to operate below an acceptable level of service prior to the addition of project traffic. The remaining intersections within the scope of study are anticipated to operate at acceptable levels of service during the peak hour.

To mitigate the intersections that are projected to operate below the appropriate adopted level of service standard, MM TRA- 1 should be implemented.

## Mitigation Measure(s)

MM TRA-1: Intersection and roadway improvements needed by the year 2040 to maintain or improve the operational level of service of the street system in the vicinity include:

- Install a signal at Bust St \& Semas Dr
- Install a signal at Bust St \& Belle Haven Dr
- Install a signal at Bust St \& SR 41 SB Ramps
- Install a signal at Bust St \& SR 41 NB Ramps
- Install a signal at Bust St \& S. 19th ½ Ave


## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.17b - Would the project conflict or be inconsistent with CEQA Guidelines Section 15064.3, subdivision (b)?

An evaluation of vehicle miles traveled (VMT) for project traffic was conducted based on applicable California Environmental Quality Act (CEQA) Guidelines. The analysis involved comparing an estimate of VMT attributable to the project to a baseline VMT and assessing whether project VMT would result in a significant transportation impact. Following CEQA Guidelines, only passenger vehicles were included in the analysis.

Several factors were taken into consideration when estimating project VMT, including proposed land use, project trip type and distribution, and location of other land developments. 82.8 percent of project traffic is anticipated to be students, 15.7 percent of project traffic is anticipated to be faculty and staff, and 1.5 percent is anticipated to be heavy truck trips. Of the staff and faculty trips, 40 percent were anticipated to be local trips and 60 percent were anticipated to be traveling from other towns such as Hanford, Visalia, and Fresno. No pass-by trips are anticipated since there are no other land developments in the vicinity of the project.

As shown in Table 3.4.17-3, it is anticipated that the project would result in an average VMT of 5.49 miles per person. An average regional VMT of 8.37 miles per capita for the year 2020 was obtained from the Kings County 2018 Regional Transportation Plan.

Table 3.4.17-3
Traffic Conditions Analysis

| Trip Type | Project <br> ADT | Weighted <br> Average | Miles <br> Traveled | VMT per <br> Trip | Vehicle <br> Occupancy | VMT per <br> Person |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Staff/Faculty | 159 | 9.30 | 1,477 | 9.30 | 1 | 9.30 |
| Student | 838 | 4.0 | 3,352 | 4.0 | 1 | 4.0 |
| Heavy | 15 | 47.6 | 723 | 47.6 | 1 | 47.6 |
| Trucks | 1,012 |  | Weighted Average |  | 5.49 |  |
| Total | $\mathbf{1 , 0 1 2}$ |  |  |  |  |  |

The average project VMT of 5.49 miles per person is more than 15 percent less than the baseline average VMT of 8.37 miles per capita. Therefore, the project would have less-thansignificant impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.17c - Would the project substantially increase hazards due to a geometric design feature (e.g., sharp curves or dangerous intersections) or incompatible uses (e.g., farm equipment)?

The project will be designed to current standards and safety regulations. All intersections will be constructed as to comply with the City and Caltrans regulations, and design and safety standards of Chapter 33 of the California Building Codes (CBC) and the guidelines of Title 24 in order to create safe and accessible roadways.

Vehicles exiting the subdivision will be provided with a clear view of the roadway without obstructions. Landscaping associated with the entry driveways could impede such views, if improperly installed. Specific circulation patterns and roadway designs will incorporate all applicable safety measures to ensure that hazardous design features or inadequate emergency access to the site or other areas surrounding the project area would not occur.

Therefore, with the incorporated design features and all applicable rules and regulations, the project will have a less-than-significant impact.

## Mitigation Measure(s)

No mitigation is required.

## LEVEL OF SIGNIFICANCE

Impacts would be less than significant.

## Impact \#3.4.17d - Would the project result in inadequate emergency access?

See the discussion in Impact \#3.4.9f.
State and City Fire Codes establishes standards by which emergency access may be determined. The proposed project would have to provide adequate unobstructed space for fire trucks to turn around. The proposed project site would have adequate internal circulation capacity including entrance and exit routes to provide adequate unobstructed space for fire trucks and other emergency vehicles to gain access and to turn around.

The proposed project would not inhibit the ability of local roadways to continue to accommodate emergency response and evacuation activities. The proposed project would not interfere with the District's established Emergency Response Plan.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.18-Tribal Cultural Resources

Would the project:
a. Would the project cause a substantial adverse change in the significance of a tribal cultural resource, defined in Public Resources Code Section 21074 as either a site, feature, place, cultural landscape that is geographically defined in terms of the size and scope of the landscape, sacred place, or object with cultural value to a California Native American tribe, and that is:
i. Listed or eligible for listing in the California Register of Historical Resources, or in a local register of historical resources as defined in Public Resources Code Section 5020.1(k), or
ii. A resource determined by the lead agency, in its discretion and supported by substantial evidence, to be significant pursuant to criteria set forth in subdivision (c) of Public Resources Code Section 5024.1. In applying the criteria set forth in subdivision (c) of Public Resource Code Section 5024.1, the lead agency shall consider the significance of the resource to a California Native American tribe.

## Discussion

Impact \#3.4.18a(i) - Would the project cause a substantial adverse change in the significance of a tribal cultural resource, defined in Public Resources Code Section 21074 as either a site, feature, place, cultural landscape that is geographically defined in terms of the size and scope of the landscape, sacred place, or object with cultural value to a California Native American tribe, and that is listed or eligible for listing in the California Register of Historical Resources, or in a local register of historical resources as defined in Public Resources Code Section 5020.1(k)?

Please see Impacts \#3.4.5a, \#3.4.5b, and \#3.4.5d, above.

On December 10, 2020 letters were mailed to tribes listed in Appendix B. The letters included a brief project description and location maps (Appendix B). To date, no response has been received from any of the Indian tribes contacted.

On November 24, 2020, the Native American Heritage Commission (NAHC) was asked to conduct a search of its Sacred Lands File to identify previously recorded sacred sites or cultural resources of special importance to tribes and provide contact information for local Native American representatives who may have information about the project area. The NAHC responded on December 18, 2020, with its findings and attached a list of Native American tribes and individuals culturally affiliated with the project area.

With implementation of Mitigation Measures MM CUL-1 through MM CUL-2, the project would not cause a substantial adverse change in the significance of a tribal cultural resource that is listed or eligible for listing in the California Register of Historical Resources, or in a local register of historical resources.

## Mitigation Measure(s)

Implement MM CUL-1 through MM CUL-2.

## Level of Significance

Impact would be less than significant with mitigation incorporated.
Impact \#3.15.17a(ii) - Would the project cause a substantial adverse change in the significance of a tribal cultural resource, defined in Public Resources Code Section 21074 as either a site, feature, place, cultural landscape that is geographically defined in terms of the size and scope of the landscape, sacred place, or object with cultural value to a California Native American tribe, and that is a resource determined by the lead agency, in its discretion and supported by substantial evidence, to be significant pursuant to criteria set forth in subdivision (c) of Public Resources Code Section 5024.1. In applying the criteria set forth in subdivision (c) of Public Resource Code Section 5024.1, the lead agency shall consider the significance of the resource to a California Native American tribe?

Please see Impacts \#3.4.5a, \#3.4.5b, and \#3.4.5d, above.
With implementation of Mitigation Measures MM CUL-1 through MM CUL-2, the project would not cause a substantial adverse change in the significance of a tribal cultural resource that is a resource determined by the Lead Agency, in its discretion and supported by substantial evidence, to be significant pursuant to criteria set forth in subdivision (c) of Public Resources Code Section 5024.1.

## Mitigation Measure(s)

Implement MM CUL-1 through MM CUL-2.

## Level of Significance

Impact would be less than significant with mitigation incorporated.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
| Sotentially | Significant | with | Less-than- |

### 3.4.19-Utilities and Service Systems

Would the project:
a. Require or result in the relocation or construction of new or expanded water, wastewater treatment, or storm water drainage, electric power, natural gas, or telecommunications facilities, the construction or relocation of which could cause significant environmental effects?
b. Have sufficient water supplies available to serve the project and reasonably foreseeable future development during normal, dry and multiple dry years?
c. Result in a determination by the wastewater treatment provider that serves or may serve the project that it has adequate capacity to serve the project's projected demand in addition to the provider's existing commitments?
d. Generate solid waste in excess of State or local standards, or in excess of the capacity of local infrastructure, or otherwise impair the attainment of solid waste reduction goals?
e. Comply with federal, State, and local management and reduction statutes and regulations related to solid waste?

## Discussion:

Impact \#3.4.19a - Would the project require or result in the relocation or construction of new or expanded water, wastewater treatment, or storm water drainage, electric power, natural gas, or telecommunications facilities, the construction or relocation of which could cause significant environmental effects?

The project would be constructed on land that has already been designated for commercial facilities in the General Plan. The City has indicated that the infrastructure necessary to serve the project is available and sufficient and will connect to the City's existing water and sewer systems. The project is located within the planned future growth and service area for the City services.

Therefore, no additional sewer capacity would be required for the proposed project. Impacts are considered less than significant.

The City of Lemoore belongs to the San Joaquin Valley Power Authority, which was formed in November 2006, to develop and conduct electricity-related programs for the region. The San Joaquin Valley Power Authority is the governing body authorized by Community Choice, created by the California legislature in 2002, to provide an opportunity for local government (cities, counties or combinations of cities and counties) to purchase electricity on behalf of their residents and businesses. Community Choice is only for the purchase of electricity. The delivery, metering, billing, operation and maintenance of wires and poles remains the responsibility of PG\&E within Lemoore (City of Lemoore , 2008).

There is existing trunk and transmission facilities adequate to meet present and projected demand in the community. The project will connect to the existing transmission lines for electrical power. Telecommunication requirements for the project are typical of this type of land use and would not require any expansion or construction of new telecommunication facilities.

The proposed project would not require or result in the construction or expansion of existing of new water, wastewater treatment, electrical or telecommunications facilities. Therefore, the project would have a less-than-significant impact.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.19b - Would the project have sufficient water supplies available to serve the project and reasonably foreseeable future development during normal, dry and multiple dry years?

As noted in Impact \#3.4.10b, the Tulare Lake Subbasin total storage capacity is estimated to be 17,100,000 acre-feet to a depth of 300 feet, and 82,500,000 acre-feet to the base of fresh groundwater. According to the 2015 Urban Water Management Plan, the City's 2015 maximum day demand is approximately 12.8 mgd . As noted in Section 3.4.10b, the existing college campus uses approximately 0.068 acre feet of water monthly (City of Lemoore, 2020). The proposed project will minimally increase the student population by five percent or 232 students. Since students commute and do not live on campus, this increase would not substantially increase water demand. It is anticipated that the subbasin has sufficient water available to supply the project.

The project will connect to the existing water supply system. The usage of water would be consistent with the City's current demands. The proposed increase in water usage at the
project site is minimal and not anticipated to require the construction of new water facilities or the expansion of existing facilities. Impacts would be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.19c - Would the project result in a determination by the wastewater treatment provider that serves or may serve the project that it has adequate capacity to serve the project's projected demand in addition to the provider's existing commitments?

The project will connect to the existing City sewer system. The generation of wastewater and water would be consistent with the City requirements. The proposed increase in water and wastewater usage at the project site is minimal and is not anticipated to require the construction of new water or wastewater treatment facilities or the expansion of existing facilities. Impacts would be less than significant.

The project will connect to the existing storm drain lines. The site engineering and design plans for the proposed project would be required to implement BMPs, comply with requirements of the City Building and Development Standards and comply with the NPDES General Permit during construction. Implementation of MM GEO-1 would reduce impacts to less than significant.

Therefore, the project would not require or result in the construction of new storm water drainage facilities or expansion of existing facilities.

## Mitigation Measure(s)

Implementation of MM GEO-1.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.19d - Would the project generate solid waste in excess of State or local standards, or in excess of the capacity of local infrastructure, or otherwise impair the attainment of solid waste reduction goals?

Implementation of the proposed project would result in the generation of solid waste on the site, which would increase the demand for solid waste disposal. During construction these materials, which are not anticipated to contain hazardous materials, would be collected and transported away from the site to an appropriate disposal facility.

Solid waste disposal for Lemoore is managed by Kings Waste and Recycling Authority (KWRA). The City's PWD Refuse Division is responsible for solid waste collection services. The majority of the City's solid waste is taken to the Kettleman Hills non-hazardous landfill facility, owned by Chemical Waste Management (CWMI). The facility is located south of Lemoore and has an available capacity of 15.6 million cubic yards as of 2020 (Cal Recycle , 2020). KWRA is currently studying the future needs of solid waste services including building a new landfill to be operated by CWMI near the existing site. The County has a 25year contract with CWMI to handle its solid waste until 2023 (City of Lemoore , 2008).

The project, in compliance with federal, State, and local statutes and regulations related to solid waste, would dispose of all waste generated onsite at an approved solid waste facility. The project does not, and would not conflict with federal, State, or local regulations related to solid waste. The proposed project would be served by a landfill with sufficient permitted capacity to accommodate the project's solid waste disposal needs in compliance with federal, State, and local statutes and regulations related to solid waste. Therefore, the project would have a less-than-significant impact.

## Mitigation Measure(s)

No mitigation is required.
Level of Significance
Impacts would be less than significant.
Impact \#3.4.19e - Would the project comply with federal, State, and local management and reduction statutes and regulations related to solid waste?

See discussion for Impact \#3.4.19d.

## Mitigation Measure(s)

No mitigation is required.
Level of Significance
Impacts would be less than significant.

### 3.4.20 - Wildfire

If located in or near state responsibility areas or lands classified as very high fire hazard severity zones, would the project:
a. Substantially impair an adopted emergency response plan or emergency evacuation plan?
b. Due to slope, prevailing winds, and other factors, exacerbate wildfire risks, and thereby expose project occupants to, pollutant concentrations from a wildfire or the uncontrolled spread of a wildfire?
c. Require the installation or maintenance of associated infrastructure (such as roads, fuel breaks, emergency water sources, power lines or Require the installation or maintenance of associated infrastructure (such as roads, fuel breaks, emergency water sources, power lines or
d. Expose people or structures to significant risks, including downslope or downstream flooding or landslides, as a result of runoff, post-fire slope instability, or drainage changes?

## Discussion:

Impact \#3.4.20a - Would the project substantially impair an adopted emergency response plan or emergency evacuation plan?

See Impact \#3.4.9f regarding emergency response.
Mitigation Measure(s)
No mitigation is required.
Level of Significance
Impacts would be less than significant.

Impact \#3.4.20b - Would the project, due to slope, prevailing winds, and other factors, exacerbate wildfire risks, and thereby expose project occupants to, pollutant concentrations from a wildfire?

Wildfire hazard data for the Lemoore Planning Area is provided by the California Department of Forestry and Fire Protection, as summarized in Table 3.4.20-1. The majority of the City is considered to have either little or no threat or a moderate threat of wildfire. Only one percent of the Planning Area currently has a high threat of wildfire. Wildfire hazard present in the Planning Area should decrease as vacant parcels become developed.

Table 3.4.20-1
Existing Wildfire Hazards

| Fire Hazards | Acreage | Percent of City Area |
| :---: | :---: | :---: |
| Little or No Threat | 5,648 | 46 |
| Moderate | 6,494 | 53 |
| High | 85 | 1 |
| Very High | 0 | 0 |
| Total | $\mathbf{1 2 , 2 2 7}$ | $\mathbf{1 0 0}$ |

There are no other factors of the project or the surrounding area that would exacerbate wildfire risks, and thereby expose project occupants to pollutant concentration from a wildfire or the uncontrolled spread of a wildfire. Therefore, impacts would be less than significant.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.20c - Would the project, require the installation or maintenance of associated infrastructure (such as roads, fuel breaks, emergency water sources, power lines?

See Impacts \#3.4.20a and b, above.
As discussed above, the proposed project site is not located in or near State responsibility areas or lands classified as very high hazard severity zones. Additionally, the project would not require the installation or maintenance of infrastructure that would exacerbate fire risk or result in environmental impacts. Therefore, impacts would be less than significant.

## Mitigation Measure(S)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.
Impact \#3.4.20d - Would the project, expose people or structures to significant risks, including downslope or downstream flooding or landslides, as a result of runoff, post-fire slope instability, or drainage changes?

The project site is not located near the ocean or a steep topographic feature (i.e., mountain, hill, bluff, etc.). Additionally, there is no body of water within the vicinity of the project site. As shown in Figure 3.4.10-1, the project is not located within a FEMA 100-year floodplain. According to FEMA, the site is located in an area of minimal flood hazard and has a less than 0.2 percent chance of an annual flooding. As such, the project would not place housing within a 100-year flood hazard area as mapped on a federal flood hazard boundary or flood insurance rate map or other flood hazard delineation map.

Therefore, the project will not expose people or structures to risks of flooding, landslides, runoff, slope instability, or drainage changes.

## Mitigation Measure(s)

No mitigation is required.

## Level of Significance

Impacts would be less than significant.

|  | Less than |  |  |
| :---: | :---: | :---: | :---: |
|  | Significant |  |  |
| Potentially | with | Less-than- |  |
| Significant | Mitigation | Significant | No |
| Impact | Incorporated | Impact | Impact |

### 3.4.21-MANDAtory Findings of Significance

a. Does the project have the potential to degrade the quality of the environment, substantially reduce the habitat of a fish or wildlife species, cause a fish or wildlife population to drop below self-sustaining levels, threaten to eliminate a plant or animal community, substantially reduce the number or restrict the range of a rare or endangered plant or animal, or eliminate important examples of the major periods of California history or prehistory?
b. Does the project have impacts that are individually limited, but cumulatively considerable? ("Cumulatively considerable" means that the incremental effects of a project are significant when viewed in connection with the effects of past projects, the effects of other current projects, and the effects of probable future projects.)
c. Does the project have environmental effects that would cause substantial adverse effects on human beings, either directly or indirectly?

## Discussion:

Impact \#3.4.21a - Does the project have the potential to degrade the quality of the environment, substantially reduce the habitat of a fish or wildlife species, cause a fish or wildlife population to drop below self-sustaining levels, threaten to eliminate a plant or animal community, substantially reduce the number or restrict the range of a rare or endangered plant or animal, or eliminate important examples of the major periods of California history or prehistory?

As evaluated in this IS/MND, the proposed project would not substantially degrade the quality of the environment; substantially reduce the habitat of a fish or wildlife species; cause a fish or wildlife population to drop below self-sustaining levels; threaten to eliminate a plant or animal community; reduce the number or restrict the range of an endangered, rare, or threatened species; or eliminate important examples of the major periods of California history or prehistory. Mitigation measures have been included to lessen the significance of
potential impacts. Similar mitigation measures would be expected of other projects in the surrounding area, most of which share a similar cultural paleontological and biological resources. Consequently, the incremental effects of the proposed project, after mitigation, would not contribute to an adverse cumulative impact on these resources. Therefore, the project would have a less-than-significant impact with mitigation incorporated.

## Mitigation Measure(s)

Implement MM BIO-1 through MM BIO-8; MM CUL-1 through MM CUL-2.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.21b - Does the project have impacts that are individually limited, but cumulatively considerable? ("Cumulatively considerable" means that the incremental effects of a project are significant when viewed in connection with the effects of past projects, the effects of other current projects, and the effects of probable future projects)?

As described in the impact analyses in Sections 3.4.1 through 3.4.20 of this IS/MND, any potentially significant impacts of the proposed project would be reduced to a less-thansignificant level following incorporation of the mitigation measures. All planned projects in the vicinity of the proposed project would be subject to review in separate environmental documents and required to conform to the City of Lemoore General Plan, zoning, mitigate for project-specific impacts, and provide appropriate engineering to ensure the development meets are applicable federal, State and local regulations and codes. As currently designed, and with compliance of the recommended mitigation measures, the proposed project would not contribute to a cumulative impact. Thus, the cumulative impacts of past, present, and reasonably foreseeable future projects would be less than cumulatively considerable.

## Mitigation Measure(s)

Implement MM BIO-1 through MM BIO-8, MM CUL-1 through MM CUL-2, MM GEO-1 through MM GEO-3, MM HYD-1, and MM TRA-1.

## Level of Significance

Impacts would be less than significant with mitigation incorporated.
Impact \#3.4.21c - Does the project have environmental effects that would cause substantial adverse effects on human beings, either directly or indirectly?

All of the project's impacts, both direct and indirect, that are attributable to the project were identified and mitigated to a less-than-significant level. The project will have the appropriate engineering to ensure the development meets are applicable federal, State and local regulations and codes. Thus, the cumulative impacts of past, present, and reasonably foreseeable future projects would be less than cumulatively considerable. Therefore, the
proposed project would not either directly or indirectly cause substantial adverse effects on human beings because all potentially adverse direct impacts of the proposed project are identified as having no impact, less-than-significant impact, or less-than-significant impact with mitigation incorporated.

## Mitigation Measure(s)

Implement MM BIO-1 through MM BIO-8, MM CUL-1 through MM CUL-2, MM GEO-1 through MM GEO-3, MM HYD-1, and MM TRA-1.

Level of Significance
Impacts would be less than significant with mitigation incorporated.

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- South Valley Regional Manager


# SECTION 6 - Mitigation Monitoring and Reporting Program 

## RESERVED- to be included later

Appendix A
Small Project Analysis Level Assessment

# SMALL PROJECT ANALYSIS LEVEL ASSESSMENT West Hills CCD Lemoore Lemoore, CA 

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Project 200505.0231

1. EXECUTIVE SUMMARY ..... 1-1
1.1 Executive Summary ..... 1-1
1.2 Statement of Finding ..... 1-1
2. PROJECT INFORMATION ..... 2-1
2.1 Introduction. ..... 2-1
2.2 Project Location ..... 2-1
3. SMALL PROJECT ANALYSIS LEVEL QUALIFICATION ..... 3-1
4. AIR QUALITY IMPACTS THRESHOLDS AND EVALUATION METHODOLOGY ..... 4-1
5. PROJECT-RELATED EMISSIONS ..... 5-1
5.1 Short-Term Emissions ..... 5-1
5.2 Long-Term Emissions ..... 5-1
5.3 Greenhouse Gas Emissions ..... 5-2
5.4 Potential Impact on Sensitive Receptors ..... 5-3
5.5 Potential Impacts to Visibility to Nearby Class 1 Areas ..... 5-3
5.6 Potential Odor Impacts ..... 5-3
5.7 Ambient Air Quality Impacts ..... 5-3
5.8 Toxic Air Contaminant (TAC) Impacts ..... 5-4
6. CONCLUSIONS ..... 6-1
7. REFERENCES ..... 7-1
APPENDIX A. CALEEMOD EMISSIONS ESTIMATES OUTPUT FILES ..... A-1
APPENDIX B. TOXIC EMISSIONS AND PRIORITIZATION ..... B-1

Figure 2-1. Project Location
Figure 2-2. Proposed Site Plan 2-2
Table 3-1. Small Project Analysis Level in Units for Educational ..... 3-1
Table 3-2. Small Project Analysis Level in Daily Trips for Educational ..... 3-1
Table 4-1. SJVAPCD Air Quality Thresholds of Significance - Criteria Pollutants ..... 4-1
Table 5-1. Construction Emissions ..... 5-1
Table 5-2. Total Project Operational Emissions ..... 5-2
Table 5-3. Estimated Annual Greenhouse Gas Emissions ..... 5-2

## 1. EXECUTIVE SUMMARY

### 1.1 Executive Summary

Trinity Consultants (Trinity) has completed a limited air quality assessment for the West Hills Community College, Lemoore campus. The Project includes the construction of a new 42,000 square foot, two-story Instruction Center on an undeveloped but disturbed portion of the existing campus.

This limited air quality assessment uses the San Joaquin Valley Air Pollution Control District's (SJVAPCD) screening tool, Small Project Analysis Level (SPAL) (SJVAPCD 2020). This SPAL assessment was prepared pursuant to the SJVAPCD's Guidance for Assessing and Mitigating Air Quality Impacts (GAMAQI) (SJVAPCD 2015), the California Environmental Quality Act (CEQA) (Public Resources Code 21000 to 21189) and the CEQA Guidelines (California Code of Regulations Title 14, Division 6, Chapter 3, Sections 15000 - 15387).

### 1.2 Statement of Finding

Based on the SPAL established by the SJVAPCD's GAMAQI, the emissions estimates prepared pursuant to this SPAL assessment do not exceed the SJVAPCD's established emissions thresholds and significance thresholds for all CEQA air quality determinations; this Project would therefore not pose a significant impact to the San Joaquin Valley Air Basin and would have a less than significant air quality impact.

## 2. PROJECT INFORMATION

### 2.1 Introduction

The Project site is located at the West Hills Community College, Lemoore campus. The Project includes the construction of a new 42,000 square foot, two-story Instruction Center on an undeveloped but disturbed portion of the existing campus. The Project was assessed as if it would be developed in one phase. This assessment examines the projected gross impacts to air quality posed by this Project to the San Joaquin Valley Air Basin to determine whether or not the Project remains below established air quality thresholds of significance.

### 2.2 Project Location

The Project is located in Lemoore, California near the southwest corner of Bush Street and College Avenue. Figure 2-1 depicts the Project location within the City of Lemoore and Figure 2-2 depicts the proposed site plan.

Figure 2-1. Project Location


Figure 2-2. Proposed Site Plan


## 3. SMALL PROJECT ANALYSIS LEVEL QUALIFICATION

This assessment was prepared pursuant to the SJVAPCD's GAMAQI (SJVAPCD 2015), the CEQA (Public Resources Code 21000 to 21189) and CEQA Guidelines (California Code of Regulations Title 14, Division 6, Chapter 3, Sections 15000 - 15387). The SJVAPCD created the SPAL screening tool to streamline air quality assessments of commonly encountered projects. According to GAMAQI, the SJVAPCD "pre-calculated the emissions on a large number and types of projects to identify the level at which they have no possibility of exceeding the emissions thresholds" ${ }^{1}$.

The SJVAPCD SPAL process established review parameters to determine whether a project qualifies as a "small project." A project that is found to be "less than" the established parameters has "no possibility of exceeding criteria pollutant emissions thresholds." Table 3-1 presents the SPAL size parameters for educational projects, and Table 3-2 presents the SPAL daily trip parameters for educational projects.

Table 3-1. Small Project Analysis Level in Units for Educational

| Land Use Category - Educational | Project Size (square feet)* |
| :---: | :---: |
| Elementary | 156,000 |
| Junior High School | 168,800 |
| High School | 153,600 |
| Junior College (2 year) | 74,400 |
| University/College (4 year) | 1,200 students |
| Library | 38,400 |
| Place of Worship | 141,000 |
| Proposed Project - Junior College | 42,000 |
| SPAL Exceeded? | No |
| *Project size based on SPAL Table 5, as posted on SJVAPCD webpage: <br> https://www.valleyair.org/transportation/CEQA\%20Rules/GAMAQI-SPAL.PDF |  |

As shown in Table 3-1, the proposed Project would not exceed the established SPAL limits for a "Junior College" educational project. The Project would construct a new 42,000 square foot, two-story Instruction Center on an undeveloped but disturbed portion of the existing campus.

Table 3-2. Small Project Analysis Level in Daily Trips for Educational

| Land Use Category Educational | Average Daily Trips (non-HHD)* | Average Daily Trips (HHD)* |
| :---: | :---: | :---: |
| Elementary | 1,000 | 15 |
| Junior High School |  |  |
| High School |  |  |
| Junior College (2 year) |  |  |
| University/College (4 year) |  |  |
| Library |  |  |
| Place of Worship |  |  |
| Proposed Project - Junior College | 997 | 15 |
| SPAL Exceeded? | No | No |
| *Daily trips based on SPAL Table 5, as https://www.valleyair.org/transportatio | sted on SJVAPCD webpag CEQA\%20Rules/GAMAQI- |  |

[^1]As shown in Table 3-2, the proposed Project would not exceed the established SPAL limits for a "Junior College" educational project. The Project would include 997 additional daily trips for all vehicle types except HHD and 15 additional daily trips for HHD vehicles. The SPAL threshold for HHD trips is based on a 50-mile trip length. Per traffic estimations from Ruettgers and Schuler, the HHD trips for the proposed Project are based on a 47.6-mile trip length.

Based on the above information, this Project qualifies for a limited air quality analysis applying the SPAL guidance to determine air quality impacts.

## 4. AIR QUALITY IMPACTS THRESHOLDS AND EVALUATION METHODOLOGY

Significance thresholds are based on the CEQA Appendix G Environmental Checklist Form (not included herein) and SJVAPCD air quality thresholds (SJVAPCD 2015). A potentially significant impact to air quality, as defined by the CEQA Checklist, would occur if the project caused one or more of the following to occur:

- Conflict with or obstruct implementation of the applicable air quality plan;
- Result in a cumulatively considerable net increase of any criteria pollutant for which the project region is non-attainment under an applicable federal or state ambient air quality standard;
- Expose sensitive receptors to substantial pollutant concentrations; and/or
- Result in other emissions (such as those leading to odors) adversely affecting a substantial number of people.

The SJVAPCD has identified quantitative emission thresholds to determine whether the potential air quality impacts of a project require analysis in the form of an Environmental Impact Report. The SJVAPCD air quality thresholds from the GAMAQI are presented in Table 4-1 (SJVAPCD 2015). The SJVAPCD separates construction emissions from operational emissions, and further separates permitted operational emissions from non-permitted operational emissions, for determining significance thresholds for air pollutant emissions.

Table 4-1. SJVAPCD Air Quality Thresholds of Significance - Criteria Pollutants

| Pollutant/ <br> Precursor | Construction <br> Emissions | Permitted Equipment <br> and Activities | Non-Permitted <br> Equipment and Activities |
| :---: | :---: | :---: | :---: |
|  | Emissions (tpy) | Emissions (tpy) | Emissions (tpy) |
| CO | 100 | 100 | 100 |
| NOx | 10 | 10 | 10 |
| ROG | 10 | 10 | 10 |
| SOx | 27 | 27 | 27 |
| $\mathrm{PM}_{10}$ | 15 | 15 | 15 |
| $\mathrm{PM}_{2.5}$ | 15 | 15 | 15 |

Source: SJVAPCD 2015
Criteria pollutant emissions were estimated using the California Emissions Estimator Model (CalEEMod) version 2016.3.2 (California Air Pollution Control Officers Association (CAPCOA) 2016). This project would generate short-term construction emissions and long-term operational emissions.

An air quality evaluation also considers: 1) exposure of sensitive receptors to substantial pollutant concentrations; and 2) the creation of other emissions (such as those leading to odors) adversely affecting a substantial number of people. The criteria for this evaluation are based on the Lead Agency's determination of the proximity of the proposed Project to sensitive receptors. A sensitive receptor is a location where human populations, especially children, senior citizens and sick persons, are present, and where there is a reasonable expectation of continuous human exposure to pollutants, according to the averaging period for ambient air quality standards, i.e., the 24 -hour, 8 -hour or 1 -hour standards. Commercial and industrial sources are not considered sensitive receptors.

## 5. PROJECT-RELATED EMISSIONS

This document was prepared pursuant to the SJVAPCD's GAMAQI and SPAL guidelines and provides a cursory review of the Project emissions to demonstrate that it would not exceed established air quality emissions thresholds.

### 5.1 Short-Term Emissions

Table 5-1 shows the construction emission levels using default CalEEMod factors for construction of a new 42,000 square foot, two-story Instruction Center on an undeveloped but disturbed portion of the existing campus (see Attachment A).

Construction emission estimates also included the following SJVAPCD's required measures for all projects:

- Water exposed area 3 times per day; and
- Reduce vehicle speed to less than 15 miles per hour.

Based on these anticipated activity levels, the Project construction activities would not exceed construction thresholds (Table 4-1). Therefore, construction emissions were found to be less than significant, and no further evaluation is required.

Table 5-1. Construction Emissions

| Emissions Source | Pollutant |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ROG | NOx | CO | SOx | PM ${ }_{10}$ | PM2.5 |
|  | (tons/year) |  |  |  |  |  |
| 2023 Construction Emissions | 0.10 | 0.91 | 1.01 | 0.002 | 0.08 | 0.05 |
| 2024 Construction Emissions | 0.31 | 0.20 | 0.25 | 0.000 | 0.02 | 0.01 |
| SJVAPCD Construction Emissions Thresholds | 10 | 10 | 100 | 27 | 15 | 15 |
| Is Threshold Exceeded? | No | No | No | No | No | No |

### 5.2 Long-Term Emissions

Table 5-2 presents the Project's long-term operations emissions generated from mobile, energy, and area sources as well as from water use and waste generation emissions. Most of these emissions impacts are from mobile sources traveling to and from the Project area. The following changes to default values were incorporated during the CalEEMod analysis:

- Daily trip rate for non-HHD vehicles was updated to 997 trips per day according to the Traffic Study (Ruettgers \& Schuler 2020)
- Trip rate was split into 159 trips per day for staff/faculty, with an average trip length of 9.3 miles, and 838 trips per day for students, with an average trip length of 4 miles.
- Daily trip rate for HHD vehicles was updated to 15 trips per day, with an average trip length of 47.6 miles, according to the Traffic Study (Ruettgers \& Schuler 2020)

Operational emission estimates also included the following mitigation measures even though the project was less than significant before mitigation:

- Improved Destination Accessibility;
- Improved Pedestrian Network;
- Use electric lawnmower, leaf blower, and chainsaw (3\% per SJVAPCD).

Table 5-2. Total Project Operational Emissions

| Emissions Source | Pollutant |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ROG | NOX | CO | SOx | PM ${ }_{10}$ | PM 2.5 |
|  | (tons/year) |  |  |  |  |  |
| Unmitigated |  |  |  |  |  |  |
| Operational Emissions | 0.38 | 2.38 | 2.00 | 0.01 | 0.87 | 0.24 |
| SJVAPCD Operational Emissions Thresholds -non-permitted sources | 10 | 10 | 100 | 27 | 15 | 15 |
| Is Threshold Exceeded Before Mitigation? | No | No | No | No | No | No |
| Mitigated |  |  |  |  |  |  |
| Operational Emissions | 0.38 | 2.34 | 1.91 | 0.01 | 0.81 | 0.22 |
| SJVAPCD Operational Emissions Thresholds -non-permitted sources | 10 | 10 | 100 | 27 | 15 | 15 |
| Is Threshold Exceeded? | No | No | No | No | No | No |

As calculated (see Attachment A), the long-term operational emissions associated with the proposed Project would be less than SJVAPCD significance threshold levels and would, therefore, not pose a significant impact to criteria air pollutants. This finding is consistent with the SPAL screening thresholds.

### 5.3 Greenhouse Gas Emissions

The Project's greenhouse gas (GHG) emissions are primarily from mobile source activities. Not all GHGs exhibit the same ability to induce climate change; as a result, GHG contributions are commonly quantified as carbon dioxide equivalents $\left(\mathrm{CO}_{2} \mathrm{e}\right)$ (see Attachment A). The proposed Project's operational $\mathrm{CO}_{2} \mathrm{e}$ emissions were estimated using CalEEMod. These emissions are summarized in Table 5-3.

Table 5-3. Estimated Annual Greenhouse Gas Emissions

|  | $\mathbf{C O}_{2}$ Emissions <br> metric tons | $\mathbf{C H}_{4}$ Emissions <br> metric tons | $\mathbf{N}_{2} \mathbf{O}$ Emissions <br> metric tons | $\mathbf{C O}_{2}$ e Emissions <br> metric tons |
| :---: | :---: | :---: | :---: | :---: |
| 2024 Project Operations | $1,298.58$ | 0.82 | 0.004 | $1,320.16$ |
| 2005 BAU | $1,928.57$ | 1.44 | 0.004 | $1,965.82$ |
| BAU less Project <br> emissions |  |  |  | $32.8 \%$ |

The current inventory and forecast for GHG emissions in the California Air Resources Board's 2008 Climate Change Scoping Plan supports the 2011 IPPC estimates. The 2008 Climate Change Scoping Plan also indicates that GHG emissions will increase to 596.41 million metric tons of $\mathrm{CO}_{2} \mathrm{e}$ by 2020 . It is widely understood that climate change is a "global" issue and, as such, GHG emissions are a cumulative problem and can only be evaluated as such.

The amount of $\mathrm{CO}_{2}$ that would be generated by the Project is so small in relation to the California $\mathrm{CO}_{2}$ equivalent estimates for 2020 ( 596 million metric tons $\mathrm{CO}_{2} \mathrm{e}$ ) that it's not possible for the contribution of the project to be cumulatively considerable. Additionally, the Project's GHG emissions are less than the 2005 business as usual emissions for the Project by 645.66 metric tons $\mathrm{CO}_{2} \mathrm{e}$, which is a $32.8 \%$ reduction. Therefore, the Project would not generate a cumulatively considerable GHG impact nor would it conflict with any
applicable plan, policy or regulation adopted for the purpose of reducing the emissions of GHGs. The Project will also not conflict with any elements of the California Air Resources Board's 2008 Climate Change Scoping Plan. Therefore, this potential impact is less than significant.

### 5.4 Potential Impact on Sensitive Receptors

The proposed Project is located near the southwest corner of Bush Street and College Avenue. Sensitive receptors are defined as areas where young children, chronically ill individuals, the elderly, or people who are more sensitive than the general population reside. Schools, hospitals, nursing homes and daycare centers are locations where sensitive receptors would likely reside. There are currently sensitive receptors at the existing Lemoore University Elementary Charter and Lemoore Middle College High School located on the proposed Project site. There are no other known schools, hospitals, or nursing homes within a one-mile radius of the Project.

Based on the predicted operational emissions and activity types, the proposed Project is not expected to affect any on-site or off-site sensitive receptors and is not expected to have any adverse impacts on any known sensitive receptor.

### 5.5 Potential Impacts to Visibility to Nearby Class 1 Areas

It should be noted that visibility impact analyses are not usually conducted for area sources. The recommended analysis methodology was initially intended for stationary sources of emissions which were subject to the Prevention of Significant Deterioration (PSD) requirements in 40 CFR Part 60. Since the Project's emissions are predicted to be significantly less than the PSD threshold levels, an impact at either the Dome Land Wilderness or the Sequoia National Park Areas (the two nearest Class 1 areas to the Project) is extremely unlikely. Therefore, based on the Project's predicted emissions, the Project is not expected to have any adverse impact to visibility at any Class 1 Area.

### 5.6 Potential Odor Impacts

The proposed Project is a junior college building surrounded by open land. Expected uses are not known to be a source of nuisance odors and are not listed in Table 6 of the SJVAPCD's GAMAQI. The Project is therefore not anticipated to have substantial odor impacts. The Project is therefore anticipated to have a less than significant odor impact.

### 5.7 Ambient Air Quality Impacts

As stated in the of GAMAQI (2015, p 96-97), SJVAPCD has developed screening levels for requiring an Ambient Air Quality Analysis (AAQA). The SJVAPCD recommends that an AAQA be performed for all criteria pollutants when emissions of any criteria pollutant resulting from project construction or operational activities exceed the 100 pounds per day screening level, after compliance with Rule 9510 requirements and implementation of all enforceable mitigation measures.

As shown above in Table 5-1 and Table 5-2, average daily emissions for construction and operational activities associated with this Project would not exceed 100 pounds per day. Therefore, an AAQA is not required for this Project.

### 5.8 Toxic Air Contaminant (TAC) Impacts

TACs, as defined by the California Health \& Safety Code (CH\&SC) §44321, are listed in Appendices AI and AII in AB 2588 Air Toxic "Hot Spots" and Assessment Act's Emissions Inventory Criteria and Guideline Regulation document. SJVAPCD's risk management objectives for permitting and CEQA are as follows:

- Minimize health risks from new and modified sources of air pollution.
- Health risks from new and modified sources shall not be significant relative to the background risk levels and other risk levels that are typically accepted throughout the community.
- Avoid unreasonable restrictions on permitting.

The proposed Project is a junior college building and is not expected to generate any TAC emissions. The increase in HHD trucks on-site due to this Project would generate small amounts of TAC emissions. The diesel particulate matter (DPM) generated by the additional HHD trucks is less than 0.1 pound per year. The prioritization score from this additional DPM is less than 1, and therefore the potential health risk impacts would be considered less than significant, and no further health risk assessment is required. The TAC emission calculations and prioritization are provided in Appendix B.

## 6. CONCLUSIONS

Based on the criteria established by the SJVAPCD's GAMAQI and SPAL guidelines, the proposed Project does not meet the minimum standards to require a full Air Quality Impact Analysis. Furthermore, the Project as proposed would not exceed the SJVAPCD's criteria air pollutant emission levels and would generate less than significant air quality impacts.

## 7. REFERENCES

California Environmental Quality Act (CEQA). 2019. (Public Resources Code 21000-21189) and CEQA Guidelines (California Code of Regulations Title 14, Division 6, Chapter 3, Sections 15000 - 15387).
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Ruettgers \& Schuler. 2020. Proposed Expansion Lemoore Community College Campus.
San Joaquin Valley Air Pollution Control District (SJVAPCD). 2020. Small Project Analysis Levels (SPAL), November 13, 2020. https://www.valleyair.org/transportation/CEQA\ Rules/GAMAQI-SPAL.PDF
-----------. 2015. Guidance for Assessing and Mitigating Air Quality Impacts (GAMAQI). March 19, 2015. http://www.valleyair.org/transportation/GAMAQI 3-19-15.pdf
-----------. 2009. Guidance for Valley Land-use Agencies in Addressing GHG Emission Impacts for New Projects under CEQA. December 17, 2009.

## APPENDIX A. CALEEMOD EMISSIONS ESTIMATES OUTPUT FILES

West Hills CCD Lemoore - Kings County, Annual

## West Hills CCD Lemoore

Kings County, Annual

### 1.0 Project Characteristics

1.1 Land Usage

| Land Uses | Size | Metric | Lot Acreage | Floor Surface Area | Population |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Junior College (2Yr) | 42.00 | 1000 sqft | 0.96 | $42,000.00$ | $\vdots$ |

### 1.2 Other Project Characteristics

| Urbanization | Rural | Wind Speed (m/s) | 2.2 | Precipitation Freq (Days) |
| :--- | :--- | :--- | :--- | :--- |
| Climate Zone | 3 |  | Operational Year |  |

### 1.3 User Entered Comments \& Non-Default Data

Project Characteristics -
Land Use -
Construction Phase - Start January 2023, End April 2024
Grading -
Vehicle Trips - Based on vehicle trip adjustment spreadsheet
Construction Off-road Equipment Mitigation -
Mobile Land Use Mitigation -
Area Mitigation -
Fleet Mix - Based on vehicle trip adjustment spreadsheet

West Hills CCD Lemoore - Kings County, Annual

| Table Name | Column Name | Default Value | New Value |
| :---: | :---: | :---: | :---: |
| tbIConstDustMitigation | WaterUnpavedRoadVehicleSpeed | 0 | 15 |
| tbiConstructionPhase | NumDays | 5.00 | 15.00 |
| tbiConstructionPhase | NumDays | 100.00 | 297.00 |
| tbiConstructionPhase | NumDays | 2.00 | 6.00 |
| tbiConstructionPhase | NumDays | 5.00 | 15.00 |
| tbiConstructionPhase | NumDays | 1.00 | 3.00 |
| tbIFleetMix | $\mathrm{HHD}^{-1}$ | 0.17 | 0.11 |
| tbiFleetMix | LDÄ | 0.51 | 0.66 |
| tblFleetMix | LDT1 | 0.03 | 0.03 |
| tbiFleetMix | LDT2 | 0.15 | 0.19 |
| tbIFleetMix | LHD1 | 0.02 | 0.00 |
| tbiFleetMix | L-̇D2 | $4.0800 \mathrm{e}-003$ | 0.00 |
| tbIFleetMix | MCY | $5.4520 \mathrm{e}-003$ | 0.00 |
| tbiFleetMix | MDV | 0.11 | 0.00 |
| tbiFleetMix | M ${ }^{\text {H }}$ | $6.1300 \mathrm{e}-004$ | 0.00 |
| tbiFleetMix | MHD | 0.01 | 0.00 |
| tblFieetMix | OBUS | $1.6890 \mathrm{e}-003$ | 0.00 |
| tbiFleetMix | SBUS | $9.0400 \mathrm{e}-004$ | 0.00 |
| tbiFleetMix | UBUS | $1.6060 \mathrm{e}-003$ | 0.00 |
| tbiProjectCharacteristics | UrbanizationLevel | Urban | Rural |
| tbiVehicleTrips | $\mathrm{CCO}_{-}^{\text {-TL }}$ | 6.60 | 4.84 |
| tblVehicleTrips | CC_TTP | 88.60 | 82.80 |
| tbiVehicleTrips | CNW_TL | 6.60 | 47.60 |
| tbiVehicleTrips | CNW_TTP | 5.00 | 1.50 |
| tbiVehicleTrips | CW_-- | 14.70 | 9.30 |
| tbIVehicleTrips | CW_TTP | 6.40 | 15.70 |

West Hills CCD Lemoore - Kings County, Annual

| tblVehicleTrips | DV_TP | 7.00 | 0.00 |
| :---: | :---: | :---: | :---: |
| tbIVehicleTrips | PB_TP | 1.00 | 0.00 |
| tblVehicleTrips | PR_TP | 92.00 | 100.00 |
| tblVehicleTrips | ST-̄' | 11.23 | 24.10 |
| tblVehicleTrips | SU-T | 1.21 | $24.10^{-7}$ |
| tblVehicleTrips | WD_TR | 27.49 | 24.10 |

### 2.0 Emissions Summary

### 2.1 Overall Construction

## Unmitigated Construction

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2023 |  | 0.9076 | 1.0134 | $\begin{gathered} 1.9500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0370 | 0.0416 | 0.0786 | 0.0105 | 0.0383 | 0.0488 | 0.0000 | 173.1500 | 173.1500 | 0.0439 | 0.0000 | 174.2484 |
| 2024 | 0.3145 | 0.1998 | 0.2500 | $\begin{gathered} 4.7000-- \\ 004 \end{gathered}$ | $\begin{gathered} 8.2000- \\ 003 \end{gathered}$ | $\begin{gathered} 8.8300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0170 | $\begin{array}{r} 2.000- \\ 003 \end{array}$ | $\begin{gathered} 8.1800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0104 | 0.0000 | 41.1613 | 41.1613 | 0.0101 | 0.0000 | 41.4131 |
| Maximum | 0.3145 | 0.9076 | 1.0134 | $\begin{gathered} 1.9500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0370 | 0.0416 | 0.0786 | 0.0105 | 0.0383 | 0.0488 | 0.0000 | 173.1500 | 173.1500 | 0.0439 | 0.0000 | 174.2484 |

## Mitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2023 | 0.0953 | 0.9076 | 1.0134 | $1.9500 \mathrm{e}-$ 003 | 0.0352 | 0.0416 | 0.0768 | $9.6700 \mathrm{e}-$ 003 | 0.0383 | 0.0480 | 0.0000 | : 173.1498 | ; 173.1498 | 0.0439 | 0.0000 | 174.2482 |
| 2024 | 0.3145 | 0.1998 | 0.2500 | $\begin{gathered} 4.7000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 8.2000 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 8.8300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0170 | $\begin{gathered} 2.2000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 8.1800 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0104 | 0.0000 | 41.1613 | 41.1613 | ---0101 | -0.0000 | 41.4130 |
| Maximum | 0.3145 | 0.9076 | 1.0134 | $\begin{gathered} 1.9500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0352 | 0.0416 | 0.0768 | $\begin{gathered} 9.6700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0383 | 0.0480 | 0.0000 | 173.1498 | 173.1498 | 0.0439 | 0.0000 | 174.2482 |
|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
| Percent Reduction | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 | 1.94 | 6.39 | 0.00 | 1.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

West Hills CCD Lemoore - Kings County, Annual

| Quarter | Start Date | End Date | Maximum Unmitigated ROG + NOX (tons/quarter) | Maximum Mitigated ROG + NOX (tons/quarter) |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 1-2-2023 | 4-1-2023 | 0.2450 | 0.2450 |
| 2 | 4-2-2023 | 7-1-2023 | 0.2520 | 0.2520 |
| 3 | 7-2-2023 | 10-1-2023 | 0.2548 | 0.2548 |
| 4 | 10-2-2023 | 1-1-2024 | 0.2550 | 0.2550 |
| 5 | 1-2-2024 | 4-1-2024 | 0.3092 | 0.3092 |
| 6 | 4-2-2024 | 7-1-2024 | 0.2018 | 0.2018 |
|  |  | Highest | 0.3092 | 0.3092 |

### 2.2 Overall Operational

## Unmitigated Operational

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Area | 0.1933 | 0.0000 | $\begin{gathered} 3.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | $\begin{gathered} 7.5000 \mathrm{e}- \\ 004 \\ \hline \end{gathered}$ | $\begin{gathered} 7.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.0000 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 004 \end{gathered}$ |
| Energy | 5.0000e- | -0.0455 | 0.0382 | 2.7000e- |  | $\begin{gathered} 3.4600 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 3.4600 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | ,189.0427 | 189.0427 | $\begin{gathered} 7.2600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 2.2100 \mathrm{e}- \\ 003 \end{gathered}$ | 189.8836 |
| Mobile | 0.1805 | 2.3378 | 1.9692 | 0.0124 | 0.8612 | 6.2000e- 003 | 0.8674 | 0.2297 | $\begin{aligned} & 5.7700 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.2355 | -0.000 | :1,152.585 | 1,152.585 | 0.0884 | 0.0000 | 1,154.795 |
| Waste |  |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 11.0833 | 0.0000 | 11.0833 | 0.6550 | 0.0000 | 27.4584 |
| Water |  |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.6536 | 6.5235 | 7.1771 | 0.0674 | $\begin{gathered} 1.6500 \mathrm{e}-\mathrm{-} \\ 003 \end{gathered}$ | 9.3532 |
| Total | 0.3787 | 2.3832 | 2.0077 | 0.0127 | 0.8612 | $\begin{gathered} 9.6600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.8709 | 0.2297 | $\begin{gathered} 9.2300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.2389 | 11.7369 | $\begin{gathered} 1,348.152 \\ 1 \end{gathered}$ | $\begin{gathered} 1,359.889 \\ 0 \end{gathered}$ | 0.8181 | $\begin{gathered} 3.8600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{array}{\|c\|} \hline 1,381.491 \\ 3 \end{array}$ |

### 2.2 Overall Operational

## Mitigated Operational



### 3.0 Construction Detail

## Construction Phase

West Hills CCD Lemoore - Kings County, Annual

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Site Preparation | :Site Preparation | 1/2/2023 | 1/4/2023 | 5 | 3 |  |
| 2 | Grading | :Grading | 1/5/2023 | 1/12/2023 | 5 | 6 |  |
| 3 | Building Construction | Building Construction | 11/13/2023 | 3/4/2024 | 5 | 297 |  |
| 4 | Paving | Paving | 3/5/2024 | 3/25/2024 | 5 | $15$ |  |
| 5 | Architectural Coating | Architectural Coating | :3/26/2024 | :4/15/2024 | 5 | 15 |  |

## Acres of Grading (Site Preparation Phase): 1.5

Acres of Grading (Grading Phase): 0

## Acres of Paving: 0

Residential Indoor: 0; Residential Outdoor: 0; Non-Residential Indoor: 63,000; Non-Residential Outdoor: 21,000; Striped Parking Area: 0 (Architectural Coating - sqft)

OffRoad Equipment

West Hills CCD Lemoore - Kings County, Annual

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | ;Graders | 1 | 8.00 | 187! | 0.41 |
| Site Preparation | Tractors/Loaders/Backhoes | 1 | 8.00 | 97 | 0.37 |
| Grading | :Concrete/Industrial Saws | 1 | 8.00 | 81: | 0.73 |
| Grading | Rubber Tired Dozers | 1 | 1.00 | 247! | 0.40 |
| Grading | Tractors/Loaders/Backhoes | 2 | 6.00 | 97! | 0.37 |
| Building Construction | :Cranes | 1 | 4.00 | 231 | 0.29 |
| Building Construction | Forklifts | 2 | 6.00 | 89 | 0.20 |
| Building Construction | Tractors/Loaders/Backhoes | 2 | 8.00 | 97: | 0.37 |
| Paving | :Cement and Mortar Mixers | 4 | 6.00 | 9 | 0.56 |
| Paving | :Pavers | 1 | 7.00 | 130 | 0.42 |
| Paving | :Rollers | 1 | 7.00 | 80 | 0.38 |
| Paving | Tractors/Loaders/Backhoes | 1 | 7.00 | 97! | 0.37 |
| Architectural Coating | :Air Compressors | $1:$ | 6.00 | 78 : | 0.48 |

Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation |  | 5.00 | 0.00 | 0.00 | 16.80 | 6.60 | 20.00 | D_Mix | !HDT_Mix | HHDT |
| Grading |  | 10.00 | 0.00 | 0.00 | 16.80 | 6.60 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Building Constructio |  | 18.00 | 7.00 | 0.00 | 16.80 | 6.60 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Paving |  | 18.00 | 0.00 | 0.00 | 16.80 | 6.60 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Architectural Coating |  | 4.00 | 0.00 | 0.00 | 16.80 | 6.60 | 20.00 | D_Mix | :HDT_Mix | H-ETT |

### 3.1 Mitigation Measures Construction

Water Exposed Area
Reduce Vehicle Speed on Unpaved Roads

West Hills CCD Lemoore - Kings County, Annual

### 3.2 Site Preparation-2023

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | $\begin{aligned} & 8.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $9.0000 \mathrm{e}-$ 005 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | $8.0000 \mathrm{e}-$ 004 | $\begin{gathered} 9.2800 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 5.8900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 3.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 3.4000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{aligned} & 3.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 3.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 1.2824 | 1.2824 | $\begin{aligned} & 4.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 1.2928 |
| Total | $\begin{aligned} & 8.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 9.2800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 5.8900 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 8.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 3.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.1400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 9.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 3.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 1.2824 | 1.2824 | $\begin{aligned} & \hline 4.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 1.2928 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 2.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | $\begin{gathered} 9.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 9.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e} \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.0709 | 0.0709 | 0.0000 | 0.0000 | 0.0709 |
| Total | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 2.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | $\begin{gathered} 9.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 9.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.0709 | 0.0709 | 0.0000 | 0.0000 | 0.0709 |

### 3.2 Site Preparation - 2023

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | $\begin{gathered} 3.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $3.1000 \mathrm{e}-$ 004 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | $8.0000 \mathrm{e}-$ $004$ | $\begin{gathered} 9.2800 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{aligned} & 5.8900 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e} \\ 005 \end{gathered}$ |  | $\begin{gathered} 3.4000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 3.4000-\mathrm{e} \\ 004 \end{gathered}$ |  | $\begin{gathered} 3.1000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 3.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.2824 | 1.2824 | $\begin{gathered} 4.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.2928 |
| Total | $\begin{gathered} 8.0000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.2800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.8900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 3.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 3.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 6.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 3.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 3.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 1.2824 | 1.2824 | $\begin{gathered} 4.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.2928 |

## Mitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 3.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $\begin{aligned} & 2.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | $\begin{gathered} 9.0000 \mathrm{e} \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 9.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 2.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | 0.0000 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.0709 | 0.0709 | 0.0000 | 0.0000 | 0.0709 |
| Total | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.6000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{gathered} 9.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{aligned} & 9.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.0709 | 0.0709 | 0.0000 | 0.0000 | 0.0709 |

### 3.3 Grading - 2023

## Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | $\begin{gathered} 2.2600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 2.2600 e 003 | $\begin{gathered} 1.2400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | $\begin{gathered} 1.2400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | ${ }^{1.94000-}$ | 0.0173 | 0.0222 | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ |  | $\begin{gathered} 8.5000- \\ 004 \end{gathered}$ | $\begin{gathered} 8.5000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{gathered} 8.1000-- \\ 004 \end{gathered}$ | $\begin{gathered} 8.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 3.1255 | 3.1255 | $\begin{gathered} 5.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 3.1397 |
| Total | $\begin{gathered} 1.9400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0173 | 0.0222 | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 2.2600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 8.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 3.1100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.2400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 8.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 3.1255 | 3.1255 | $\begin{gathered} 5.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 3.1397 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{aligned} & 1.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 1.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 1.0600 \mathrm{e} \\ & 003 \end{aligned}$ | 0.0000 | $\begin{aligned} & 3.7000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | $\begin{aligned} & 3.8000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 1.0000 \mathrm{e} \\ & 004 \end{aligned}$ | 0.0000 | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 0.2834 | 0.2834 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.2836 |
| Total | $\begin{gathered} 1.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.0600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 0.2834 | 0.2834 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.2836 |

### 3.3 Grading - 2023

## Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | $\begin{gathered} 8.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{gathered} 8.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 4.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{gathered} 4.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | ${ }^{1.94000} 0$ | 0.0173 | 0.0222 | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 8.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 8.5000- \\ 004 \end{gathered}$ |  | $\begin{gathered} 8.1000 e- \\ 004 \end{gathered}$ | $\begin{gathered} 8.1000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0000 | 3.1254 | 3.1254 | $\begin{gathered} 5.7000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0000 | 3.1397 |
| Total | $\begin{gathered} 1.9400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0173 | 0.0222 | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 8.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 8.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.7300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 8.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.2900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 3.1254 | 3.1254 | $\begin{gathered} 5.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 3.1397 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 1.5000e- | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.0600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | $\begin{gathered} -0000 \mathrm{e} \\ 1.004 \end{gathered}$ | 0.0000 | 0.2834 | 0.2834 | $\begin{gathered} 1.0000 \mathrm{e} \\ 005 \end{gathered}$ | 0.0000 | 0.2836 |
| Total | $\begin{gathered} 1.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.1000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.0600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{aligned} & 3.80000- \\ & \hline 004 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.2834 | 0.2834 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.2836 |

### 3.4 Building Construction-2023

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.0794 | 0.8055 | 0.8907 | $\begin{gathered} 1.4300 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0402 | 0.0402 |  | 0.0370 | 0.0370 | 0.0000 | 125.7616 | 125.7616 | 0.0407 | 0.0000 | 126.7784 |
| Total | 0.0794 | 0.8055 | 0.8907 | $\begin{gathered} 1.4300 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0402 | 0.0402 |  | 0.0370 | 0.0370 | 0.0000 | 125.7616 | 125.7616 | 0.0407 | 0.0000 | 126.7784 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | $1.8600 \mathrm{e}-$ 003 | 0.0671 | 0.0139 | 2.2000 e 004 | $5.2900 \mathrm{e}-$ 003 | $6.0000 \mathrm{e}-$ 005 | $5.3600 \mathrm{e}-$ 003 | $\begin{gathered} 1.5300 \mathrm{e}-\mathrm{-} \\ 003 \end{gathered}$ | $\begin{gathered} 6.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{aligned} & 1.5900 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 21.2857 | 21.2857 | $1.6700 \mathrm{e}-$ 003 | 0.0000 | 21.3276 |
| Worke | 0.0111 | $8.2300 \mathrm{e}-$ 003 | 0.0795 | $2.4000 \mathrm{e}-$ 004 | 0.0282 | $1.7000 \mathrm{e}-$ 004 | 0.0284 | $7.5000 \mathrm{e}-$ 003 | $1.5000 \mathrm{e}-$ 004 | $7.6500 \mathrm{e}-$ 003 | 0.0000 | 21.3405 | 21.3405 | $6.0000 \mathrm{e}-$ 004 | 0.0000 | 21.3554 |
| Total | 0.0130 | 0.0753 | 0.0933 | $\begin{aligned} & 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0335 | $\begin{gathered} 2.3000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0338 | $\begin{gathered} 9.0300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 2.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 9.2400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 42.6262 | 42.6262 | $\begin{aligned} & 2.2700 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 42.6830 |

### 3.4 Building Construction-2023

## Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.0794 | 0.8055 | 0.8907 | $\begin{aligned} & 1.4300 \mathrm{e}- \\ & 003 \end{aligned}$ |  | 0.0402 | 0.0402 |  | 0.0370 | 0.0370 | 0.0000 | 125.7614 | 125.7614 | 0.0407 | 0.0000 | 126.7783 |
| Total | 0.0794 | 0.8055 | 0.8907 | $\begin{gathered} 1.4300 \mathrm{e}- \\ 003 \end{gathered}$ |  | 0.0402 | 0.0402 |  | 0.0370 | 0.0370 | 0.0000 | 125.7614 | 125.7614 | 0.0407 | 0.0000 | 126.7783 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | $1.8600 \mathrm{e}-$ 003 | 0.0671 | 0.0139 | $2.2000 \mathrm{e}-$ 004 | 5.2900 e 003 | $6.0000 \mathrm{e}-$ 005 | $\begin{gathered} 5.3600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.5300 \mathrm{e}-\mathrm{-} \\ 003 \end{gathered}$ | $\begin{gathered} 6.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 1.5900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 21.2857 | 21.2857 | $\begin{gathered} 1.6700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 21.3276 |
| Worker | 0.0111 | $\begin{gathered} 8.2300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0795 | $\begin{gathered} 2.4000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0282 | $\begin{gathered} 1.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0284 | $\begin{gathered} 7.5000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.5000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 7.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 21.3405 | 21.3405 | $\begin{gathered} 6.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 21.3554 |
| Total | 0.0130 | 0.0753 | 0.0933 | $\begin{aligned} & 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0335 | $\begin{gathered} 2.3000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0338 | $\begin{gathered} 9.0300 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & \hline 2.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 9.2400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 42.6262 | 42.6262 | $\begin{aligned} & 2.2700 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 42.6830 |

### 3.4 Building Construction-2024

## Unmitigated Construction On-Site

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.0137 | 0.1374 | 0.1626 | $\begin{gathered} 2.6000 \mathrm{e} \\ 004 \end{gathered}$ |  | $\begin{gathered} 6.4900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.4900 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 5.9700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.9700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 23.0558 | 23.0558 | $\begin{gathered} 7.4600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 23.2422 |
| Total | 0.0137 | 0.1374 | 0.1626 | $\begin{aligned} & 2.6000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{aligned} & 6.4900 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 6.4900 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 5.9700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.9700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 23.0558 | 23.0558 | $\begin{gathered} 7.4600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 23.2422 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust <br> PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | $\begin{gathered} 3.3000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0122 | 2.4100 e 003 | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 9.7000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 9.8000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 2.8000 \mathrm{e}-\mathrm{-} \\ 004 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $2.9000 \mathrm{e}-$ 004 | 0.0000 | 3.8686 | 3.8686 | $3.1000 \mathrm{e}-$ 004 | 0.0000 | 3.8765 |
| Worke | $1.9100 \mathrm{e}-$ 003 | $1.3600 \mathrm{e}-$ 003 | 0.0134 | $4.0000 \mathrm{e}-$ 005 | $\begin{gathered} 5.1700 \mathrm{e}- \\ 003 \end{gathered}$ | $3.0000 \mathrm{e}-$ 005 | $5.2000 \mathrm{e}-$ 003 | $\begin{gathered} 1.3700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 1.4000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 3.7693 | 3.7693 | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 3.7718 |
| Total | $\begin{gathered} 2.2400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0135 | 0.0158 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 6.1400 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} \hline 6.1800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $\begin{gathered} 1.6900 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 7.6379 | 7.6379 | $\begin{gathered} 4.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 7.6482 |

### 3.4 Building Construction-2024

Mitigated Construction On-Site

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.0137 | 0.1374 | 0.1626 | $\begin{gathered} 2.6000 \mathrm{e} \\ 004 \end{gathered}$ |  | $\begin{gathered} 6.4900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 6.4900 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 5.9700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.9700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 23.0557 | 23.0557 | $\begin{gathered} 7.4600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 23.2421 |
| Total | 0.0137 | 0.1374 | 0.1626 | $\begin{aligned} & 2.6000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{aligned} & 6.4900 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 6.4900 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 5.9700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 5.9700 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 23.0557 | 23.0557 | $\begin{gathered} 7.4600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 23.2421 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | $0.0000$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | $3.3000 \mathrm{e}-$ 004 | 0.0122 | $2.4100 \mathrm{e}-$ 003 | $4.0000 \mathrm{e}-$ 005 | $9.7000 \mathrm{e}-$ 004 | $1.0000 \mathrm{e}-$ 005 | $9.8000 \mathrm{e}-$ 004 | $2.8000 \mathrm{e}-$ 004 | $1.0000 \mathrm{e}-$ 005 | $2.9000 \mathrm{e}-1$ 004 | 0.0000 | 3.8686 | 3.8686 | $3.1000 \mathrm{e}-$ 004 | 0.0000 | 3.8765 |
| Worker | $1.9100 \mathrm{e}-$ 003 | $\begin{gathered} 1.3600 \mathrm{e} \\ 003 \end{gathered}$ | 0.0134 | $\begin{gathered} 4.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 5.1700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{gathered} 5.2000 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 1.3700 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 3.0000 \mathrm{e} \\ 005 \end{gathered}$ | $\begin{aligned} & 1.4000 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 3.7693 | 3.7693 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 3.7718 |
| Total | $\begin{gathered} 2.2400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0135 | 0.0158 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 6.1400 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} \hline 6.1800 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 1.6900 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 7.6379 | 7.6379 | $\begin{gathered} 4.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 7.6482 |

### 3.5 Paving - 2024

## Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | $\begin{gathered} 4.4300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0392 | 0.0527 | $\begin{aligned} & 8.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{gathered} 1.8200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.8200 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 7.0505 | 7.0505 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 7.1018 |
| Paving | 0.0000 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | $\begin{gathered} 4.4300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0392 | 0.0527 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 1.8200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.8200 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 7.0505 | 7.0505 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 7.1018 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $6.2000 \mathrm{e}-$ | $4.4000 \mathrm{e}-$ | $4.3700 \mathrm{e}-$ | $1.0000 \mathrm{e}-$ | $1.6900 \mathrm{e}-$ | $1.0000 \mathrm{e}-$ | $1.7000 \mathrm{e}-$ | $4.5000 \mathrm{e}-$ | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | $4.6000 \mathrm{e}-$ | 0.0000 | 1.2291 | 1.2291 | $3.0000 \mathrm{e}-$ | 0.0000 | 1.2299 |
| Total | $\begin{gathered} 6.2000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 4.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 4.3700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.6900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 4.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 1.2291 | 1.2291 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 1.2299 |

### 3.5 Paving - 2024

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | $\begin{gathered} 4.4300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0392 | 0.0527 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 1.8200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.8200 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 7.0504 | 7.0504 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 7.1018 |
| Paving | 0.0000 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | $\begin{gathered} 4.4300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0392 | 0.0527 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 1.8200 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.8200 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 7.0504 | 7.0504 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 7.1018 |

## Mitigated Construction Off-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{gathered} 6.2000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & 4.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 4.3700 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{aligned} & 1.0000 \mathrm{e} \\ & 005 \end{aligned}$ | $\begin{gathered} 1.6900 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 1.0000 \mathrm{e} \\ & 005 \end{aligned}$ | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{aligned} & 4.5000 \mathrm{e} \\ & 004 \end{aligned}$ | $\begin{aligned} & 1.0000 \mathrm{e} \\ & 005 \end{aligned}$ | $\begin{aligned} & 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 1.2291 | 1.2291 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 1.2299 |
| Total | $\begin{gathered} 6.2000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 4.4000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 4.3700 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{aligned} & 1.6900 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 1.7000 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 4.5000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | $\begin{gathered} 4.6000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.2291 | 1.2291 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 1.2299 |

West Hills CCD Lemoore - Kings County, Annual

### 3.6 Architectural Coating - 2024

## Unmitigated Construction On-Site

|  | ROG | NOX | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Archit. Coating | 0.2920 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | $\begin{gathered} 1.3600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 9.1400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0136 | $\begin{aligned} & 2.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{gathered} 4.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 4.6000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{aligned} & 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | $4.60000-$ 004 | 0.0000 | 1.9149 | 1.9149 | $1.1000 \mathrm{e}-$ <br> 004 | 0.0000 | 1.9176 |
| Total | 0.2934 | $\begin{gathered} 9.1400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0136 | $\begin{aligned} & 2.0000 \mathrm{e}- \\ & 005 \end{aligned}$ |  | $\begin{aligned} & 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{aligned} & 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 4.6000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.9149 | 1.9149 | $\begin{aligned} & 1.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 1.9176 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | $0.0000$ | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{aligned} & 1.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $3.7000 \mathrm{e}-$ 004 | 0.0000 | $\begin{gathered} 3.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0000 | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 0.2731 | $0.2731$ | $\begin{gathered} 1.0000 \mathrm{e} \\ 005 \end{gathered}$ | 0.0000 | 0.2733 |
| Total | $\begin{aligned} & 1.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{aligned} & 3.7000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | $\begin{gathered} 3.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 0.2731 | 0.2731 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.2733 |

### 3.6 Architectural Coating-2024

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Archit. Coating | 0.2920 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | $1.3600 e-$ 003 | 9.1400 e 003 | 0.0136 | $2.0000 \mathrm{e}-$ 005 |  | $4.6000-$ 004 | $4.6000-$ 004 |  | $4.6000 \mathrm{e}-$ 004 | $4.6000 \mathrm{e}-$ 004 | 0.0000 | 1.9149 | 1.9149 | $1.1000 \mathrm{e}-$ 004 | 0.0000 | 1.9176 |
| Total | 0.2934 | $\begin{gathered} 9.1400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0136 | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ |  | $\begin{gathered} 4.6000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{aligned} & \hline 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{aligned} & 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & \hline 4.6000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 1.9149 | 1.9149 | $\begin{aligned} & 1.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 1.9176 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | $\begin{aligned} & 1.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 9.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.8000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | $1.0000 \mathrm{e}-$ 004 | 0.0000 | 0.2731 | 0.2731 | $1.0000 \mathrm{e}-$ 005 | 0.0000 | 0.2733 |
| Total | $\begin{aligned} & 1.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.7000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{gathered} 3.8000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 0.2731 | 0.2731 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.2733 |

### 4.0 Operational Detail - Mobile

### 4.1 Mitigation Measures Mobile

Improve Destination Accessibility
Improve Pedestrian Network

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Mitigated |  |  |  |  |  | $\begin{gathered} 5.8400 \mathrm{e}- \\ 003 \end{gathered}$ | 0.8076 | 0.2139 | $\begin{gathered} 5.4300 \mathrm{e}- \\ 003 \end{gathered}$ | 0.2193 | 0.0000 | ${ }^{1,091.273}$ | $\begin{gathered} 1,091.273 \\ 5 \end{gathered}$ | 0.0877 | 0.0000 | $\begin{array}{\|c} 1,093.465 \\ 8 \end{array}$ |
| Ünmitigated |  |  |  |  |  | -7.2000 e 003 | 0.8674 | 0.2297 | $\begin{gathered} -7.7700 \mathrm{e}- \\ 003 \end{gathered}$ |  |  |  | $\begin{gathered} 1,152.585 \\ 2 \end{gathered}$ | 0.0884 | 0.0000 | $\underset{4}{1,154.795}$ |

### 4.2 Trip Summary Information

|  | Average Daily Trip Rate |  |  | Unmitigated | Mitigated |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Weekday | Saturday | Sunday | Annual VMT | Annual VMT |
| Junior College (2Yr) | $1,012.20$ | $1,012.20$ | 1012.20 | $2,277,561$ | $2,120,409$ |
| Total | $1,012.20$ | $1,012.20$ | $1,012.20$ | $2,277,561$ | $2,120,409$ |

### 4.3 Trip Type Information

|  | Miles |  |  | Trip \% |  |  | Trip Purpose \% |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW | Primary | Diverted | Pass-by |
| Junior College (2Yr) | 9.30 | 4.84 | 47.60 | - 15.70 | 82.80 | 1.50 | 100 | 0 | 0 |

### 4.4 Fleet Mix

West Hills CCD Lemoore - Kings County, Annual

| Land Use | LDA | LDT1 | LDT2 | MDV | LHD1 | LHD2 | MHD | HHD | OBUS | UBUS | MCY | SBUS | MH |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Junior College (2Yr) | 0.65584 | 0.03494 | 0.19494 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.1142 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.000000 |

### 5.0 Energy Detail

Historical Energy Use: N

### 5.1 Mitigation Measures Energy

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Electricity Mitigated |  |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 139.5328 | 139.5328 | $\begin{gathered} 6.3100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.3100 \mathrm{e}- \\ 003 \end{gathered}$ | 140.0795 |
| Electricity Unmitigated |  |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 139.5328 | 139.5328 | $6.3100 e-$ 003 | 1.21000 003 | 140.0795- |
| NaturalGas Mitigated | $\begin{gathered} 5.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0455 | 0.0382 | $\begin{gathered} 2.7000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $3.4600 e-$ 003 | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | $\begin{gathered} 3.4600 \mathrm{e} \\ 003 \end{gathered}$ | $\begin{gathered} 3.4600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 49.5099 | 49.5099 | $\begin{gathered} 9.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 49.8041 |
| Naturaläas Unmitigated | $\begin{gathered} 5.0000 \mathrm{e} \\ 003 \end{gathered}$ |  |  | 2.70000 004 |  | $\begin{gathered} -\mathbf{- 2 6 0 0 e} \\ 003 \end{gathered}$ | -7.-00-0- 003 |  | $\begin{gathered} -7.4600 \mathrm{e}- \\ 003 \end{gathered}$ |  |  |  |  | $\begin{gathered} 9.5000 \mathrm{e} \\ 004 \end{gathered}$ | $\begin{gathered} 9.1000 \mathrm{e} \\ 004 \end{gathered}$ | 49.8041 |

### 5.2 Energy by Land Use - NaturalGas

## Unmitigated

|  | NaturalGa s Use | ROG | NOX | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU/yr | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Junior College (2Yr) | 927780 | $\begin{gathered} 5.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0455 | 0.0382 | $\begin{aligned} & 2.7000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 49.5099 | 49.5099 | $\begin{aligned} & 9.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 49.8041 |
| Total |  | $\begin{gathered} 5.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0455 | 0.0382 | $\begin{gathered} 2.7000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ |  | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{aligned} & 3.4600 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 49.5099 | 49.5099 | $\begin{aligned} & 9.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 9.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 49.8041 |

## Mitigated

|  | $\begin{gathered} \text { NaturalGa } \\ \text { s Use } \end{gathered}$ | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU/yr | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Junior College (2Yr) | 927780 | $\begin{gathered} 5.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0455 | 0.0382 | $\begin{gathered} 2.7000 \mathrm{e}- \\ 004 \end{gathered}$ |  | $\begin{gathered} 3.4600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.4600 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.4600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.4600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 49.5099 | 49.5099 | $\begin{gathered} 9.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 49.8041 |
| Total |  | $\begin{gathered} 5.0000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0455 | 0.0382 | $\begin{aligned} & \hline 2.7000 \mathrm{e}- \\ & 004 \end{aligned}$ |  | $\begin{gathered} 3.4600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.4600 \mathrm{e}- \\ 003 \end{gathered}$ |  | $\begin{gathered} 3.4600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 3.4600 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 49.5099 | 49.5099 | $\begin{gathered} 9.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 49.8041 |

West Hills CCD Lemoore - Kings County, Annual

### 5.3 Energy by Land Use - Electricity

Unmitigated

|  | Electricity Use | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kWh/yr | MT/yr |  |  |  |
| Junior College (2Yr) | 479640 | 139.5328 | $\begin{aligned} & 6.3100 \mathrm{e}- \\ & 003 \end{aligned}$ | $\begin{gathered} 1.3100 \mathrm{e}- \\ 003 \end{gathered}$ | 140.0795 |
| Total |  | 139.5328 | $\begin{gathered} 6.3100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.3100 \mathrm{e}- \\ 003 \end{gathered}$ | 140.0795 |

## Mitigated

|  | $\begin{array}{\|c} \text { Electricity } \\ \text { Use } \end{array}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kWh/yr | MT/yr |  |  |  |
| Junior College <br> (2Yr) | 479640 | 139.5328 | $\begin{gathered} 6.3100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.3100 \mathrm{e}- \\ 003 \end{gathered}$ | 140.0795 |
| Total |  | 139.5328 | $\begin{gathered} 6.3100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.3100 \mathrm{e}- \\ 003 \end{gathered}$ | 140.0795 |

### 6.0 Area Detail

### 6.1 Mitigation Measures Area

## West Hills CCD Lemoore - Kings County, Annual

Use Electric Lawnmower
Use Electric Leafblower
Use Electric Chainsaw

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Mitigated | - 0.1933 | 0.0000 | $3.8000 \mathrm{e}-$ 004 | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | $7.4000 \mathrm{e}-$ 004 | $7.4000 \mathrm{e}-1$ 004 | 0.0000 | 0.0000 | $\begin{gathered} 7.9000 \mathrm{e}- \\ 004 \end{gathered}$ |
| Unmitigated | - 0.1933 | 0.0000 | $\begin{aligned} & 3.9000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | $7.5000 \mathrm{e}-$ 004 | $7.5000 \mathrm{e}-$ 004 | 0.0000 | 0.0000 | $8.0000 \mathrm{e}-$ 004 |

West Hills CCD Lemoore - Kings County, Annual

### 6.2 Area by SubCategory

## Unmitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Architectural Coating | 0.0292 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Consumer Products | 0.1640 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping | $\begin{aligned} & 4.0000 \mathrm{e}- \\ & 005 \end{aligned}$ | 0.0000 | $\begin{gathered} 3.9000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | $\begin{gathered} 7.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 7.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.0000 | $\begin{gathered} 8.0000 \mathrm{e}- \\ 004 \end{gathered}$ |
| Total | 0.1933 | 0.0000 | $\begin{gathered} 3.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | $\begin{gathered} 7.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 7.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.0000 | $\begin{aligned} & \hline 8.0000 \mathrm{e}- \\ & 004 \end{aligned}$ |

Mitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Architectural Coating | 0.0292 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Consumer Products | 0.1640 |  |  |  |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping | $3.0000-$ 005 | 0.0000 | $3.8000 \mathrm{e}-$ 004 | 0.000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | $7.4000-$ 004 | $7.4000 \mathrm{e}-$ 004 | 0.0000 | 0.0000 | $7.9000 \mathrm{e}-$ 004 |
| Total | 0.1933 | 0.0000 | $\begin{aligned} & 3.8000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 |  | 0.0000 | 0.0000 |  | 0.0000 | 0.0000 | 0.0000 | $\begin{aligned} & 7.4000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 7.4000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.0000 | $\begin{aligned} & 7.9000 \mathrm{e}- \\ & 004 \end{aligned}$ |

7.0 Water Detail

### 7.1 Mitigation Measures Water

|  | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: |
| Category | MT/yr |  |  |  |
| Mitigated | 7.1771 | 0.0674 | ${ }^{1.65000-}$ | 9.3532 |
| Unmitigated | 7.1771 | 0.0674 | ${ }^{1.65000}$ | 9.3532 |

### 7.2 Water by Land Use Unmitigated

|  | Indoor/Out door Use | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Mgal | MT/yr |  |  |  |
| Junior College (2Yr) | $\begin{aligned} & 2.06006 / \\ & 3.22214 \end{aligned}$ | 7.1771 | 0.0674 | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 9.3532 |
| Total |  | 7.1771 | 0.0674 | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 9.3532 |

### 7.2 Water by Land Use

Mitigated

|  | $\begin{array}{\|l\|} \hline \text { Indoor/Out } \\ \text { door Use } \end{array}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Mgal | MT/yr |  |  |  |
| Junior College (2Yr) | $\begin{aligned} & 2.06006 / \\ & 3.22214 \\ & \hline \end{aligned}$ | 7.1771 | 0.0674 | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 9.3532 |
| Total |  | 7.1771 | 0.0674 | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 9.3532 |

### 8.0 Waste Detail

8.1 Mitigation Measures Waste

## Category/Year



### 8.2 Waste by Land Use

Unmitigated

|  | Waste <br> Disposed | Total CO2 | CH4 | N2O | CO2e |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | tons | $\mathrm{MT} / \mathrm{yr}$ |  |  |  |  |  |
| Junior College <br> $(2 Y r)$ | 54.6 |  | 11.0833 | 0.6550 | 0.0000 |  |  |
| Total |  | 11.0833 | 0.6550 | 0.0000 | 27.4584 |  |  |

## Mitigated

|  | Waste <br> Disposed | Total CO2 | CH4 | N2O | CO2e |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | tons | $\mathrm{MT} / \mathrm{yr}$ |  |  |  |  |
| Junior College <br> $(2 Y r)$ | 54.6 |  | 11.0833 | 0.6550 | 0.0000 |  |
| Total |  | 11.0833 | 0.6550 | 0.0000 | 27.4584 |  |

### 9.0 Operational Offroad

| Equipment Type | Number | Hours/Day | Days/Year | Horse Power | Load Factor | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

### 10.0 Stationary Equipment

Fire Pumps and Emergency Generators

| Equipment Type | Number | Hours/Day | Hours/Year | Horse Power | Load Factor | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Boilers

| Equipment Type | Number | Heat Input/Day | Heat Input/Year | Boiler Rating | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: |

User Defined Equipment

| Equipment Type | Number |
| :--- | :--- |

### 11.0 Vegetation

Project: West Hills CCD Lemoore SPAL
Land Use Subtype: Junior College (2-year)
Key

| Data from CalEEMod or client | value |
| :---: | :---: |
| Data entered in CalEEMod | value |

Weekly Trips

| Weekday Trip Rate ${ }^{1}$ (trips/size <br> unit) | Saturday Trip Rate ${ }^{1}$ <br> (trips/size unit) | Sunday Trip Rate ${ }^{1}$ <br> (trips/size unit) | \# of Size Unit | Total Weekly ${ }^{2}$ <br> Trips | Total Annual <br> Trips |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 24.10 | 24.10 | 24.10 | 42 | 7,084 | 368,368 |

1.Weekly trip rate provided by traffic engineer.
2. Total Weekly Trips $=\left[\left(\right.\right.$ Trip Rate $\left._{\text {weekday }} \times 5\right)+$ Trip Rate Saturday + Trip Rate $\left._{\text {Sunday }}\right] *$ Land Use $_{i}$

2. Trip purpose assumed to be $100 \%$ primary trips.
3. Trip percentage breakdown based on number of each trip type provided by traffic engineer
Annual VMT

| Annual Trips by Type |  |  | Average Trip Length $^{1}$ |  |  |  | Annual VMT $^{2}$ |  |  | Total Annual |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C-C | C-W | C-NW | C-C | C-W | C-NW | C-C | C-W | C-NW | VMT |  |
| 305,032 | 57,876 | 5,460 | 4.84 | 9.30 | 47.60 | $1,476,355$ | 538,247 | 259,896 | $2,274,498$ |  |


2. VMT = (Number of Trips xAverage Trip Length)

Default Vehicle Fleet Mix

| Category | Vehicle Type |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LDA | LDT1 | LDT2 | MDV | LHD1 | LHD2 | MHD | HHD | OBUS | UBUS | MCY | SBUS | MH | Total |
| Default Fleet Mix | 0.508492 | 0.027097 | 0.151146 | 0.105962 | 0.015839 | 0.00408 | 0.011483 | 0.165636 | 0.001689 | 0.001606 | 0.005452 | 0.000904 | 0.000613 | 0.999999 |
| Annual VMT by Vehicle Type | 1,156,564 | 61,632 | 343,781 | 241,010 | 36,026 | 9,280 | 26,118 | 376,739 | 3,842 | 3,653 | 12,401 | 2,056 | 1,394 | 2,274,495 |

## Heavy Heavy Duty (HHD) VMT Adjustmen

| Weekly Trips ${ }^{1}$ | Trip Length (miles) ${ }^{\mathbf{2}}$ | Total Annual Trips | Total Annual <br> VMT | Annual VMT to <br> Adjust |
| :---: | :---: | :---: | :---: | :---: |
| 105 | 47.60 | 5,460 | 259,896 | 116,843 |

der

## VMT Adjustment

Annual VMT to Adjust

1. HHD VMT to Adjust plus MDV, LHD1, LHD2, MHD, OBUS, UBUS, MCY, SBUS, MH VMT

| Category | Vehicle Type |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LDA | LDT1 | LDT2 | Total |
| Default Annual VMT | 1,156,564 | 61,632 | 343,781 | 1,561,977 |
| Additional VMT | 335,144 | 17,859 | 99,619 | 452,622 |
| Total VMT | 1,491,707 | 79,492 | 443,400 | 2,014,599 |


| Category | Vehicle Type |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LDA | LDT1 | LDT2 | MDV | LHD1 | LHD2 | MHD | HHD | OBUS | UBUS | MCY | SBUS | MH | Total |
| Annual VMT by Vehicle Type | 1,491,707 | 79,492 | 443,400 | 0 | 0 | 0 | 0 | 259,896 | 0 | 0 | 0 | 0 | 0 | 2,274,495 |
| Fleet Mix | 0.655841 | 0.034949 | 0.194945 | 0.000000 | 0.000000 | 0.000000 | 0.000000 | 0.114265 | 0.000000 | 0.000000 | 0.000000 | 0.000000 | 0.000000 | 1.000000 |

## West Hills CCD Lemoore - BAU - Kings County, Annual

## West Hills CCD Lemoore - BAU

## Kings County, Annual

### 1.0 Project Characteristics

1.1 Land Usage

| Land Uses | Size | Metric | Lot Acreage | Floor Surface Area | Population |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Junior College (2Yr) | 42.00 | 1000 sqft | 0.96 | $42,000.00$ | $\vdots$ |

### 1.2 Other Project Characteristics

| Urbanization | Rural | Wind Speed (m/s) | 2.2 | Precipitation Freq (Days) |
| :--- | :--- | :--- | :--- | :--- |
| Climate Zone | 3 |  | Operational Year |  |

### 1.3 User Entered Comments \& Non-Default Data

Project Characteristics -
Land Use -
Construction Phase -

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| Table Name | Column Name | Default Value | New Value |
| :---: | :---: | :---: | :---: |
| tblConstructionPhase | PhaseEndDate | 6/23/2004 | 6/9/2004 |
| tblConstructionPhase | PhaseEndDate | 6/9/2004 | 5/26/2004 |
| tblConstructionPhase | PhaseEndDate | 1/21/2004 | 1/7/2004 |
| tblConstructionPhase | PhaseEndDate | 6/16/2004 | 6/2/2004 |
| tblConstructionPhase | PhaseEndDate | 1/19/2004 | 1/5/2004 |
| tbiConstructionPhase | PhaseStartDate | 6/17/2004 | 6/3/2004 |
| tblConstructionPhase | PhaseStartDate | 1/22/2004 | 1/8/2004 |
| -------------- | PhaseStartDate | 1/20/2004 | 1/6/2004 |
| tblConstructionPhase | PhaseStartDate | 6/10/2004 | 5/27/2004 |
| tblConstructionPhase | PhaseStartDate | 1/17/2004 | 1/5/2004 |
|  | UrbanizationLevel | Urban | Rural |

### 2.0 Emissions Summary

### 2.1 Overall Construction

## Unmitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 <br> Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2004 |  |  |  |  |  |  |  |  |  |  | 0.0000 | 86.9835 | 86.9835 | 0.0218 | 0.0000 | 87.5293 |
| Maximum |  |  |  |  |  |  |  |  |  |  | 0.0000 | 86.9835 | 86.9835 | 0.0218 | 0.0000 | 87.5293 |

## Mitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2004 |  |  |  |  |  |  |  |  |  | ' | 0.0000 | 86.9834 | 86.9834 | 0.0218 | 0.0000 | 87.5293 |
| Maximum |  |  |  |  |  |  |  |  |  |  | 0.0000 | 86.9834 | 86.9834 | 0.0218 | 0.0000 | 87.5293 |


|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{array}{r} \text { PM2.5 } \\ \text { Total } \end{array}$ | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Percent Reduction | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

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| Quarter | Start Date | End Date | Maximum Unmitigated ROG + NOX (tons/quarter) | Maximum Mitigated ROG + NOX (tons/quarter) |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Highest |  |  |

### 2.2 Overall Operational

 Unmitigated Operational|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Area |  |  |  |  |  |  |  |  |  |  | 0.0000 | 7.5000e- | $\begin{aligned} & 7.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 0.0000 | $\begin{aligned} & 8.4000 \mathrm{e}- \\ & 004 \end{aligned}$ |
| Energy |  |  |  |  |  |  |  |  |  |  | 0.0000 | ${ }^{189.0427}$ | 189.0427 | 7.2600 e 003 | $2.2100 \mathrm{e}-$ 003 | 189.8836 |
| Mobile |  |  |  |  |  |  |  |  |  |  | 0.0000 | $\left.\right\|_{7} ^{1,721.268}$ | ${ }_{\text {1,721.268 }}^{7}$ | 0.7143 | 0.0000 | $\begin{gathered} 1,739.125 \\ \hline \end{gathered}$ |
| Waste |  |  |  |  |  |  |  |  |  |  | 11.0833 | 0.0000 | 11.0833 | 0.6550 | 0.0000 | 27.4584 |
| Water |  |  |  |  |  |  |  |  |  |  | 0.6536 | 6.5235 | 7.1771 | 0.0674 | $\begin{aligned} & 1.6500 \mathrm{e}- \\ & 003 \end{aligned}$ | 9.3532 |
| Total |  |  |  |  |  |  |  |  |  |  | 11.7369 | $\begin{array}{\|c\|} \hline 1,916.835 \\ 7 \end{array}$ | $\begin{gathered} 1,928.572 \\ 5 \end{gathered}$ | 1.4439 | $\begin{gathered} 3.8600 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1,965.821 \\ 2 \end{gathered}$ |

### 2.2 Overall Operational

Mitigated Operational


### 3.0 Construction Detail

## Construction Phase

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| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Site Preparation | :Site Preparation | 11/5/2004 | 1/5/2004 |  |  |  |
| 2 | Grading | Grading | 1/6/2004 | 1/7/2004 |  | 2 |  |
| 3 | Building Construction | Building Construction | 1/8/2004 | 5/26/2004 |  | 100 |  |
| 4 | Paving | Paving | 5/27/2004 | 6/2/2004 | 5 | 5 |  |
| 5 | Architectural Coating | :Architectural Coating | ;-6/3/2004 | ;6/9/2004 |  | 5' |  |

## Acres of Grading (Site Preparation Phase): 0.5

Acres of Grading (Grading Phase): 0

## Acres of Paving: 0

Residential Indoor: 0; Residential Outdoor: 0; Non-Residential Indoor: 63,000; Non-Residential Outdoor: 21,000; Striped Parking Area: 0 (Architectural Coating - sqft)

OffRoad Equipment

West Hills CCD Lemoore - BAU - Kings County, Annual

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Architectural Coating | Air Compressors | 1 | 6.00! | 78' | 0.48 |
| Paving | Cement and Mortar Mixers | 4 | 6.00 | 91 | 0.56 |
| Grading | Concrete/Industrial Saws | 1 | 8.00 | 81! | 0.73 |
| Building Construction | Cranes | 1 | 4.00 | 2311 | 0.29 |
| Building Construction | Forklifts | 2 | 6.00 | 891 | 0.20 |
| Site Preparation | Graders | 1 | 8.00 | 187! | 0.41 |
| Paving | Pavers | 1 | 7.00 | 130 | 0.42 |
| Paving | Rollers | 1 | 7.00 | 80 | 0.38 |
| Grading | Rubber Tired Dozers | 1 | 1.00 | 247 | 0.40 |
| Building Construction | Tractors/Loaders/Backhoes | 2 | 8.00 | 97! | 0.37 |
| Grading | Tractors/Loaders/Backhoes | 2 | 6.00 | 97! | 0.37 |
| Paving | Tractors/Loaders/Backhoes | 1 | 7.00 | 97! | 0.37 |
| Site Preparation | Tractors/Loaders/Backhoes | 1 | 8.00 | 97! | 0.37 |

Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation |  | 5.00 | 0.00 | 0.00 | 16.80 | 6.60 | 20.0 | D_Mix | HDT_Mix | HHDT |
| Grading |  | 10.00 | 0.00 | 0.00 | 16.80 | 6.60 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Building Construction |  | 18.0 | 7.0 | 0.00 | 16.80 | 6.6 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Paving | - 7 | 18.00 | 0.00 | 0.00 | 16.80 | 6.60 | 20.00 | D_Mix | HDT_Mix | HHDT |
| Architectural Coating | 1 | 4.00 | 0.00 | 0.00 | 16.80 | 6.60 | 20.00 | D_Mix | :HDT_Mix | HHDT |

### 3.1 Mitigation Measures Construction

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### 3.2 Site Preparation - 2004

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.5117 | 0.5117 | $1.0000 \mathrm{e}-$ 004 | 0.0000 | 0.5143 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.5117 | 0.5117 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.5143 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | $\begin{gathered} \text { Fugitive } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |  |
| Vendor |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0327 | 0.0327 | 1.0000 e 005 | 0.0000 | 0.0328 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0327 | 0.0327 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.0328 |

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3.2 Site Preparation - 2004

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.5117 | 0.5117 | 1.0000 e 004 | 0.0000 | 0.5143 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.5117 | 0.5117 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.5143 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0327 | 0.0327 | $1.0000 \mathrm{e}-$ | 0.0000 | 0.0328 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0327 | 0.0327 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.0328 |

### 3.3 Grading - 2004

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \hline \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dus |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road |  |  |  |  |  |  |  |  |  |  | 0.0000 | 1.1395 | 1.1395 | 3.0000e- | 0.0000 | 1.1469 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 1.1395 | 1.1395 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.1469 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 Total | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.1308 | 0.1308 | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.1314 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.1308 | 0.1308 | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.1314 |

3.3 Grading-2004

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road |  |  |  |  |  |  |  |  |  |  | 0.0000 | 1.1395 | 1.1395 | 3.0000 e 004 | 0.0000 | 1.1469 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 1.1395 | 1.1395 | $\begin{gathered} 3.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 1.1469 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.1308 | 0.1308 | 2.0000e- | 0.0000 | 0.1314 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.1308 | 0.1308 | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.1314 |

West Hills CCD Lemoore - BAU - Kings County, Annual

### 3.4 Building Construction-2004

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road |  |  |  |  |  |  |  |  |  |  | 0.0000 | 60.0010 | 60.0010 | 0.0150 | 0.0000 | 60.3765 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 60.0010 | 60.0010 | 0.0150 | 0.0000 | 60.3765 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling |  |  |  |  |  |  |  |  |  | , | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor |  |  |  |  |  |  |  |  |  | ' | 0.0000 | 9.2908 | 9.2908 | $3.3500 \mathrm{e}-$ 003 | 0.0000 | 9.3745 |
| Worker |  |  |  |  |  |  |  |  |  | , | 0.0000 | 11.7711 | 11.7711 | $\begin{gathered} 2.0500 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | -71.8223 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 21.0619 | 21.0619 | $\begin{aligned} & 5.4000 \mathrm{e}- \\ & 003 \end{aligned}$ | 0.0000 | 21.1968 |

West Hills CCD Lemoore - BAU - Kings County, Annual

### 3.4 Building Construction-2004 Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road |  |  |  |  |  |  |  |  |  |  | 0.0000 | 60.0009 | 60.0009 | 0.0150 | 0.0000 | 60.3764 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 60.0009 | 60.0009 | 0.0150 | 0.0000 | 60.3764 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N 2 O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor |  |  |  |  |  |  |  |  |  |  | 0.0000 | 9.2908 | 9.2908 | $3.3500 e-$ 003 | 0.0000 | 9.3745 |
| Worker |  |  |  |  |  |  |  |  |  |  | 0.0000 | 11.7711 | 11.7711 | $\begin{gathered} 2.0500 \mathrm{e} \\ 003 \end{gathered}$ | 0.0000 | 11.8223 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 21.0619 | 21.0619 | $\begin{gathered} 5.4000 \mathrm{e}- \\ 003 \end{gathered}$ | 0.0000 | 21.1968 |

3.5 Paving - 2004

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road |  |  |  |  |  |  |  |  |  |  | 0.0000 | 2.7483 | 2.7483 | $\begin{gathered} 6.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 2.7654 |
| Paving |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 2.7483 | 2.7483 | $\begin{gathered} 6.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 2.7654 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.5886 | 0.5886 | $\begin{gathered} 1.0000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.5911 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.5886 | 0.5886 | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 0.5911 |

3.5 Paving - 2004

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \hline \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road |  |  |  |  |  |  |  |  |  |  | 0.0000 | 2.7483 | 2.7483 | $\begin{gathered} 6.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 2.7654 |
| Paving |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 2.7483 | 2.7483 | $\begin{gathered} 6.9000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 2.7654 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.5886 | 0.5886 | $1.0000 \mathrm{e}-$ | 0.0000 | 0.5911 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.5886 | 0.5886 | $\begin{aligned} & 1.0000 \mathrm{e}- \\ & 004 \end{aligned}$ | 0.0000 | 0.5911 |

West Hills CCD Lemoore - BAU - Kings County, Annual

### 3.6 Architectural Coating - 2004

## Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 <br> Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Archit. Coating |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.6383 | 0.6383 | $1.8000 \mathrm{e}-$ 004 | 0.0000 | 0.6428 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.6383 | 0.6383 | $\begin{gathered} 1.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.6428 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling |  |  |  |  |  |  |  |  |  | , | 0.0000 | , 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor |  |  |  |  |  |  |  |  |  | ' | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker |  |  |  |  |  |  |  |  |  | , | 0.0000 | 0.1308 | 0.1308 | $\begin{gathered} 2.0000 \mathrm{e} \\ 005 \end{gathered}$ | 0.0000 | 0.1314 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.1308 | 0.1308 | $\begin{gathered} 2.0000 \mathrm{e}- \\ 005 \end{gathered}$ | 0.0000 | 0.1314 |

### 3.6 Architectural Coating - 2004

## Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \hline \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Archit. Coatin |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.6383 | 0.6383 | $1.8000 \mathrm{e}-$ | 0.0000 | 0.6428 |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.6383 | 0.6383 | $\begin{gathered} 1.8000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.6428 |

## Mitigated Construction Off-Site



### 4.0 Operational Detail - Mobile

### 4.1 Mitigation Measures Mobile

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | PM10 <br> Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Mitigated |  |  |  |  |  |  |  |  |  |  | 0.0000 | ${ }^{1,721.268}$ | ${ }^{1,721.268} 7$ | 0.7143 | 0.0000 | ${ }_{\text {1,739. }}^{2}$ |
| Unmitigated |  |  |  |  |  |  |  |  |  |  | 0.0000 | :1,721.268 | ${ }_{7}^{1,721.268}$ |  | 0.0000 | $\begin{gathered} 1,739.125 \\ \hline 1 \end{gathered}$ |

### 4.2 Trip Summary Information

|  | Average Daily Trip Rate |  | Unmitigated |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Weekday | Saturday | Sunday | Mitigated |  |
| Junior College (2Yr) | $1,154.58$ | 1471.66 | 50.82 | $:$ | Annual VMT |
| Total | $1,154.58$ | 471.66 | 50.82 | $2,184,963$ | $2,184,963$ |

### 4.3 Trip Type Information

|  | Miles |  |  | Trip \% |  |  | Trip Purpose \% |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW | Primary | Diverted | Pass-by |
| Junior College (2Yr) | 14.70 | 6.60 | 6.60 | 6.40 | 88.60 | 5.00 | 92 | 7 | 1 |

### 4.4 Fleet Mix

| Land Use | LDA | LDT1 | LDT2 | MDV | LHD1 | LHD2 | MHD | HHD | OBUS | UBUS | MCY | SBUS | MH |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Junior College (2Yr) | 0.404531 | 0.053546 | 0.13225 | 0.18420 | 0.04410 | 0.00567 | 0.01463 | 0.14812 | 0.00133 | 0.00275 | 0.0058 | 0.00122 | 0.001758 |

### 5.0 Energy Detail

Historical Energy Use: N

### 5.1 Mitigation Measures Energy

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Electricity Mitigated |  |  |  |  |  |  |  |  |  |  | 0.0000 | ${ }^{139.5328}$ | 139.5328 | $6.3100 \mathrm{e}-$ 003 | $1.3100 \mathrm{e}-$ 003 | 140.0795 |
| Electricity Unmitigated |  |  |  |  |  |  |  |  |  |  | 0.0000 | ${ }^{139.5328}$ | 139.5328 | 6.3100e- | 1.3100 e 003 | 140.0795 |
| $\begin{aligned} & \text { NaturalGas } \\ & \text { Mitigated } \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | 0.0000 | 49.5099 | 49.5099 | 9.5000e- | 9.1000 e 004 | -79.8041 |
| NaturalGas Unmitigated |  |  |  |  |  |  |  |  |  |  | 0.0000 | -79.5099 | 49.5099 | $\begin{gathered} 9.5000-\overline{e-} \\ 004 \end{gathered}$ | $\begin{gathered} 9.1000 \mathrm{e} \\ 004 \end{gathered}$ | 49.8047 |

West Hills CCD Lemoore - BAU - Kings County, Annual

### 5.2 Energy by Land Use - NaturalGas Unmitigated

|  | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{gathered} \text { Exhaust } \\ \text { PM2.5 } \end{gathered}$ | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU/yr | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Junior College (2Yr) | 927780 |  |  |  |  |  |  |  |  |  |  | 0.0000 | 49.5099 | 49.5099 | $\begin{aligned} & 9.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 49.8041 |
| Total |  |  |  |  |  |  |  |  |  |  |  | 0.0000 | 49.5099 | 49.5099 | $\begin{aligned} & 9.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 49.8041 |

## Mitigated

|  | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU/yr | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Junior College (2Yr) | 927780 |  |  |  |  |  |  |  |  |  |  | 0.0000 | 49.5099 | 49.5099 | $\begin{aligned} & 9.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{aligned} & 9.1000 \mathrm{e}- \\ & 004 \end{aligned}$ | 49.8041 |
| Total |  |  |  |  |  |  |  |  |  |  |  | 0.0000 | 49.5099 | 49.5099 | $\begin{gathered} 9.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{gathered} 9.1000 \mathrm{e}- \\ 004 \end{gathered}$ | 49.8041 |

### 5.3 Energy by Land Use - Electricity

Unmitigated

|  | Electricity Use | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kWh/yr | MT/yr |  |  |  |
| Junior College (2Yr) | 479640 | ${ }^{139.5328}$ | $\begin{gathered} 6.3100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.3100 \mathrm{e}- \\ 003 \end{gathered}$ | 140.0795 |
| Total |  | 139.5328 | $\begin{gathered} 6.3100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.3100 \mathrm{e}- \\ 003 \end{gathered}$ | 140.0795 |

## Mitigated

|  | Electricity Use | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kWh/yr | MT/yr |  |  |  |
| Junior College (2Yr) | 479640 | 139.5328 | $\begin{gathered} 6.3100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.3100 \mathrm{e}- \\ 003 \end{gathered}$ | 140.0795 |
| Total |  | 139.5328 | $\begin{gathered} 6.3100 \mathrm{e}- \\ 003 \end{gathered}$ | $\begin{gathered} 1.3100 \mathrm{e}- \\ 003 \end{gathered}$ | 140.0795 |

### 6.0 Area Detail

### 6.1 Mitigation Measures Area

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \hline \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Mitigated |  |  |  |  |  |  |  |  |  |  | 0.0000 | [ 7.5000 e | $\begin{gathered} 7.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.0000 | $\begin{gathered} 8.4000 \mathrm{e}- \\ 004 \end{gathered}$ |
| Unmitigated |  |  |  |  |  |  |  |  |  |  | 0.0000 | 7.5000 e 004 | 7.5000 e 004 | 0.0000 | 0.0000 | $\begin{aligned} & 8.4000 \mathrm{e}- \\ & 004 \end{aligned}$ |

### 6.2 Area by SubCategory

## Unmitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Architectural Coating |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Consumer Products |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping |  |  |  |  |  |  |  |  |  |  | 0.0000 | $\begin{aligned} & : \quad 7.5000 \mathrm{e}- \\ & 004 \end{aligned}$ | $\begin{gathered} 7.5000 \mathrm{e} \\ 004 \end{gathered}$ | 0.0000 | 0.0000 | $\begin{gathered} 8.4000 \mathrm{e}- \\ 004 \end{gathered}$ |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | $\begin{array}{\|c\|} \hline 7.5000 \mathrm{e}- \\ 004 \end{array}$ | $\begin{gathered} 7.5000 \mathrm{e}- \\ 004 \end{gathered}$ | 0.0000 | 0.0000 | $\begin{gathered} 8.4000 \mathrm{e}- \\ 004 \end{gathered}$ |

### 6.2 Area by SubCategory

 Mitigated|  | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Architectural Coating |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Consumer Products |  |  |  |  |  |  |  |  |  |  | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping |  |  |  |  |  |  |  |  |  |  | 0.0000 | $7.5000 \mathrm{e}-$ 004 | $7.5000 \mathrm{e}-$ 004 | 0.0000 | 0.0000 | $\begin{aligned} & 8.4000 \mathrm{e}- \\ & 004 \end{aligned}$ |
| Total |  |  |  |  |  |  |  |  |  |  | 0.0000 | $\begin{gathered} 7.5000 \mathrm{e}- \\ 004 \end{gathered}$ | $\begin{array}{\|c} 7.5000 \mathrm{e}- \\ 004 \end{array}$ | 0.0000 | 0.0000 | $\begin{gathered} 8.4000 \mathrm{e}- \\ 004 \end{gathered}$ |

### 7.0 Water Detail

7.1 Mitigation Measures Water

|  | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: |
| Category | MT/yr |  |  |  |
| Mitigated | 7.1771 |  | $1.6500 \mathrm{e}-$ 003 | 9.3532 |
| Unmitigated | $7.1771$ | $0.0674$ | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 9.3532 |

### 7.2 Water by Land Use

## Unmitigated

|  | Indoor/Out door Use | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Mgal | MT/yr |  |  |  |
| Junior College (2Yr) | $\begin{aligned} & \hline 2.06006 / \\ & 3.22214 \\ & \hline \end{aligned}$ | 7.1771 | 0.0674 | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 9.3532 |
| Total |  | 7.1771 | 0.0674 | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 9.3532 |

### 7.2 Water by Land Use

Mitigated

|  | Indoor/Out door Use | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Mgal | MT/yr |  |  |  |
| Junior College (2Yr) | $\begin{aligned} & 2.06006 / \\ & 3.22214 \\ & \hline \end{aligned}$ | 7.1771 | 0.0674 | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 9.3532 |
| Total |  | 7.1771 | 0.0674 | $\begin{gathered} 1.6500 \mathrm{e}- \\ 003 \end{gathered}$ | 9.3532 |

### 8.0 Waste Detail

8.1 Mitigation Measures Waste

## Category/Year



### 8.2 Waste by Land Use

Unmitigated

|  | Waste <br> Disposed | Total CO2 | CH4 | N2O | CO2e |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | tons | $\mathrm{MT} / \mathrm{yr}$ |  |  |  |  |  |
| Junior College <br> $(2 Y r)$ | 54.6 |  | 11.0833 | 0.6550 | 0.0000 |  |  |
| Total |  | 11.0833 | 0.6550 | 0.0000 | 27.4584 |  |  |

## Mitigated

|  | Waste Disposed | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | tons | MT/yr |  |  |  |
| Junior College (2Yr) | 54.6 | 11.0833 | 0.6550 | 0.0000 | 27.4584 |
| Total |  | 11.0833 | 0.6550 | 0.0000 | 27.4584 |

### 9.0 Operational Offroad

| Equipment Type | Number | Hours/Day | Days/Year | Horse Power | Load Factor | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

### 10.0 Stationary Equipment

Fire Pumps and Emergency Generators

| Equipment Type | Number | Hours/Day | Hours/Year | Horse Power | Load Factor | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Boilers

| Equipment Type | Number | Heat Input/Day | Heat Input/Year | Boiler Rating | Fuel Type |
| :---: | :---: | :---: | :---: | :---: | :---: |

User Defined Equipment

| Equipment Type | Number |
| :---: | :---: |

### 11.0 Vegetation

## APPENDIX B. TOXIC EMISSIONS AND PRIORITIZATION

## West Hills CCD Lemoore SPAL

HHD Diesel Particulate Matter
Based on:

| Trips/Year: | 5,475 | (15 trips per day $\times 365$ days/year) |
| :---: | :---: | :--- |
| Miles/Trip: | 0.5 | (on-site distance for HHD trucks) |
| Miles/Year: | 2,738 |  |


|  | PM10 $^{\mathbf{1}}$ |
| :---: | :---: |
| Em. Factor (grams/mile) | $1.32 \mathrm{E}-02$ |
| $\mathrm{Lbs} /$ Mile $^{2}$ | $2.91 \mathrm{E}-05$ |
| $\mathrm{Lbs} /$ Year |  |

1. EMFAC PM10 emission factor for 2024 T7 Single vehicle category.
2. Assume total DPM is equivalent to total PM10.

# Max Prioritization <br> for <br> CEQA West Hills CCD (C-1) 

| Grouped Facilities: None |  |  |  |  | Options Selected: |  | $\square$ 2,500 m Distance Limit |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Area Name: No Sub-Areas Identified Receptor: Stack Table Distance |  |  |  |  |  |  | Remove Pollutants $<1 / 2$ the Applicable Degree of Accuracy |  |  |
| Toxic Device \#: 1 <br> Device Name: HHD Trucks <br> Receptor Distance (m): 0 <br> Greater Than 2500m $\square$ |  |  |  | Emissions and Potency Method <br> Prioritization Scores |  |  | Dispersion Adjustment Method <br> Prioritization Scores |  |  |
| CAS NUMBER POLLUTANT NAME | PROID | LBS/YEAR | LBS/HOUR | CANCER | CHRONIC | ACUTE | CANCER | CHRONIC | ACUTE |
| 9901 Diesel engine exhaust, particulate matt | 1 | 7.97E-02 | 0.00E+00 | 1.84E-01 | $2.73 \mathrm{E}-04$ |  | 3.06E-03 | 4.55E-06 |  |
|  |  | TOTALS FOR DEVICE 1 |  | $1.84 \mathrm{E}-01$ | $2.73 \mathrm{E}-04$ |  | 3.06E-03 | $4.55 \mathrm{E}-06$ |  |
|  |  | Total For Area: |  | 1.84E-01 | $2.73 \mathrm{E}-04$ |  | 3.06E-03 | $4.55 \mathrm{E}-06$ |  |

Emissions and Potency

## Method

Prioritization Scores


CANCER
$1.84 \mathrm{E}-01$
2.73E-04

Dispersion Adjustment
Method
Prioritization Scores
CANCER CHRONIC ACUTE

CHRONIC ACUTE
3.06E-03 4.55E-06

TS = Total Score
$\mathrm{t}=\quad$ Specific Toxic Substance
EYR $=$ Emissions in lbs / year
EHR = Emissions in Maximum lbs / hour for Acute and
Average lbs / hour for Chronic
NF $=\quad$ Normalization Factor $($ Cancer $=128$, Acute $=25$, Chronic $=2.5)$
URF = Unit Risk Factor
AREL = Acute Reference Exposure Level
CREL = Chronic Reference Exposure Level
SHA $=$ Stack Height Adjustment ( $<20 \mathrm{~m}=60,<45 \mathrm{~m}=9,>=45 \mathrm{~m}=1$ )
RP $=$ Receptor Proximity Adjustment Factor
$R=\quad$ Receptor Distance
H = Stack Height

| For Stacks $0 \mathrm{~m}<=\mathrm{H}<20 \mathrm{~m}$ |  | For Stacks $20 \mathrm{~m}<=\mathrm{H}<45 \mathrm{~m}$ |  | For Stacks $->=\mathrm{H}<45 \mathrm{~m}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R | RP | R | RP | R | RP |
| $0 \mathrm{~m}<\mathrm{R}<100 \mathrm{~m}$ | 1.0 | $0 \mathrm{~m}<\mathrm{R}<100 \mathrm{~m}$ | 1.0 | $0 \mathrm{~m}<\mathrm{R}<100 \mathrm{~m}$ | 1.0 |
| $100 \mathrm{~m}<\mathrm{R}<250 \mathrm{~m}$ | 0.25 | $100 \mathrm{~m}<\mathrm{R}<250 \mathrm{~m}$ | 0.85 | $100 \mathrm{~m}<\mathrm{R}<250 \mathrm{~m}$ | 1.0 |
| $250 \mathrm{~m}<\mathrm{R}<500 \mathrm{~m}$ | 0.04 | $250 \mathrm{~m}<\mathrm{R}<500 \mathrm{~m}$ | 0.22 | $250 \mathrm{~m}<\mathrm{R}<500 \mathrm{~m}$ | 0.90 |
| $500 \mathrm{~m}<\mathrm{R}<1000 \mathrm{~m}$ | 0.011 | $500 \mathrm{~m}<\mathrm{R}<1000 \mathrm{~m}$ | 0.064 | $500 \mathrm{~m}<\mathrm{R}<1000 \mathrm{~m}$ | 0.40 |
| $1000 \mathrm{~m}<\mathrm{R}<1500 \mathrm{~m}$ | 0.003 | $1000 \mathrm{~m}<\mathrm{R}<1500 \mathrm{~m}$ | 0.018 | $1000 \mathrm{~m}<\mathrm{R}<1500 \mathrm{~m}$ | 0.13 |
| $1500 \mathrm{~m}<\mathrm{R}<2000 \mathrm{~m}$ | 0.002 | $1500 \mathrm{~m}<\mathrm{R}<2000 \mathrm{~m}$ | 0.009 | $1500 \mathrm{~m}<\mathrm{R}<2000 \mathrm{~m}$ | 0.066 |
| $\mathrm{R}>2000 \mathrm{~m}$ | 0.001 | $\mathrm{R}>2000 \mathrm{~m}$ | 0.006 | $\mathrm{R}>2000 \mathrm{~m}$ | 0.042 |

Cancer Score:

$$
\operatorname{TS}(\mathrm{t})=\operatorname{EYR}(\mathrm{t}) * \operatorname{URF}(\mathrm{t}) * R P * S H A * 128
$$

Acute Score:

$$
\operatorname{TS}(\mathrm{t})=[\operatorname{EHR}(\mathrm{t}) / \operatorname{AREL}(\mathrm{t})] * R P * S H A * 25
$$

Chronic Score:
$\mathrm{TS}(\mathrm{t})=[\operatorname{EYR}(\mathrm{t}) / \operatorname{CREL}(\mathrm{t})] * R P * 150 * S H A * 2.5\}$

ApPENDIX B
Cultural Memorandum

## TECHNICAL MEMORANDUM

Date: December 7, 2020
Project: Cultural resources records search- West Hills Community College Lemoore Campus Institutional Center Project, City of Lemoore, Kings County, CA (200400)

To: Jaymie Brauer, Principal Planner
From: Robert Parr, MS, RPA, Senior Archaeologist
Subject: Cultural Resources Records Search Results (RS\#20-429)

## Background

This cultural resources records search (RS \#20-429) was conducted at the Southern San Joaquin Valley Information Center, CSU Bakersfield for the above referenced Project in the City of Lemoore, Kings County to determine whether any known cultural resources were located on or near the proposed project that might be impacted by project development and activities.

## Location

The Project located on Bush St and College Ave and is within Section 8, T19S R20E, MDB\&M and in the Lemoore USGS quadrangle (Figures 1-4).

## Project Description

The West Hills Community College District is proposing to construct a 42,000 square foot, 2 story Instructional Center (IC) on an undeveloped but disturbed portion of the existing campus. The proposed expansion is anticipated to increase the overall student population by approximately 5 percent. The IC will be used to expand education opportunities in the areas of allied health services, computer science and graphic arts.

## Results

The records search covered an area within one-half mile of the Project and included a review of the National Register of Historic Places, California Points of Historical Interest, California Registry of Historic Resources, California Historical Landmarks, California State Historic Resources Inventory, and a review of cultural resource reports on file.

The records search indicated that the subject property had never been surveyed for cultural resources and it is not known if any exist there.

Five cultural resource studies have been conducted within a half mile of the property (Hatoff et al. 1995; Love and Tang 2002a, 2002b; Varner 2003; Girado and Orfila 2009). Only one cultural

## TECHNICAL MEMORANDUM

resource, a segment of the historic route of the Southern Pacific Railroad (now the San Joaquin Valley Railroad) (P-16-000122), has been identified within a half mile of the proposed project. However, the Project will not impact this resource.

A Sacred Lands File request was also submitted to the Native American Heritage Commission. A response dated December 18, 2020 indicates negative results (see Attachment B).

## Conclusions

Based on the results of cultural records search findings and the lack of archaeological resources previously identified within a half mile radius of the proposed Project, the potential to encounter subsurface cultural resources is minimal. Additionally, the Project construction would be conducted within the developed and previously disturbed roadways and road easements. The potential to uncover subsurface historical or archaeological deposits is would be considered unlikely.

However, there is still a possibility that historical or archaeological materials may be exposed during construction. Grading and trenching, as well as other ground-disturbing actions have the potential to damage or destroy these previously unidentified and potentially significant cultural resources within the project area, including historical or archaeological resources. Disturbance of any deposits that have the potential to provide significant cultural data would be considered a significant impact. To reduce the potential impacts of the Project on cultural resources, the following measures are recommended. With implementation of CUL-1 and CUL-2, the Project would have a less than significant impact related to cultural resources.

CUL-1: If prehistoric or historic-era cultural materials are encountered during construction activities, all work in the immediate vicinity of the find shall halt until a qualified archaeologist can evaluate the find and make recommendations. Cultural resource materials may include prehistoric resources such as flaked and ground stone tools and debris, shell, bone, ceramics, and fire-affected rock as well as historic resources such as glass, metal, wood, brick, or structural remnants. If the qualified archaeologist determines that the discovery represents a potentially significant cultural resource, additional investigations may be required to mitigate adverse impacts from Project implementation. These additional studies may include avoidance, testing, and evaluation or data recovery excavation. Implementation of the mitigation measure below would ensure that the proposed Project would not cause a substantial adverse change in the significance of a historical resource.

CUL-2: If human remains are discovered during construction or operational activities, further excavation or disturbance shall be prohibited pursuant to Section 7050.5 of the California Health and Safety Code. The specific protocol, guidelines, and channels of communication outlined by

## TECHNICAL MEMORANDUM

the Native American Heritage Commission, in accordance with Section 7050.5 of the Health and Safety Code, Section 5097.98 of the Public Resources Code (Chapter 1492, Statutes of 1982, Senate Bill 297), and Senate Bill 447 (Chapter 44, Statutes of 1987), shall be followed. Section $7050.5(\mathrm{c})$ shall guide the potential Native American involvement, in the event of discovery of human remains, at the direction of the county coroner.

(s) Robert E. Parr, MS, RPA

Senior Archaeologist

## Attachment A- Figures

Attachment B- Sacred Lands File Response by the Native American Heritage Commission

## TECHNICAL MEMORANDUM

## References

(all reports on file at the Southern San Joaquin Valley Information Center, California State University, Bakersfield)

Girado, Amy and Rebecca S. Orfila
2009 A Cultural Resources Assessment of Approximately 70 Acres of Land for the City Lemoore Arsenic Mitigation Program, Kings County, California. (KI-00191)

Hatoff, Brian, Barb Voss, Sharon Waechter, Vance Benté, and Stephen Wee 1995 Cultural Resources Inventory Report for the Proposed Mojave Northward Expansion Project. (KI-00028)

Love, Bruce and Bai "Tom" Tang
2002a Archaeological Survey Report: Cross Valley Rail Corridor Project Between the Cities of Visalia and Huron, Tulare, Kings, and Fresno Counties, California. (KI-00110).

2002b Historic Study Report/Historical Resources Evaluation Report: Cross Valley Rail Corridor Project Between the Cities of Visalia and Huron, Tulare, Kings, and Fresno Counties, California. (KI-00111)

Varner, Dudley M.
2003 A Cultural Resource Study for the Tachi Yokuts Cultural Center Project, West Hills Community College Districy, Lemoore Campus, Kings County, California. (KI-00140)

## ATTACHMENT A PROJECT FIGURES






## TECHNICAL MEMORANDUM

Attachment BSacred Lands File Response by the Native American Heritage Commission

CHAIRPERSON
Laura Miranda
Luiseño

VICE CHAIRPERSON Reginald Pagaling Chumash

## SEC RETARY

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Luiseño

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Wintun

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# NATIVE AMERIC AN HERITAGE COMMISSION 

December 18, 2020

Jaymie Braver
Quad Knopf, Inc.

Via Email to: jaymie.brauer@qkinc.com

Re: Native Americ an Tibal Consultation, Pursuant to the Assembly Bill 52 (AB 52), Amendments to the Califomia Environmental Quality Act (CEQA) (Chapter 532, Statutes of 2014), Public Resources Code Sections 5097.94 (m), 21073, 21074, 21080.3.1, 21080.3.2, 21082.3, 21083.09, 21084.2 and 21084.3, West Hills Community College District Leemore Campus Construction Project, Kings County

DearMs. Braver:

Pursuant to Public Resourc es Code section 21080.3 .1 (c ), attached is a c onsulta tion list of tribes that a re traditionally a nd culturally a ffilia ted with the geogra phic a rea of the above-listed project. Please note that the intent of the AB 52 amendments to CEQA is to a void and/or mitigate impacts to tribal cultural resources, (Pub. Resources Code §21084.3 (a)) ("Public a genc ies shall, when feasible, a void damaging effects to a ny tribal cultural resource.")

Public Resources Code sections 21080.3.1 and 21084.3(c) require CEQA lead agencies to consult with Califomia Native American tribes that have requested notice from such agencies of proposed projects in the geographic a rea that are tra ditionally and culturally affilia ted with the tribes on projects for which a Notice of Preparation or Notice of Negative Declaration or Mitigated Negative Declaration has been filed on or afterJ uly 1, 2015. Specifically, Public Resources Code section 21080.3.1 (d) provides:

Within 14 days of determining that an application for a project is complete or a decision by a public agency to undertake a project, the lead agency shall provide formal notification to the designated contact of, or a tribal representa tive of, tra ditionally a nd culturally affiliated Califomia Native American tribes that have requested notice, which shall be accomplished by means of at least one written notific ation that includes a brief description of the proposed project and its location, the lead agency contact information, and a notific ation that the Califomia Native American tribe has 30 days to request consultation pursuant to this section.

The AB 52 a mendments to CEQA law does not preclude initiating consultation with the tribes that a re culturally and tra ditionally affilia ted within your jurisdiction prior to receiving requests for notific ation of projects in the tribe's a reas of traditional a nd cultural affiliation. The Native American Heritage Commission (NAHC) recommends, but does not require, ea rly consultation as a best practice to ensure that lead agencies receive sufficient information about cultural resources in a project area to avoid damaging effects to tribal cultural resources.

The NAHC a lso recommends, but does not require that agencies should a lso include with their notific a tion letters, information rega rding a ny cultural resources assessment that has been completed on the area of potential effect (APE), such as:

1. The results of any record search that may have been conducted at an Information Center of the Califomia Historic al Resources Information System (CHRIS), including, but not limited to:

- A listing of any and all known cultural resources that have already been recorded on or adjacent to the APE, such as known archa eologic al sites;
- Copies of any and all cultural resource records and study reports that may have been provided by the Information Center as part of the records search response;
- Whether the records search indicates a low, moderate, or high probability that unrecorded cultural resources are located in the APE; and
- If a survey is recommended by the Information Center to detemmine whether previously unrecorded cultural resources are present.

2. The results of a ny archa eological inventory survey that was conducted, including:

- Any report that may conta in site forms, site signific ance, a nd suggested mitigation measures.

All information regarding site locations, Native American human remains, and associated funerary objects should be in a separate confidential addendum, and not be made available for public disclosure in accordance with Govemment Code section 6254.10.
3. The result of a ny Sacred Lands File (SLF) check conducted through the Native American Herita ge Commission was negative.
4. Any ethnographic studies conducted for any a rea including all or part of the APE; and
5. Any geotec hnical reports regarding a ll or part of the APE.

Lead a gencies should be a ware that records mainta ined by the NAHC a nd CHRIS are not exha ustive a nd a negative response to these searches does not preclude the existence of a tribal cultural resource. A tribe may be the only source of information regarding the existence of a tribal cultural resource.

This information will a id tribes in determining whether to request formal consultation. In the event that they do, having the information beforehand will help to facilita te the consultation process.

If you receive notification of change of addresses and phone numbers from tribes, please notify the NAHC. With your a ssistance, we can assure that our consulta tion list rema ins current.

If you have any questions, please contact me at my email address: Nancy.Gonzalez-Lopez@nahc.ca.gov.
Sincerely,


Cultural Resources Analyst

Attachment

# Native American Heritage Commission <br> Tribal Consultation List <br> December 18, 2020 

| Kings River Choinumni Farm Tribe |  |
| :--- | :--- |
| Stan Alec |  |
| 3515 East Fedora Avenue | Foothill Yokuts |
| Fresno $\quad$ CA 93726 | Choinumni |
| (559) 647-3227 Cell |  |


| Wuksache Indian Tribe/Eshom Vallev Band |  |
| :--- | :--- |
| Kenneth Woodrow. Chairberson |  |
| 1179 Rock Haven Ct. | Foothill Yokuts |
| Salinas CA 93906 | Mono |
| kwood8934@aol.com | Wuksache |

(831) 443-9702

Table Mountain Rancheria
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(559) 822-2587

Table Mountain Rancheria
Bob Pennell. Cultural Resources Director
P.O. Box 410 Yokuts

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rpennell@tmr.org
(559) 325-0351
(559) 217-9718 - cell

Tule River Indian Tribe
Neil Pevron. Chairperson
P.O. Box 589

Yokuts
Porterville , CA 93258
neil.peyron@tulerivertribe-nsn.gov
(559) 781-4271

December 10, 2020
FROM: West Hills Community College District
RE: Tribal Cultural Resources under the California Environmental Quality Act, AB 52 (Gatto, 2014). A Formal Notification of a Decision to Undertake a Project and Notification of Consultation Opportunity, pursuant to Public Resources Code § 21080.3.1 (hereafter PRC).

## Dear Chairperson:

The West Hills Community College District (District) has decided to undertake the West Hills- Lemoore Campus Construction Project (Project) in the City of Lemoore, California. The District is designated as Lead Agency under the California Environmental Quality Act (CEQA).

The project site is located on the West Hills Community College- Lemoore campus on the northwest corner of Pederson Avenue and College Avenue in the City of Lemoore, Kings County, CA. The project site is within a portion of Assessor's Parcel Numbers 023-510-018, which totals approximately 27.1 acres in area, Section 8, Township 19S, Range 20E, MMB\&M.

The District is proposing to construct a 42,000 square foot, two-story Instructional Center (IC) and ancillary parking on an undeveloped but disturbed portion of the existing Lemoore campus. Figure 1 shows the regional location and Figure 2 shows the Project's aerial location. Figure 3 shows the PLSS/USGS quadrangle and Figure 4 shows the topography of the site.

No new construction would occur outside of the existing campus footprint. The College has a current student enrollment of 4,600 students and the proposed expansion is anticipated to increase the overall student population by approximately 5 percent or approximately 232 students. The IC will be used to expand education opportunities in the areas of allied health services, computer science and graphic arts.

Pursuant to PRC § 21080.3.1 (b), you have 30 days from the receipt of this letter to request consultation, in writing, with the West Hills Community College District.

Should you have any comments or questions please contact our designated representative, Jaymie L. Brauer at (661) 616-2600 or at jaymie.brauer@ QKinc.com.

Very Respectfully,

## Richard Storti

Richard Storti
Deputy Chancellor- Business Services

[^2]
## ATTACHMENT A PROJECT FIGURES






Appendix C
Geotechnical Report

# GEOTECHNICAL ENGINEERING INVESTIGATION REPORT AND GEOLOGIC AND SEISMIC HAZARDS EVALUATION PROPOSED STUDENT CENTER WEST HILLS COLLEGE, LEMOORE LEMOORE, CALIFORNIA 

## BSK G11-003-11B

Prepared for:

AP Architects, Inc.
3434 Truxtun Avenue, Suite 240
Bakersfield, CA 93301

June 6, 2010

## VIA US MAIL \& EMAIL

June 6, 2011

Ms. Celina Garcia
AP Architects, Inc.
3434 Truxtun Avenue, Suite 240
Bakersfield, CA 93301

# SUBJECT: Geotechnical Engineering Investigation and Geologic / Seismic Hazards Evaluation Proposed Student Center West Hills College, Lemoore Lemoore, California 

Dear Ms. Garcia:
BSK Associates (BSK) has completed the geotechnical investigation and geologic and seismic hazards evaluation for the proposed West Hills College Student Center in Lemoore, California. The geotechnical investigation, which included a field exploration, laboratory testing program, engineering analysis, and preparation of this report, was conducted in accordance with our proposal BSK GB10-5306, dated December 6, 2010. The enclosed report provides geotechnical recommendations for use in preparation of plans and specifications for the subject project. Appendix C provides the Geologic and Seismic Hazards Evaluation.
We appreciate the opportunity to assist you during the design phase of your project and look forward to continuing our relationship on this project through construction. If you have any questions, please contact us.

Respectfully submitted, BK ASSOCIATES


Karl Schwartz, EIT. Staff Engineer


On Man Leu, P.E., G.E. Bakersfield Branch Manager


Martin B. Cline, C.E.G.
Senior Engineering Geologist

## Distribution: Client (4 Originals, Email: [cgarcia@addington.net]) BSK File (1 original + E-Copy)

[^3]
## TABLE OF CONTENTS

Page
1.0 INTRODUCTION ..... 1
1.1 Planned Construction ..... 1
1.2 Purpose And Scope Of Services ..... 1
2.0 FIELD INVESTIGATION AND LABORATORY TESTING ..... 2
2.1 Field Exploration ..... 2
2.2 Laboratory Testing ..... 2
3.0 SITE CONDITIONS ..... 2
3.1 Overview of Geologic Setting .....  2
3.2 Site Description and Surface Conditions ..... 2
3.3 Subsurface Conditions .....  2
3.4 Groundwater Conditions ..... 3
3.5 Seismically Induced Settlement ..... 3
4.0 CONCLUSIONS AND RECOMMENDATIONS ..... 3
4.1 Seismic Design Criteria ..... 4
4.2 Soil Corrosivity ..... 4
4.3 Site Preparation and Earthwork Construction ..... 5
4.4 Foundations ..... 6
4.5 Lateral Earth Pressures and Frictional Resistance ..... 6
4.6 Excavation Stability ..... 7
4.7 Pipe Bedding and Envelope ..... 8
4.8 Trench Backfill and Compaction ..... 8
4.9 Concrete Slabs-on-Grade ..... 8
4.10 Surface Drainage Control ..... 10
5.0 PLANS AND SPECIFICATIONS REVIEW ..... 10
6.0 CONSTRUCTION TESTING AND OBSERVATIONS ..... 10
7.0 LIMITATIONS ..... 11

# TABLE OF CONTENTS (Continued) 

## TABLES

Table 1: $\quad$ Seismic Design Parameters
Table 2: $\quad$ Recommended Static Lateral Earth Pressures
Table 3: Recommended Pavement Structural Section

## APPENDICES

Appendix A: Field Exploration
Figure A-1: Site Vicinity Map
Figure A-2: $\quad$ Boring Location Map
Table A-1: Consistency of Coarse-Grained Soil by Sampler Blow Count
Table A-2: Consistency of Fine-Grained Soil by Sampler Blow Count
Figure A-3: Boring Log Legend
Boring Logs: Borings B-1 through B-8

Appendix B: Laboratory Testing
Table B-1: $\quad$ Summary of Corrosion Test Results
Table B-2: Summary of \#200 Wash results
Table B-3: Relative Compaction of Existing Building Pad
Figures B-1 and B-2: Direct Shear Tests
Figures B-3 and B-4: Consolidation Tests
Figure B-5: Expansion Index Test
Figure B-6: Modified Proctor Test

Appendix C: Geologic and Seismic Hazards Evaluation

# GEOTECHNICAL ENGINEERING INVESTIGATION REPORT AND GEOLOGIC AND SEISMIC HAZARDS EVALUATION PROPOSED STUDENT CENTER WEST HILLS COLLEGE, LEMOORE <br> LEMOORE, CALIFORNIA 

### 1.0 INTRODUCTION

This report presents the results of a Geotechnical Engineering Investigation and Geologic \& Seismic Hazards Evaluation conducted by BSK Associates (BSK) for the proposed West Hills College, Lemoore Student Center (Site). The Site is located southeast of the intersection of Bush Street and College Avenue in Lemoore, California as shown on the Site Vicinity Map, Figure A-1. The geotechnical engineering investigation was conducted in accordance with BSK Proposal GB105306, dated December 6, 2010.

This report provides a description of the geotechnical conditions at the site and provides specific recommendations for earthwork and foundation design with respect to the planned building. In the event that changes occur in the design of the project, this report's conclusions and recommendations will not be considered valid unless the changes are reviewed with BSK and the conclusions and recommendations are modified or verified in writing. Examples of such changes would include location, size of structures, foundation loads, basement addition, etc.

### 1.1 Planned Construction

BSK's understanding of the planned project is based on information provided from Ms. Celina Garcia with AP Architects. We understand that the proposed building will be a single story, concrete slab-on-grade structure. The building pad will be raised 5 feet to enhance constructability and provide site drainage. The building will have CMU exterior walls and light metal stud interior framing. Structural loads were provided during our investigation. Based on the information provided by AP Architects, the structural loads to be on the order of 0.36 kips per lineal foot for wall loads, and column loads on the order of 65 kips . In addition to the planned structure, concrete flat works areas are planned.

In the event that significant departures are identified between our assumed structural characteristics and foundation loading, and those reflecting the actual proposed construction, then we should be notified in writing and be given the opportunity to verify or amend this report and its recommendations to reflect the corresponding changes.

### 1.2 Purpose And Scope Of Services

The objective of this geotechnical investigation was to characterize the subsurface conditions in the areas of the proposed building and concrete flat works areas, and provide geotechnical engineering recommendations for the preparation of plans and specifications. The scope of the investigation included a field exploration, laboratory testing, engineering analyses, preparation of this report, and preparation of a geologic/seismic hazards evaluation report that is provided in Appendix C.

### 2.0 FIELD INVESTIGATION AND LABORATORY TESTING

### 2.1 FIELD Exploration

The field exploration for this investigation was conducted under the oversight of a BSK Staff Engineer. Eight (8) borings were drilled at the site between May 12 and May 19, 2011 using a truck-mounted hollow stem auger drill rig and hand auguring equipment. Four (4) CPT soundings were taken around the site to a maximum explored depth of 50 feet. The hand auger and hollow stem auger borings were drilled to depths ranging from 5 to 21.5 feet beneath the existing ground surface (bgs). The locations of the borings are indicated on the Boring Location Map, Figure A-2. Details of the field exploration and the boring logs are provided in Appendix A.

### 2.2 LABORATORY TESTING

Laboratory tests were performed on selected soil samples to evaluate moisture content, dry density, shear strength, consolidation properties, expansion potential, corrosion characteristics, fines content, and maximum dry density and optimum moisture content. A description of the laboratory test methods and results are presented in Appendix B.

### 3.0 SITE CONDITIONS

The following sections address the geologic setting, site description, surface and subsurface conditions, and groundwater conditions at the Site. This information is based on BSK's field exploration, and published maps and reports.

### 3.1 Overview of Geologic Setting

The Site is located in the southeast quarter of the northwest quarter of Section 8, Township 19 South, Range 20 East, Mount Diablo Base and Meridian. The coordinates for the site location are $36.21219^{\circ}$ North latitude and $119.82609^{\circ}$ West longitude. Appendix C provides further information on the regional geology.

### 3.2 Site Description and Surface Conditions

The Site is currently in an open field within the campus, to the south of some existing buildings. A large earth pad was placed at the location previously. The pad is about 5 feet high and covers most of the area occupied by the proposed Student Center footprint. The integrity of the pad is in question because of its observed condition. There are many animal burrows, which are located around the existing building pad, there are no compaction testing records available, and the time of construction is unknown. The in place relative compaction at the upper 4 feet of the existing pad ranged from 79 to 93 percent and the majority of the compaction results were below 90 percent (based on ASTM D1557). The results of the in place dry densities are presented in Table B-3 in Appendix B.

The rest of the site is flat with dry grass. The site is bounded by WHC, Lemoore to the north and east, and by open fields to the south and west.

### 3.3 SUBSURFACE Conditions

The soils encountered during our subsurface exploration consisted of silty sands, silty clays, clayey silts, and sandy silts. Based on the hand auguring soil boring data, the existing building pad consists primarily of silty sand. Based on hollow stem auger borings and CPT soundings, the native soil
consists primarily of silty clays and clayey silts in the upper 10 feet. The soil below 10 feet is layered sand and silt with some silty clay. The maximum explored depth was 50 feet. Based on the results of the consolidation tests, the on-site soils below 2 feet are considered to have a low potential for hydrocompaction. The upper 5 feet of the on-site soils are considered to have medium expansion potential with an expansion index of 83 . The soils were classified in the field during drilling operations. The stratification lines were approximated based on observations made at the time of drilling. The actual boundaries between different soil types may be gradual and soil conditions may vary between points of exploration. For a more detailed description of the subsurface materials encountered, the logs of the borings should be consulted Borings B-01 through B-08 in Appendix A. These logs include the soil type, color, moisture and dry density, and the applicable Unified Soil Classification Chart presented on Figure A-3. The CPT soundings can be consulted for depths greater than 16.5 feet bgs. The logs of the CPT soundings are found in Appendix C.

### 3.4 Groundwater Conditions

Groundwater was encountered in the borings during our investigation at a depth of 7 feet bgs between May 12 and May 19, 2011. To ascertain groundwater levels for the area during other times, groundwater elevation data from the California Department of Water Resources (DWR) was reviewed. Water level hydrographs from wells near the Site are presented in Appendix C. The hydrographs indicate that the historical shallowest depth to groundwater near the Site from 1950 to 2007 was approximately 6 feet bgs.

### 3.5 Seismically Induced Settlement

Our analysis indicates that during the design event, the factor of safety against liquefaction is less than a value of 1.0 (acceptable for most structures) in some minor subsurface units. Based on the limited thickness of the potential liquefiable units (less than two feet), the overall potential for significant liquefaction to occur at the Site is low.

Liquefaction analyses were performed assuming the shallowest groundwater depth of 6 feet and incorporating information from the boring logs and CPT logs. Four (4) CPT soundings were performed. The locations of the CPT soundings are presented in the Boring Location Map, Figure A-2, Appendix A.

The range of total seismically induced settlement for the MCE is approximately 1.0 to 1.4 inches and the associated differential settlement is approximately 0.4 inches spanning a distance of approximately 100 feet between CPT locations. The design standard for buildings under extreme seismic events is that they do not collapse, though they may be damaged. These magnitudes of settlement are consistent with the designs standard.

### 4.0 CONCLUSIONS AND RECOMMENDATIONS

Based upon the data collected during this investigation, and from a geotechnical engineering standpoint, it is our opinion that the geologic setting or soil conditions would not preclude the construction of the proposed improvements. The near-surface soils across the project site consist primarily of silty sands, silty clays, and clayey silts that may be considered to have favorable bearing characteristics for design purposes. However, our test borings indicate that there are localized zones of moderately expansive soils in the upper 6 feet at the site within the planned building and concrete flat works. These conditions will require localized over excavation and replacement with an
approved engineered fill pending inspection by the geotechnical engineer once the areas have been fully exposed during earthwork operations. Also, another geotechnical constraint is the shallow groundwater.

The proposed structures may be supported on reinforced concrete foundations provided that the recommendations presented herein are incorporated into the design and construction of the project.

### 4.1 SEISmic Design Criteria

There are not any known active or potentially active fault zones within 30 miles of the project site. Based on sampler blow counts and the correlated Standard Penetration Test (SPT) " N " values from our soil borings and in accordance with Table 1613.5.2 of the 2010 California Building Code (CBC), the site can be classified as Site Class D $(15 \leq \mathrm{N} \leq 50)$.
Use of the 2010 California Building Code (CBC) seismic design criteria is considered appropriate and the following parameters should be considered applicable for the structural design of structural improvements:

| Table 1: Seismic Design Parameters |  |  |  |
| :---: | :---: | :---: | :---: |
| Seismic Design Parameter | Value |  | Reference |
| MCE Mapped Spectral Acceleration $(\mathrm{g})$ | $\mathrm{S}_{\mathrm{S}}=0.81$ | $\mathrm{~S}_{1}=0.31$ | USGS Mapped <br> Value |
| Amplification Factors (Site Class D) | $\mathrm{F}_{\mathrm{a}}=1.18$ | $\mathrm{~F}_{\mathrm{v}}=1.78$ | Table 1613.5.3 |
| Site Adjusted MCE Spectral Acceleration $(\mathrm{g})$ | $\mathrm{S}_{\mathrm{MS}}=0.95$ | $\mathrm{~S}_{\mathrm{M} 1}=0.55$ | Equations 16-37, <br> 38 |
| Design Spectral Acceleration $(\mathrm{g})$ | $\mathrm{S}_{\mathrm{DS}}=0.63$ | $\mathrm{~S}_{\mathrm{D} 1}=0.37$ | Equations 16-39, <br> 40 |
| Design Peak Ground Acceleration $\left(\mathrm{S}_{\mathrm{DS}} / 2.5\right)(\mathrm{g})$ | $\mathrm{PGA}=0.25$ |  | CGS Note 48 |

As shown above, the mapped spectral acceleration parameter at 1 -second period $\left(\mathrm{S}_{1}\right)$ is less than 0.75 and is greater than 0.20 , therefore the site lies in Seismic Design Category D as specified in Section 1613.5 .6 of the 2010 CBC. Appendix C provides the complete details of the Seismic Hazard Assessment performed.

### 4.2 SoIL Corrosivity

One soil sample was analyzed to evaluate the potential for concrete deterioration or steel corrosion due to attack by soluble salts in the on-site soils. Based on the test results, native, near-surface soils have high soluble sulfate and chloride contents, a low resistivity, and are slightly basic. Native soils are generally considered to have a high corrosion potential with respect to buried concrete and metal conduits. We recommend that Type V cement be used in the formulation of concrete and buried reinforcing steel protection with a minimum concrete cover required by the American Concrete Institute (ACI) Building Code Requirements for Structural Concrete, ACI 318-95, Chapter 7.7. We recommend the use of a water/cement ratio of 0.45 . Buried metal conduits should have a protective coating in accordance with the manufacturer's specifications. If detailed recommendations for corrosion protection are desired, a corrosion specialist must be consulted.

### 4.3 Site Preparation and Earthwork Construction

The following procedures must be implemented during Site preparation for the proposed Site improvements. References to maximum dry density, optimum moisture content, and relative compaction are based on ASTM D 1557 (latest test revision) laboratory test procedures.

1. The areas of proposed improvements should be cleared of surface vegetation and debris. Materials resulting from the clearing and stripping operations should be removed and properly disposed of off-site. Removal of vegetation must be complete and include the associated root systems. The anticipated stripping depth is 4 to 6 inches. Organic rich strippings must not be used in engineered fill but may be used in landscape areas.
2. At the building pad area, based on our compaction test results, the existing pad has average compaction below 90 percent. Therefore, the existing pad should be removed. After the existing pad is removed, the site should be over-excavated to a depth of 12 inches below existing grade or 12 inches below the bottom of the footing elevation, whichever is greater. The overexcavation must extend at least five feet laterally outside the planned building.
3. Following the required stripping and over-excavation, the exposed ground surface must be inspected by the Geotechnical Engineer to evaluate if loose or soft zones are present that will require additional over excavation. Following approval by the Geotechnical Engineer, the ground surface must be scarified a depth of 8 inches, moisture conditioned to within two percent ( $2 \%$ ) of optimum moisture content, and compacted to at least 90 percent of the maximum dry density. Over-excavated areas must be backfilled with engineered fill as described below. The upper 12 inches in paved areas should be compacted to a minimum of 95 percent relative compaction.
4. Generally, the near surface on-site soils are considered to have a moderate expansion potential. At the building pad and exterior concrete flatworks, these soils may be used at a minimum of two feet below the finished pad. The existing pad material can be used as engineered fill as long as the material is placed two feet below the finished pad elevation. Imported or native excavated soils, free of organic materials or deleterious substances, may be placed as engineered fill. On-site clayey soil as engineered fill must be placed in uniform layers not exceeding 8 inches in loose thickness, moisture conditioned to within 2 to 4 percent above optimum moisture content, and compacted to at least 90 percent relative compaction. Import soil as engineered fill must be placed in uniform layers not exceeding 8 inches in loose thickness, moisture conditioned to within 2 percent of optimum moisture content, and compacted to at least 90 percent relative compaction.
5. Import fill materials must be free from organic materials or deleterious substances. The project specifications must require the contractor to contact BSK to review the proposed import fill materials for conformance with these recommendations at least one week prior to importing to the Site, whether from on-site or off-site borrow areas. Imported fill soils must be non-hazardous and derived from a single, consistent soil type source conforming to the following criteria:

| Plasticity Index: | $<12$ |
| :--- | :--- |
| Expansion Index: | $<20$ (Very Low Expansion Potential) |
| Maximum Particle Size: | 3 inches |
| Percent Passing \#4 Sieve: | $65-100$ |
| Percent Passing \#200 Sieve: | $20-45$ |
| Minimum R-value (in paved areas) | 30 |
| Low Corrosion Potential: | Soluble Sulfates $<1,500 \mathrm{ppm}$ |
|  | Soluble Chlorides $<300 \mathrm{ppm}$ |
|  | Minimum Resistivity $>5,000 \mathrm{ohm}-\mathrm{cm}$ |

6. If possible, earthwork operations should be scheduled during a dry, warm period of the year. Should these operations be performed during or shortly following periods of inclement weather, unstable soil conditions may result in the soils exhibiting a "pumping" condition. This condition is caused by excess moisture, in combination with compaction, resulting in saturation and zero air voids in the soils. If this condition occurs, the adverse soils will need to be over-excavated to the depth at which stable soils are encountered, and replaced with suitable soils compacted as engineered fill. Alternatively, the Contractor may proceed with grading operations after utilizing a method to stabilize the soil subgrade, which should be subject to review and approval by BSK prior to implementation.

### 4.4 Foundations

Provided the Site is prepared as recommended above, the proposed structures may be supported on continuous, or isolated shallow foundations bearing on engineered fill. The thickness of foundations and steel reinforcement must be designed by the Project Structural Engineer.

Continuous and isolated spread footings must have a minimum width of 12 inches and 24 inches, respectively. Spread footing foundations may be designed using a net allowable bearing pressure of 3,000 pounds per square foot ( psf ). This bearing value applies to the dead load plus live load ( $\mathrm{DL}+$ LL) condition, and may be increased by $1 / 3$ for short duration wind or seismic loads. Total foundation settlements are expected to be less than 0.5 -inches and differential settlements between similarly loaded (DL +LL ) and sized footings are anticipated to be less than 0.25 -inches. Due to the predominantly granular nature of the foundation soils, the majority of the settlement is expected to occur within a few months after the design loads are applied.

A modulus of subgrade reaction of 120 pci can be used for design.

### 4.5 Lateral Earth Pressures and Frictional Resistance

Provided the Site is prepared as recommended above, the following earth pressure parameters for footings may be used for design purposes. The parameters shown in the table below are for drained conditions of select engineered fill or undisturbed native soil.

| Table 2: Recommended Static Lateral Earth Pressures |  |
| :---: | :---: |
| Lateral Pressure Condition | Equivalent Fluid Density (pcf) <br> Drained Condition |
| Active Pressure | 35 |
| At-Rest Pressure | 55 |
| Passive Pressure | 390 |

Active pressure refers to walls that are free to rotate. At-rest pressure refers to walls that are restrained against rotation. The lateral earth pressures listed herein assume level backfill. The conventional equation for active, at-rest, and passive conditions, using soil bulk unit weights of 120 pcf are appropriate for the medium dense to dense sand and silty sand above the groundwater because undrained conditions prevail in the soil mass.

A coefficient of friction of 0.4 may be used between soil sub-grade and the bottom of footings. The coefficient of friction and passive earth pressure values given above represent ultimate soil strength values. BSK recommends that a safety factor consistent with the design conditions be included in their usage. For stability against lateral sliding that is resisted solely by the passive earth pressure against footings or friction along the bottom of footings, a minimum safety factor of 1.5 is recommended. For stability against lateral sliding that is resisted by combined passive pressure and frictional resistance, a minimum safety factor of 2.0 is recommended. For lateral stability against seismic loading conditions, a minimum safety factor of 1.2 is recommended.

### 4.6 EXCAVATION STABILITY

Soils encountered within the depth explored are generally soils Type C in accordance with OSHA (Occupational Safety and Health Administration). The slopes surrounding or along temporary excavations may be vertical for excavations that are less than five feet deep and exhibit no indication of potential caving, but should be no steeper than $1 \mathrm{H}: 1 \mathrm{~V}$ for excavations that are deeper than five feet, up to a maximum depth of 15 feet. Certified trench shields or boxes may also be used to protect workers during construction in excavations that have vertical sidewalls and are greater than 5 feet deep. Temporary excavations for the project construction should be left open for as short a time as possible and should be protected from water runoff. In addition, equipment and/or soil stockpiles must be maintained at least 10 feet away from the top of the excavations. Because of variability in soils, BSK must be afforded the opportunity to observe and document sloping and shoring conditions at the time of construction. Slope height, slope inclination, and excavation depths (including utility trench excavations) must in no case exceed those specified in local, state, or federal safety regulations, (e.g., OSHA Health and Safety Standards for Excavations, 29 CFR Part 1926, or successor regulations).

### 4.7 Pipe Bedding and Envelope

A minimum of 6 inches of bedding material is recommended for pipe installations. The bedding material and backfill within the pipe envelope (up to 12 inches above the pipe) should consist of sandy material with not more than 10 percent passing the \#200 sieve, 100 percent passing the $3 / 8$ inch sieve, and a sand equivalent of at least 30 .

In the case of flexible pipe installation, a minimum of eight inches ( 8 ") of bedding material is recommended for pipe installation. Bedding material must consist of medium- or coarse-grained sand with a Sand Equivalent of at least 25. As an alternative to using sand, the pipe bedding and envelope material may consist of Class 2 Aggregate Base as specified in Section 26 of the Caltrans Standard Specifications or sand-cement slurry that contains 1.5 to 2.0 sacks of cement per yard of material and has a 4- to 6-inch slump.

Bedding and pipe envelope must be placed in loose thickness not exceeding 10 -inches and compacted to at least 90 percent of the maximum dry density of ASTM D1557. Soil backfill moisture content during compaction must be maintained within two percent ( $2 \%$ ) of optimum. Water jetting to attain compaction should not be allowed. Class 2 Aggregate Base, when used for bedding or pipe envelope must be compacted to at least 92 percent of ASTM D1557.

### 4.8 Trench Backfill and Compaction

Processed on-site soils, which are free of organic material, are suitable for use as general trench backfill above the pipe envelope. Native soil with particles less than three inches in the greatest dimension may be incorporated into the backfill and compacted as specified above, providing they are properly mixed into a matrix of friable soils. The backfill must be placed in thin layers not exceeding 12 inches in loose thickness, be well-blended and consistent texture, moisture conditioned to at least optimum moisture content, and compacted to at least 90 percent of the maximum dry density as determined by the ASTM D1557. The uppermost 24 inches of trench backfill below pavement sections must be compacted to at least 95 percent of the maximum dry density as determined by ASTM D1557. Moisture content within two percent of optimum must be maintained while compacting this upper 24 inch trench backfill zone.

We recommend that trench backfill be tested for compliance with the recommended Relative Compaction and moisture conditions. Field density testing should conform to ASTM Test Methods D1556 or D6938. We recommend that field density tests be performed in the utility trench bedding, envelope and backfill for every vertical lift, at an approximate longitudinal spacing of not greater than 150 feet. Backfill that does not conform to the criteria specified in this section should be removed or reworked, as applicable over the trench length represented by the failing test so as to conform to BSK recommendations.

### 4.9 CONCRETE SLABS-ON-GRADE

Non-structural Concrete slab-on-grade floors must be a minimum of 4-inches thick and must be supported on a compacted subgrade prepared in accordance with Section 4.3. In order to regulate cracking of the slabs, construction joints and/or control joints must be provided in each direction at a maximum spacing of 10 feet along with steel reinforcement as recommended by the Project Structural Engineer. Control joints must have a minimum depth of one-quarter of the slab thickness.

Due to the difficulty of installing and maintaining woven or welded wire mesh (WWM) in the middle of concrete slabs-on-grade during construction, it is recommended that any steel reinforcement used in concrete slabs-on-grade consist of steel rebar.

Interior concrete slabs must be successively underlain by: $1-1 / 2$ inches of washed concrete sand; a durable vapor barrier; and a smooth, compacted subgrade surface. The vapor barrier must meet the requirements of ASTM E 1745 Class A and have a water vapor transmission rate (WVTR) of less than or equal to 0.012 Perms as tested by ASTM E 96. Examples of acceptable vapor barrier products include: Stego Wrap (15-mil) Vapor Barrier by STEGO INDUSTRIES LLC; W.R. Meadows Premoulded Membrane with Plasmatic Core; and Zero-Perm by Alumiseal. Because of the importance of the vapor barrier, joints must be carefully spliced and taped. If migration of subgrade moisture through the slab is not a concern, then the vapor barrier and overlying sand may be deleted. The building subgrade must be kept in a moist condition until the vapor barrier or concrete slab is placed. BSK's representative must be called to the Site to review soil and moisture conditions immediately prior to placing the vapor barrier or concrete slab.

As indicated in the recent PCA Engineering Bulletin 119, Concrete Floors and Moisture, and applicable ACI Committee reports (see ACI 360R-06, Design of Slabs-on-Ground, dated October 2006 and ACI 302.1R-04, Guide for Concrete Floor and Slab Construction, dated June 2004), the sand layer between the vapor barrier and concrete floor slab may be omitted. This must reduce the amount of moisture that can be transmitted through the slab (especially if the sand layer becomes very moist or wet prior to placing the concrete); however, the risk of slab "curling" is much greater. The "curling" may result from a sharp contrast in moisture-drying conditions between the exposed slab surface and the surface in contact with the membrane. As recommended in the referenced ACI Committee reports, measures must be taken to reduce the risk of "curling" such as reducing the joint spacing, using a low shrinkage mix design, and reinforcing the concrete slab. In order to regulate cracking of the slab, we recommend that full depth construction joints and control joints be provided in each direction with slab thickness and steel reinforcing recommended by the structural engineer.

Excessive landscape water or leaking utility lines could create elevated moisture conditions under concrete slabs, which could result in adverse moisture or mildew conditions in floor slabs or walls. Accordingly, care must be taken to avoid excess irrigation around the structures, as well as to periodically monitor for leaking utility lines. Likewise, positive surface drainage must be provided around the perimeter of the structures.

As indicated above, the control of the deleterious effects of moisture vapor transmission on flooring materials can be substantially improved by the use of a low porosity concrete. This can be achieved by specifying a low water: cement ratio ( 0.45 or less by weight), $4,000 \mathrm{psi}$ compressive strength at 28 days and a minimum of 7 days wet-curing.

### 4.10 Surface Drainage Control

The control of surface drainage in the project areas is an important design consideration. BSK recommends the following:

- Final grading around concrete or asphalt pavement must provide for positive and enduring drainage away from the buildings, and ponding of water must not be allowed around, near the buildings, or on any of the paved surfaces. Paved surfaces next to the buildings must have at least a 2 percent gradient away from the building.
- Landscaping must be carefully planned to provide positive and enduring drainage away from the buildings, minimize irrigation of the area within 5 feet of the buildings, and prevent saturation of the soils immediately adjacent to or below the building areas. Unpaved landscape areas must be sloped with at least a 5 percent gradient away from the building for a distance of at least 10 feet.

Irrigation water must be applied in amounts not exceeding those required to offset evaporation, sustain plant life, and maintain a relatively uniform moisture profile around the perimeter of, and below, Site improvements

### 5.0 PLANS AND SPECIFICATIONS REVIEW

BSK recommends that it be retained to review the draft plans and specifications for the project, with regard to foundations and earthwork, prior to their being finalized and issued for construction bidding.

### 6.0 CONSTRUCTION TESTING AND OBSERVATIONS

Geotechnical testing and observation during construction is a vital extension of this geotechnical investigation. BSK recommends that it be retained for those services. Field review during site preparation and grading allows for evaluation of the exposed soil conditions and confirmation or revision of the assumptions and extrapolations made in formulating the design parameters and recommendations. BSK's observations must be supplemented with periodic compaction tests to establish substantial conformance with these recommendations. BSK must also be called to the site to observe foundation excavations, prior to placement of reinforcing steel or concrete, in order to assess whether the actual bearing conditions are compatible with the conditions anticipated during the preparation of this report. BSK must also be called to the Site to observe placement of foundation and slab concrete.

If a firm other than BSK is retained for these services during construction, that firm must notify the owner, project designers, governmental building officials, and BSK that the firm has assumed the responsibility for all phases (i.e., both design and construction) of the project within the purview of the geotechnical engineer. Notification must indicate that the firm has reviewed this report and any subsequent addenda, and that it either agrees with BSK's conclusions and recommendations, or that it will provide independent recommendations.

### 7.0 LIMITATIONS

The analyses and recommendations submitted in this report are based upon the data obtained from the test borings performed at the locations shown on Figure A-2. The report does not reflect variations which may occur between or beyond the borings. The nature and extent of such variations may not become evident until construction is initiated. If variations then appear, a re-evaluation of the recommendations of this report will be necessary after performing on-site observations during the excavation period and noting the characteristics of the variations.

The validity of the recommendations contained in this report is also dependent upon an adequate testing and observation program during the construction phase. BSK assumes no responsibility for construction compliance with the design concepts or recommendations unless it has been retained to perform the testing and observation services during construction as described above.

The findings of this report are valid as of the present. However, changes in the conditions of the Site can occur with the passage of time, whether caused by natural processes or the work of man, on this property or adjacent property. In addition, changes in applicable or appropriate standards may occur, whether they result from legislation, governmental policy or the broadening of knowledge.

BSK has prepared this report for the exclusive use of the Client and members of the project design team. The report has been prepared in accordance with generally accepted geotechnical engineering practices which existed in Kings County at the time the report was written. No other warranties either expressed or implied are made as to the professional advice provided under the terms of BSK's agreement with Client and included in this report.

## Respectfully submitted

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## APPENDIX A

## Field Exploration

## APPENDIX A

## FIELD EXPLORATION

The field exploration at the Site was conducted from May 12 to May 19, 2011, under the oversight of a BSK Staff Engineer. A total of eight (8) soil borings were drilled within the planned improvements and structures. Four of the test borings were drilled to depths of approximately 5 feet bgs in areas of the existing pad. Three (3) borings were drilled to approximately 16.5 feet bgs and one (1) to approximately 21.5 feet bgs in the proposed building. Borings were drilled using a truckmounted drill rig with hollow stem auger and a hand-auger. Four (4) CPT soundings were also taken around the perimeter of the site. The approximate locations of the test borings are indicated on Figure A-2.
The soil materials encountered in the test borings were visually classified in the field, and the Staff Engineer recorded logs during the drilling and sampling operations. Visual classification of the materials encountered in the test borings was made in general accordance with the Unified Soil Classification System (ASTM D 2488). A soil classification chart is presented herein. Boring logs are presented herein and should be consulted for more details concerning subsurface conditions. Stratification lines were approximated by the field staff based on observations made at the time of drilling, while the actual boundaries between soil types may be gradual and soil conditions may vary at other locations.

Subsurface samples were obtained at the successive depths shown on the boring logs by driving samplers which consisted of a 2.5 -inch inside diameter (I.D.) California Sampler and a 1.4-inch I.D. Standard Penetration Test (SPT) Sampler. The samplers were driven 18 inches using a 140-pound hammer dropped from a height of 30 inches by means of either an automatic hammer or a down-hole "safety hammer". The number of blows required to drive the last 12 inches was recorded as the blow count (blows/foot) on the boring logs. The relatively undisturbed soil core samples were capped at both ends to preserve the samples at their natural moisture content. Soil samples were also obtained using the SPT Sampler lined with metal tubes or unlined in which case the samples were placed and sealed in polyethylene bags. At the completion of the field exploration, the test borings were backfilled with the excavated soil cuttings.

It should be noted that the use of terms such as "loose", "medium dense", "dense" or "very dense" to describe the consistency of a soil is based on sampler blow count and is not necessarily reflective of the in-place density or unit weight of the soils being sampled. The relationship between sampler blow count and consistency is provided in the following Tables A-1 and A-2 for coarse-grained (sandy and gravelly) soils and fine grained (silty and clayey) soils, respectively.


Map Reference:. 3-D TopoQuads Copyright 2009 Delorme Yarmouth, ME 04096 Source Data: USGS Setail: 13-1 Datum: WGS84



| Table A-1: Consistency of Coarse-Grained Soil by Sampler Blow Count |  |  |
| :---: | :---: | :---: |
| Consistency Descriptor | SPT Blow Count <br> (\#Blows / Foot) | 2.5" I.D. California Sampler <br> Blow Count (\#Blows / Foot) |
| Very Loose | $<4$ | $<6$ |
| Loose | $4-10$ | $6-15$ |
| Medium Dense | $10-30$ | $15-45$ |
| Dense | $30-50$ | $45-80$ |
| Very Dense | $>50$ | $>80$ |


| Table A-2: Consistency of Fine-Grained Soil by Sampler Blow Count |  |  |
| :---: | :---: | :---: |
| Consistency Descriptor | SPT Blow Count <br> (\#Blows / Foot) | 2.5" I.D. Cal. Sampler Blow Count <br> (\# Blows / Foot) |
| Very Soft | $<2$ | $<3$ |
| Soft | $2-4$ | $3-6$ |
| Medium Stiff | $4-8$ | $6-12$ |
| Stiff | $8-15$ | $12-24$ |
| Very Stiff | $15-30$ | $24-45$ |
| Hard | $>30$ | $>45$ |


| MAJOR DIVISIONS |  |  |  | TYPICAL NAMES |
| :---: | :---: | :---: | :---: | :---: |
|  | GRAVELS <br> MORE THAN HALF COARSE FRACTION IS LARGER THAN NO. 4 SIEVE | CLEAN GRAVELS WITH LITTLE OR NO FINES | GW | WELL GRADED GRAVELS, GRAVEL-SAND MIXTURES |
|  |  |  | GP 0 | POORLY GRADED GRAVELS, GRAVEL- SAND MIXTURES |
|  |  | GRAVELS WITH OVER 15\% FINES | GM ${ }^{\circ}$ | SILTY GRAVELS, POORLY GRADED GRAVEL-SAND-SILT MIXTURES |
|  |  |  | GC 5:O | CLAYEY GRAVELS, POORLY GRADED GRAVEL-SAND-CLAY MIXTURES |
|  | SANDS <br> MORE THAN HALF COARSE FRACTION IS SMALLER THAN NO. 4 SIEVE | CLEAN SANDS WITH LITTLE OR NO FINES | SW : | WELL GRADED SANDS, GRAVELLY SANDS |
|  |  |  | SP Y | POORLY GRADED SANDS, GRAVELLY SANDS |
|  |  | SANDS WITH OVER 15\% FINES | SM | SILTY SANDS, POORLY GRADED SAND-SILT MIXTURES |
|  |  |  | SC | CLAYEY SANDS, POORLY GRADED SAND-CLAY MIXTURES |
|  | SILTS AND CLAYS LIQUID LIMIT LESS THAN 50 |  | ML | INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS, OR CLAYEY SILTS WITH SLIGHT PLASTICITY |
|  |  |  | CL | INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, lean clays |
|  |  |  | $\mathrm{OL}=$ | ORGANIC CLAYS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY |
|  | SILTS AND CLAYS |  | MH | INORGANIC SILTS , MICACEOUS OR DIATOMACIOUS FINE SANDY OR SILTY SOILS, ELASTIC SILTS |
|  |  |  | $\mathrm{CH}$ | INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS |
|  | LIQUID LIMIT GREATER THAN 50 |  | $\mathrm{OH}$ | ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS |
| HIGHLY ORGANIC SOILS |  |  | Pt | PEAT AND OTHER HIGHLY ORGANIC SOILS |

Note: Dual symbols are used to indicate borderline soil classifications.

| $\boldsymbol{\square}$ | Pushed Shelby Tube | RV | R -Value |
| :---: | :---: | :---: | :---: |
| 区 | Standard Penetration Test | SA | Sieve Analysis |
|  | Modified California | SW | Swell Test |
| [] | Auger Cuttings | TC | Cyclic Triaxial |
| 囬 | Grab Sample | TX | Unconsolidated Undrained Triaxial |
|  | Sample Attempt with No Recovery | TV | Torvane Shear |
| CA | Chemical Analysis | UC | Unconfined Compression |
| CN | Consolidation | (1.2) | (Shear Strength, ksf) |
| CP | Compaction | WA | Wash Analysis |
| DS | Direct Shear | (20) | (with \% Passing No. 200 Sieve) |
| PM | Permeability | $\nabla$ | Water Level at Time of Drilling |
| PP | Pocket Penetrometer | I | Water Level after Drilling (with date measured) |

SOIL CLASSIFICATION CHART AND KEY TO TEST DATA Unified Soil Classification System


PLATE: Figure A-3

LOG OF BORING NO. B-02

BSK
Associates
Engineerg Laboratories
BSK \& ASSOCIATES 700 22nd street
Bakersfield CA 93301
Telephone: 661-327-0671

| Project Name: | WHC, Lemoore |
| :--- | :--- |
| Location: | Lemoore, California |
| Job Number: | G11 003 10B |

Job Number: G11 003 10B

LOG OF BORING NO. B-03

BSK
Associates
Engineerg Laboratories
BSK \& ASSOCIATES 700 22nd street
Bakersfield CA 93301
Telephone: 661-327-0671
Project Name: WHC, Lemoore Location: Lemoore, California
Job Number: G11 003 10B

LOG OF BORING NO. B-04

BSK
Associates
Engineerg Laboratories
BSK \& ASSOCIATES 700 22nd street
Bakersfield CA 93301
Telephone: 661-327-0671
Project Name: WHC, Lemoore
Location: Lemoore, California
Job Number: G11 003 10B


BSK
Associates Engineergy ${ }^{\text {Caboratories }}$
BSK \& ASSOCIATES 700 22nd street
Bakersfield CA 93301 Telephone: 661-327-0671

LOG OF BORING NO. B-05

## Project Name: WHC, Lemoore <br> Location: Lemoore, California <br> Job Number: G11 003 10B



BSK
Associates
Engineergy ${ }^{\text {abboratories }}$
BSK \& ASSOCIATES 700 22nd street
Bakersfield CA 93301 Telephone: 661-327-0671

LOG OF BORING NO. B-06

## Project Name: WHC, Lemoore <br> Location: Lemoore, California <br> Job Number: G11 003 10B



BSK
Associates Engineerg Laboratories
BSK \& ASSOCIATES
700 22nd street
Bakersfield CA 93301
Telephone: 661-327-0671

LOG OF BORING NO. B-08

BSK
Associates
Engineerg Laboratories
BSK \& ASSOCIATES 700 22nd street
Bakersfield CA 93301
Telephone: 661-327-0671

## Project Name: WHC, Lemoore Location: Lemoore, California

Job Number: G11 003 10B


## APPENDIX B

## Laboratory Testing Results

## APPENDIX B

## LABORATORY TESTING

## Moisture-Density Tests

The field moisture content, as a percentage of dry weight of the soils, was determined by weighing the samples before and after oven drying in accordance with ASTM D 2216 test procedures. Dry densities, in pounds per cubic foot, were also determined for undisturbed core samples in general accordance with ASTM D 2937 test procedures. Test results are presented on the boring logs in Appendix A.

## Direct Shear Test

Two direct shear tests were performed on in-situ soil samples from selected boring. The tests were conducted to determine the soil strength characteristics. The standard test method is ASTM D 3080, Direct Shear Test for Soil under Consolidated Drained Conditions. The results of the direct shear test results are presented graphically on Figures B-1 and B-2.

## Consolidation Test

Two consolidation tests were performed on relatively undisturbed soil sample to evaluate compressibility and collapse potential characteristics. The test was performed in general accordance with ASTM D 2435. The sample was initially loaded under as-received moisture content to a selected stress level, was then saturated, and then incrementally loaded up to a maximum load of 5200 psf. The test results are presented on Figures B-3 and B-4.

## Expansion Index Test

One Expansion Index Test was performed on a bulk soil sample in an area beneath planned building slab or foundations. The test was performed in general accordance with UBC Standard 18-1. The results of the test are presented on Figure B-5.

## Soil Corrosivity

The results of chemical analyses performed on a selected soil sample using EPA Test Methods 300.0 (for soluble sulfate and chlorides) and 9045C (for pH ) are presented below.

| Table B-1: Summary of Corrosion Test Results |  |
| :---: | :---: |
| Sample Location | B-5 @ 0' -5 ' bgs |
| pH | 8 |
| Sulfate, ppm | 250 |
| Chloride, ppm | 100 |

## Minus \#200 Sieve Analysis

The fines content (amount of silt and clay) of four soil samples was evaluated by performing minus \#200 sieve analysis in accordance with ASTM D 1140 test procedures. The results of these tests are presented in Table B-2.

| Table B-2: Summary of Minus \#200 Sieve Wash Test Results |  |
| :---: | :---: |
| Location | Percentage Passing |
| B-05 @ 5 feet bgs | 43 |
| B-06 @ 10 feet bgs | 70 |
| B-07 @ 15 feet bgs | 42 |
| B-08 @ 2 feet bgs | 56 |

## Maximum Density and Optimum Moisture Content

One (1) bulk sample was tested in accordance with the Modified Proctor Method (ASTM D 1557) to determine the maximum dry density and optimum moisture content. The results of the tests are presented on Figure B-6. The maximum dry density was used to evaluate the relative compaction of the existing building pad based on in-place density tests. The results of these tests are presented in Table B-3.

| Table B-3: Relative Compaction of Existing Building Pad |  |  |  |
| :---: | :---: | :---: | :---: |
| Location | Dry Density <br> $\left(\mathrm{lb} / \mathrm{ft}^{3}\right)$ | Maximum <br> Dry Density <br> $\left(\mathrm{lb} / \mathrm{ft}^{3}\right)$ | Relative <br> Compaction (\%) |
| B-01 @ 2 feet bgs | 116 | 127 | 91 |
| B-01 @ 4 feet bgs | 114 | 127 | 90 |
| B-02 @ 2 feet bgs | 103 | 127 | 81 |
| B-02 @ 4 feet bgs | 103 | 127 | 81 |
| B-03 @ 2 feet bgs | 118 | 127 | 93 |
| B-03 @ 4 feet bgs | 105 | 127 | 83 |
| B-04 @ 2 feet bgs | 100 | 127 | 79 |
| B-04 @ 4 feet bgs | 107 | 127 | 84 |

BSK PROJECT:
PROJECT NUMBER:
SAMPLE ID:
DRY DENSITY (pcf):
MOISTURE CONTENT (\%):
INTERNAL FRICTION ANGLE, $\varphi$ (degrees)
COHESION, c (ksf):

WHC, Lemoore Student Center
G1100311B
B-06 @ 5 feet bgs
112
19
32
0.40


Figure B-1

BSK PROJECT:
PROJECT NUMBER:
SAMPLE ID:
DRY DENSITY (pcf):
MOISTURE CONTENT (\%):
INTERNAL FRICTION ANGLE, $\varphi$ (degrees)
COHESION, c (ksf):

WHC, Lemoore Student Center
G1100311B
B-08 @ 5 feet bgs
100
23


Figure B-2


Figure B-3


Figure B-4

## EXPANSION INDEX OF SOILS

## ASTM D 4829 / UBC STANDARD 18-2

Project Name: WHC, Lemoore Student Center

| Project Number: | G11-003-11B |  | Sample Date: $5 / 19 / 2011$ <br> Lab Tracking ID: |
| :--- | :--- | :--- | :--- |
| Test Date: $5 / 27 / 2011$ |  |  |  |
| Sample Location: | B-05 @ 0-5' |  |  |
| Sample Source | Native |  |  |
| Sampled By: | K. Schwartz | Tested By: N. Rossiter | Reviewed By: On Man Lau |

TEST DATA

| INITIAL SET-UP DATA |  | FINAL TAKE-DOWN DATA |  |  |
| ---: | :---: | ---: | :---: | :---: |
| Sample + Tare Weight (g) | 681.3 | Sample + Tare Weight (g) | 203.0 |  |
| Tare Weight (g) | 283.7 | Tare Weight (g) |  | 0.0 |
| Moisture Content Data |  | Wet Weight + Tare |  | 203.0 |
| Wet Weight + Tare | 402.7 | Dry Weight + Tare | 184.1 |  |
| Dry Weight + Tare | 366.8 | Tare Weight (g) | 0.0 |  |
| Tare Weight (g) | 0 | Moisture Content (\%) | $10.3 \%$ |  |
| Moisture Content (\%) | $9.8 \%$ | Final Volume (ft ${ }^{3}$ ) | 0.007878 |  |
| Initial Volume (ft $\left.{ }^{3}\right)$ | 0.007272 | Final Wet Density (pcf) | 56.8 |  |
| Remolded Wet Density (pcf) | 120.5 | Final Dry Density (pcf) | 51.5 |  |
| Remolded Dry Density (pcf) | 109.8 | Degree of Saturation | 12 |  |
| Degree of Saturation | 49 |  |  |  |

EXPANSION READINGS

| Initial Gauge Reading (in) | 0.0233 |
| :---: | :---: |
| Final Gauge Reading (in) | 0.1066 |
| Expansion (in) | 0.0833 |


| Uncorrected Expansion Index | 83 |
| :---: | :---: |
| Corrected Expansion Index, El | 83 |

Classification of Expansive Soil

| El | Potential Expansion |
| :---: | :---: |
| $0-20$ | Very Low |
| $21-50$ | Low |
| $51-90$ | Medium |
| $91-130$ | High |
| $>130$ | Very High |

Remarks: The material has medium expansion potential.

BSK PROJECT:
PROJECT NUMBER:
SAMPLE ID:
MAXIMUM DRY DENSITY (pcf):
OPTIMUM MOISTURE CONTENT (\%):
TEST DESIGNATION:

WHC Lemoore Student Center
G1100311B
B-05 @ 0-5'
127
10
ASTM D1557


Figure B-6

## APPENDIX C

## Geologic and Seismic Hazards Investigation

## Appendix C

Geologic/Seismic Hazard Investigation<br>Lemoore Student Center<br>West Hills College<br>Lemoore, California

BSK JOB G1100311B

June 6, 2011
Page
C1.0 INTRODUCTION ..... 1
C1.1 Objective and Scope of Services ..... 1
C1.2 Site Location ..... 1
C1.3 Site Topography ..... 1
C1.4 Groundwater Conditions ..... 1
C2.0 GEOLOGIC SETTING ..... 2
C2.1 Subsurface Soil Conditions ..... 2
C3.0 GEOLOGIC/SEISMIC HAZARDS ..... 2
C3.1 Fault Rupture Hazard Zones in California ..... 2
C3.2 State of California Seismic Hazard Zones (Liquefaction and Landslides) ..... 2
C3.3 Slope Stability and Potential for Slope Failure ..... 2
C3.4 Flood and Inundation Hazards ..... 2
C3.6 Land Subsidence ..... 3
C4.0 SEISMIC HAZARD ASSESSMENT ..... 3
C4.1 Seismic Source Deaggregation ..... 3
C4.2 Historical Seismicity ..... 3
C4.3 Earthquake Ground Motion ..... 4
C4.3.1 Site Class ..... 4
C4.3.2 2010 California Building Code ..... 4
C4.3.3 Seismic Design Category ..... 4
C4.4 Liquefaction ..... 4
C4.5 Seismically-Induced Settlement ..... 5
C5.0 REFERENCES ..... 6

TABLES

Table C1 Seismic Hazard Deaggregation<br>Table C2 Historic Earthquakes within 100 Miles of Site

## FIGURES

Figure C1 Vicinity Map
Figure C2 Area Hydrographs
Figure C3 Geologic Map
Figure C4 Regional Fault Map
Figure C5 Earthquake Epicenter Map
Liquefaction Analysis Data Sheets and Results (48 Pages)

# GEOLOGIC/SEISMIC HAZARD INVESTIGATION <br> LEMOORE STUDENT CENTER <br> WEST HILLS COLLEGE <br> LEMOORE, CALIFORNIA 

## C1.0 INTRODUCTION

This report presents the geologic and seismic hazards evaluation prepared in accordance with 2010 California Building Code (CBC), CCR Title 24, Chapters 16 and 18 requirements for a Geotechnical/Engineering Geologic Report. The evaluation was performed in conformance with California Geologic Survey Note 48(January 2010).

## C1.1 Objective and Scope of Services

The objective of the geologic and seismic hazards assessment is to provide the Client with an evaluation of potential geologic or seismic hazards which may be present at the site or due to regional influences. BSK's scope of services for this assessment included the following: a review of published geologic literature; an evaluation of the data collected; determination of site class and seismic design parameters; liquefaction and seismic settlement analyses.

## C1.2 Site Location

The school is located in the City of Lemoore in the north western portion of Kings County, California. The school site coordinates are:

Latitude $36.29219^{\circ} \mathrm{N}$
Longitude $119.82608^{\circ} \mathrm{W}$
As shown on Figure C1, the site is located at the southeast corner of the southwest corner of Bush Street and College Avenue in Lemoore, California.

## C1.3 Site Topography

As shown on Figure C1, Topographic map, the site and surrounding area topography is relatively flat with a ground surface elevation between 210 feet and 215 feet, USGS datum.

## C1.4 Groundwater Conditions

The Site is within the Tulare Lake sub-basin of the San Joaquin Basin Hydrologic Study Area. This includes approximately the southern two-thirds of the Great Valley. Within the Study Area, 39 groundwater basins and areas of potential storage have been identified. The boundaries of these areas are based largely on hydrologic as well as political considerations.

At the time of our field exploration between May 12 and May 19, 2011, groundwater was encountered at a depth of approximately 7 feet below ground surface in our soil borings. To ascertain groundwater levels for the area during other time periods, groundwater elevation data from the California Department of Water Resources (DWR) were obtained for the period 1950 to 2007. Water level hydrographs from wells in the vicinity Site are presented on figure C2. The hydrographs indicate that, in the vicinity of the Site, the historical shallowest depth to groundwater varies from 60 feet to 6 feet bgs. For analysis a conservative assumed depth to groundwater, based on the historical depth of 6 feet bgs was used.

## C2.0 GEOLOGIC SETTING

The site is located in the Great Valley geomorphic province. The Site is located in the structural region identified by Bartow, 1991 as the San Joaquin Valley portion of the southern Sierran block. This area forms a broad syncline with deposits of marine and overlying continental sediments, Jurassic to Holocene in age. The thickness of the sediments increases to the west and reach a thickness of as much as 20,000 feet on the west side of the San Joaquin Valley syncline.

As shown on Figure C3, the Site is situated on recent basin deposits which were deposited from the Kings River.

## C2.1 Subsurface Soil Conditions

The soils encountered during our subsurface exploration consisted of silty sands, silty clays, clayey silts, and sandy silts. Based on the hand auguring soil boring data, the existing building pad consists primarily of silty sand. Based on hollow stem auger borings and CPT soundings, the native soil consists primarily of silty clays and clayey silts in the upper 10 feet. The soil below 10 feet is layered sand and silt with some silty clay. The maximum explored depth was 50 feet. Soil boring logs are included in Appendix A.

## C3.0 GEOLOGIC/SEISMIC HAZARDS

The types of geologic and seismic hazards assessed include surface ground fault rupture, liquefaction, seismically-induced settlement, slope failure, flood hazards and inundation hazards.

## C3.1 Fault Rupture Hazard Zones in California

The purpose of the Alquist-Priolo Geologic Hazards Zones Act, as summarized in CDMG Special Publication 42 (SP 42), is to "prohibit the location of most structures for human occupancy across the traces of active faults and to mitigate thereby the hazard of fault-rupture." As indicated by SP 42, "the State Geologist is required to delineate "earthquake fault zones" (EFZs) along known active faults in California. Cities and counties affected by the zones must regulate certain development 'projects' within the zones. They must withhold development permits for sites within the zones until geologic investigations demonstrate that the sites are not threatened by surface displacement from future faulting.

The Site is not located in a Fault-Rupture Hazard Zone. As shown on Figure 4, the closest FaultRupture Hazard Zone is associated with the Nunez Fault located approximately 35 miles west of the Site.

## C3.2 State of California Seismic Hazard Zones (Liquefaction and Landslides)

The Site is not currently located in a Seismic Hazard Zone specified by State of California.

## C3.3 Slope Stability and Potential for Slope Failure

The site and surrounding areas are essentially flat and the potential hazard due to landslides from adjacent properties is not applicable.

## C3.4 Flood and Inundation Hazards

An evaluation of flooding at the site includes review of potential hazards from flooding during periods of heavy precipitation and flooding due to a catastrophic dam breach from up-gradient surface impoundments.

## Flood Hazards

Flood Insurance Rates Maps (FIRM) published by the Federal Emergency Management Agency (FEMA) were reviewed to obtain information regarding the potential for flooding at the Site. According to the June 16, 2009 FIRM Map \#06031C0165C, the Site lies in Zone A inside the 100-year Special Flood Hazard Area.

## Inundation Hazards - Dams

According to the GIS data obtained from California Emergency Management Agency, the Site is located in the pathway of inundation from a catastrophic breach of Pine Flat Dam. According to the 1993 Kings County General Plan, if the Pine Flat Dam failed while at full capacity, its floodwaters would arrive in Kings County within approximately five hours.

## C3.5 Volcanic Hazards

According to USGS Bulletin 1847, dated 1989, the site is not located in an area which would be subject to hazards from volcanic eruptions.

## C3.6 Land Subsidence

Land subsidence in California generally occurs in areas of fluid removal (petroleum and groundwater) and in arid areas due to hydrocompaction of loose near surface soils.

The Site is not located in an area susceptible to subsidence due to petroleum or groundwater withdrawal. The Site is not located in an area which soils are known to be impacted by hydrocompaction.

## C4.0 SEISMIC HAZARD ASSESSMENT

## C4.1 Seismic Source Deaggregation

Figure C4 presents a regional fault map showing the major fault which may impact the Site. The probabilistic value of ground motion at a site can be caused by earthquakes on any of the sources surrounding the site. Deaggregation of the seismic hazard was performed by using the USGS Interactive Deaggregation website. The deaggregation at the MCE hazard level results in distance, magnitude and epsilon (round-motion uncertainty) for each source which contributes to the hazard. Each source has a corresponding epsilon which is the probabilistic value relative to the mean value of ground motion for that source.

Table C1 lists the result of deaggregation at the MCE hazard level from the USGS website. The most significant source that contributes to the PGA is the nearby Great Valley 14 Fault. With an epsilon value of 1.4 and a Magnitude 7.1, this source would approximate the most extreme design level event. For liquefaction and seismic settlement, a magnitude (Mw) of 7.1 would be appropriate for input parameters which are consistent with the design earthquake ground motion.

## C4.2 Historical Seismicity

Table C2 provide the location, earthquake magnitude, Site to earthquake distances, dates and the resulting Site peak horizontal acceleration for the period 1800 to 1999 . . The table shows that the Site has experienced mean plus one sigma peak horizontal acceleration up to 0.18 g from the Coalinga Earthquake of 1983. In general, the site has been subjected to relatively low intensity ground motion, primarily from large earthquakes on distance faults and low magnitude
earthquakes closer to the site. Figure C5 presents historical earthquake magnitude and locations relative to the Site.

## C4.3 Earthquake Ground Motion

## C4.3.1 Site Class

Based on the equivalent " N " values converted from the CPT test holes completed in May 2011, as per Table 1613.5.2 of 2010 CBC , the Site is Class $\mathrm{D}(15 \leq \mathrm{N} \leq 50)$.

## C4.3.2 2010 California Building Code

The earthquake hazard level of the maximum considered earthquake (MCE) is define in ASFE 705 as the ground motion resulting from a seismic source(s) having a probability of exceedance of $2 \%$ in 50 years. The United States Geologic Survey (USGS) has prepared maps presenting the MCE spectral acceleration ( $5 \%$ damping) for periods of 0.2 seconds ( $\mathrm{S}_{\mathrm{S}}$ ) and 1.0 seconds ( $\mathrm{S}_{1}$ ). The values of $\mathrm{S}_{\mathrm{S}}$ and $\mathrm{S}_{1}$ can be obtained from the USGS Ground Motion Parameter Calculator available at: http://earthquake.usgs.gov/research/hazmaps/design/index.php.

The USGS Ground Motion Parameter Calculator and Chapter 16 of 2010 CBC produced the following values based on Site Class D conditions:

TABLE A
SPECTRAL ACCELERATION PARAMETERS

| Criteria | Value |  | Reference |
| :--- | :---: | :---: | :--- |
| MCE Mapped Spectral Acceleration $(\mathrm{g})$ | $\mathrm{S}_{\mathrm{S}}=0.81$ | $\mathrm{~S}_{1}=0.31$ | USGS Mapped Value |
| Amplification Factors (Site Class D) | $\mathrm{Fa}=1.18$ | $\mathrm{Fv}=1.78$ | Table 1613.5.3 |
| Site Adjusted MCE Spectral Acceleration $(\mathrm{g})$ | $\mathrm{S}_{\mathrm{MS}}=0.95$ | $\mathrm{~S}_{\mathrm{M} 1}=0.55$ | Equations 16-37,38 |
| Design Spectral Acceleration $(\mathrm{g})$ | $\mathrm{S}_{\mathrm{DS}}=0.63$ | $\mathrm{~S}_{\mathrm{D} 1}=0.37$ | Equations 16-39, 40 |
| Design Peak Ground Acceleration $\left(\mathrm{S}_{\mathrm{DS}} / 2.5\right)(\mathrm{g})$ | $\mathrm{PGA}=0.25$ |  | CGS Note 48 |

## C4.3.3 Seismic Design Category

$\mathrm{S}_{\mathrm{D} 1}$ is greater than 0.20 g , therefore the site is Seismic Design Category D (Table 1613.5.6(2), 2010 CBC)

## C4.4 Liquefaction

Liquefaction describes a condition in which a saturated, cohesionless soil loses shear strength during earthquake shocks. Ground motion from an earthquake may induce cyclic reversals of shearing strains of large amplitude. Lateral and vertical movements of the soil mass, combined with loss of bearing strength, usually result from this phenomenon. Historically, liquefaction of soils has caused severe damage to structures, berms, levees and roads. Seed and Idriss (1971) demonstrated that liquefaction potential depends on soil type, void ratio, depth to groundwater, duration of shaking and confining pressures over the potentially liquefiable soil mass. Fine, well sorted, loose sand, shallow groundwater, severe seismic ground motion and particularly long durations of ground shaking are conditions conducive for liquefaction.

In order to evaluate the liquefaction potential and quantify the effects of liquefaction, a BSK Job G1100311B
liquefaction and seismic settlement analysis based upon the Simple Cyclic Stress Ratio and CPT data using the computer program "Cliq," was performed. The program uses a method which is consistent with the 1998 NCEER/NSF Workshop on Evaluation of Liquefaction Resistance of Soils. The program CLiq provides consistent output results by applying the state-of-the-art NCEER method (Youd et al, 2001) along with the calibrated procedures for post-earthquake displacements by Zhang et al (2002 \& 2004).

Input parameters for the liquefaction and settlement analysis were based upon:
CPT Data from each of the four CPT test holes.
PGA based upon the design event of 0.25 g .
Magnitude 7.1 of controlling earthquake.
Assumed depth to groundwater of 6 feet bgs.
Clay-like behavior was assumed for units with an Ic above 2.60.

Data sheets and input parameters for each of the liquefaction analysis are provided in herein.
Our analysis indicates that during the design event, the factor of safety against liquefaction is less than a value of 1.0 (acceptable for most structures) in some minor subsurface units. Based on the limited thickness of the potential liquefiable units (less than two feet), the overall potential for significant liquefaction to occur at the Site is low.

## C4.5 Seismically-Induced Settlement

Settlement of the ground surface with consequential differential movement of structures is a major cause of seismic damage for buildings founded on alluvial deposits. Vibration settlement of relatively dry and loose granular deposits beneath structures can be readily induced by the horizontal components of ground shaking associated with even moderate intensity earthquakes. Silver and Seed (1971) have demonstrated that settlement of dry sands due to cyclic loading is a function of 1) the relative density of the soil; 2) the magnitude of the cyclic shear stress; and 3) the number of strain cycles. As indicated above, seismically-induced ground settlement can also occur due to the liquefaction of relatively loose, saturated granular deposits.

Seismically induced ground settlement of the saturated portion of the sandy soils based on our analysis is estimated to range from 1.0 inches to 1.4 inches. Differential seismically induced settlement is estimated to be about 0.4 inches across a horizontal distance of 100 feet.

Based on the ratio of the thickness of liquefiable units compared to non-liquefiable over-lying units using the method of Ishihara, 1985, sand boils or surface manifestations of liquefaction are not anticipated.

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## TABLES

TABLE C1
SEISMIC HAZARD DEAGGREGATION
MAXIMUM CONSIDERD EARTHQUAKE

| Seismic Source | Percent <br> Contribution | Distance <br> $\mathbf{( k m )}$ | Magnitude <br> $\mathbf{( M w )}$ | Epsilon <br> (Mean Values) |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| PGA Deaggregation |  |  |  |  |
| CA Compr. crustal gridded | 76.7 | 10.0 | 5.9 | 0.8 |
| Great Valley 14 (Kettleman Hills) | 6.1 | 31.9 | 7.1 | 1.4 |
| Great Valley 13 (Coalinga) Char | 6.4 | 31.6 | 7.0 | 1.5 |
| Great Valley 14 (Kettleman Hil G) | 3.5 | 31.9 | 6.9 | 1.7 |
| Great Valley 13 (Coalinga) GR | 3.4 | 32.0 | 6.8 | 1.7 |

TABLE C2
Historic Earthquakes Within 100 Miles of the Site Ground Motion Greater Than 0.05 g

| File Code | Latitude (North) | Longitute (West) | Date | Depth <br> (km) | Earthquake Magnitude | Site Acceleration (g) | Distance mi (km) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BRK | 36.22 | 120.29 | 5/2/1983 | 0 | 6.7 | 0.18 | 26.3 (42.3) |
| PAS | 36.151 | 120.049 | 8/4/1985 | 6 | 5.8 | 0.17 | 15.8 (25.4) |
| DMG | 35.3 | 119.8 | 01/09/1857 | 0 | 7.9 | 0.16 | 68.5 (110.3) |
| DMG | 36.7 | 118.1 | 03/26/1872 | 0 | 7.8 | 0.12 | 99.9 (160.7) |
| DMG | 35.75 | 120.25 | 3/10/1922 | 0 | 6.5 | 0.11 | 44.3 (71.3) |
| BRK | 36.22 | 120.4 | 7/22/1983 | 0 | 6.0 | 0.11 | 32.3 (52.0) |
| BRK | 36.22 | 120.29 | 5/2/1983 | 0 | 5.6 | 0.10 | 26.3 (42.3) |
| BRK | 36.22 | 120.26 | 9/9/1983 | 0 | 5.4 | 0.10 | 24.7 (39.7) |
| PAS | 36.286 | 120.413 | 10/25/1982 | 6 | 5.6 | 0.09 | 32.7 (52.6) |
| DMG | 35.8 | 120.33 | 6/8/1934 | 0 | 6.0 | 0.08 | 44.1 (71.0) |
| BRK | 36.24 | 120.29 | 5/9/1983 | 0 | 5.2 | 0.08 | 26.1 (42.0) |
| PAS | 36.131 | 119.997 | 8/5/1985 | 6 | 4.3 | 0.08 | 14.6 (23.6) |
| BRK | 36.11 | 120.16 | 1/14/1976 | 0 | 4.9 | 0.08 | 22.5 (36.1) |
| PAS | 36.182 | 120.268 | 2/14/1987 | 6 | 5.1 | 0.08 | 25.8 (41.4) |
| BRK | 36.26 | 120.4 | 7/9/1983 | 0 | 5.3 | 0.08 | 32.0 (51.5) |
| PAS | 36.145 | 120.052 | 8/4/1985 | 6 | 4.3 | 0.07 | 16.2 (26.0) |
| PAS | 36.22 | 120.136 | 9/24/1980 | 6.7 | 4.4 | 0.07 | 18.0 (28.9) |
| PAS | 36.119 | 119.989 | 8/4/1985 | 6 | 4.1 | 0.07 | 15.0 (24.2) |
| PAS | 36.052 | 119.978 | 8/4/1985 | 6 | 4.4 | 0.07 | 18.6 (30.0) |
| DMG | 35.98 | 120.04 | 9/19/1965 | 0 | 4.8 | 0.07 | 24.6 (39.6) |
| DMG | 36 | 120.5 | 02/02/1881 | 0 | 5.6 | 0.07 | 42.6 (68.6) |
| DMG | 36.17 | 120.32 | 12/27/1926 | 0 | 5.0 | 0.07 | 28.8 (46.3) |
| DMG | 36.4 | 121 | 04/12/1885 | 0 | 6.2 | 0.07 | 65.7 (105.7) |
| T-A | 36.17 | 119.32 | 07/25/1868 | 0 | 5.0 | 0.07 | 29.4 (47.3) |
| BRK | 36.21 | 120.38 | 7/25/1983 | 0 | 5.1 | 0.07 | 31.4 (50.5) |
| PAS | 36.062 | 120.163 | 1/14/1976 | 7 | 4.7 | 0.07 | 24.6 (39.6) |
| BRK | 36.25 | 120.29 | 5/3/1983 | 0 | 4.8 | 0.07 | 26.0 (41.8) |
| DMG | 36 | 120.5 | 3/3/1901 | 0 | 5.5 | 0.07 | 42.6 (68.6) |
| DMG | 35.95 | 120.5 | 6/28/1966 | 0 | 5.5 | 0.06 | 44.4 (71.4) |
| BRK | 36.13 | 120.19 | 5/3/1983 | 0 | 4.5 | 0.06 | 23.2 (37.3) |
| BRK | 36.27 | 120.33 | 5/3/1983 | 0 | 4.8 | 0.06 | 28.1 (45.2) |
| BRK | 36.2 | 120.4 | 7/22/1983 | 0 | 5.0 | 0.06 | 32.6 (52.4) |
| GSB | 36.003 | 119.916 | 9/16/1992 | 11 | 4.3 | 0.06 | 20.6 (33.1) |
| BRK | 36.46 | 120.34 | 8/3/1975 | 0 | 4.9 | 0.06 | 30.8 (49.6) |
| PAS | 36.027 | 120.056 | 8/7/1985 | 6 | 4.4 | 0.06 | 22.3 (36.0) |
| BRK | 36.25 | 120.47 | 6/11/1983 | 0 | 5.1 | 0.06 | 36.0 (57.9) |
| PAS | 36.25 | 120.267 | 5/3/1983 | 9 | 4.5 | 0.06 | 24.7 (39.8) |
| BRK | 36.26 | 120.33 | 5/4/1983 | 0 | 4.7 | 0.06 | 28.1 (45.3) |
| BRK | 36.25 | 120.31 | 5/24/1983 | 0 | 4.6 | 0.06 | 27.1 (43.6) |
| BRK | 36.18 | 120.12 | 8/12/1983 | 0 | 4.0 | 0.06 | 18.1 (29.1) |
| BRK | 36.15 | 120.25 | 5/12/1983 | 0 | 4.5 | 0.06 | 25.6 (41.1) |
| DMG | 36.9 | 118.2 | 03/26/1872 | 0 | 6.5 | 0.06 | 99.4 (160.0) |
| BRK | 36.13 | 120.25 | 5/3/1983 | 0 | 4.5 | 0.06 | 26.1 (42.1) |
| BRK | 36.25 | 120.28 | 5/3/1983 | 0 | 4.4 | 0.06 | 25.4 (40.9) |
| BRK | 36.28 | 120.36 | 5/5/1983 | 0 | 4.6 | 0.06 | 29.7 (47.8) |
| DMG | 35.383 | 118.85 | 7/29/1952 | 0 | 6.1 | 0.05 | 83.2 (133.9) |
| PAS | 36.205 | 120.176 | 5/3/1983 | 9 | 4.0 | 0.05 | 20.4 (32.8) |
| GSB | 36.007 | 119.94 | 9/27/1992 | 13 | 4.0 | 0.05 | 20.7 (33.3) |
| BRK | 36.1 | 120.18 | 5/3/1983 | 0 | 4.2 | 0.05 | 23.8 (38.2) |
| PAS | 36.091 | 120.208 | 8/4/1985 | 6 | 4.3 | 0.05 | 25.4 (40.9) |
| BRK | 36.22 | 120.3 | 5/9/1983 | 0 | 4.4 | 0.05 | 26.8 (43.2) |

TABLE C2
Historic Earthquakes Within 100 Miles of the Site Ground Motion Greater Than $\mathbf{0 . 0 5 g}$

| File <br> Code | Latitude <br> (North) | Longitute <br> (West) | Date | Depth <br> $\mathbf{( k m )}$ | Earthquake <br> Magnitude | Site <br> Acceleration <br> $(\mathbf{g})$ | Distance mi (km) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DMG | 35.97 | 120.5 | $6 / 28 / 1966$ | 0 | 5.1 | 0.05 | $43.7(70.3)$ |
| PAS | 37.464 | 118.823 | $5 / 27 / 1980$ | 2.4 | 6.3 | 0.05 | $98.1(157.8)$ |
| PAS | 36.177 | 120.175 | $5 / 3 / 1983$ | 5 | 4.0 | 0.05 | $21.0(33.8)$ |
| USG | 36.154 | 120.232 | $5 / 2 / 1983$ | 8.6 | 4.2 | 0.05 | $24.5(39.5)$ |
| GSP | 36.181 | 120.301 | $3 / 31 / 1994$ | 10 | 4.4 | 0.05 | $27.5(44.3)$ |
| PAS | 36.219 | 120.264 | $5 / 8 / 1984$ | 15.3 | 4.2 | 0.05 | $24.9(40.1)$ |
| PAS | 36.274 | 120.331 | $2 / 19 / 1984$ | 7.4 | 4.4 | 0.05 | $28.1(45.3)$ |
| DMG | 35.95 | 120.47 | $11 / 16 / 1956$ | 0 | 5.0 | 0.05 | $43.0(69.2)$ |
| BRK | 36.07 | 120.19 | $12 / 21 / 1983$ | 0 | 4.2 | 0.05 | $25.4(40.9)$ |
| GSB | 35.917 | 120.465 | $12 / 20 / 1994$ | 8 | 5.0 | 0.05 | $44.1(70.9)$ |
| DMG | 35.8 | 120.33 | $6 / 5 / 1934$ | 0 | 5.0 | 0.05 | $44.1(71.0)$ |
| DMG | 35.8 | 120.33 | $12 / 28 / 1939$ | 0 | 5.0 | 0.05 | $44.1(71.0)$ |
| DMG | 35.8 | 120.33 | $6 / 8 / 1934$ | 0 | 5.0 | 0.05 | $44.1(71.0)$ |
| DMG | 35.93 | 120.48 | $12 / 24 / 1934$ | 0 | 5.0 | 0.05 | $44.2(71.2)$ |
| DMG | 35.73 | 121.2 | $11 / 22 / 1952$ | 0 | 6.0 | 0.05 | $86.0(138.4)$ |

## FIGURES





Groundwater Levels, 19520E22C001M


Groundwater Levels, 19520E19A001M San Joaquin Valley (Tulare Lake Basin)







## LIQUEFACTION ANALYSIS

## DATA SHEETS AND

RESULTS

## LIQUEFACTION ANALYSIS REPORT

## Project title : Lemoore Student Center

## CPT file: NE Corner

Input parameters and analysis data
Analysis method:
Fines correction method: Points to test:
Earthquake magnitude $\mathrm{M}_{\mathrm{w}}$ :
Peak ground acceleration:

NCEER 1998
Robertson \& Wride
Based on Ic value
$\begin{array}{ll}\text { G.W.T. (in-situ): } & 6.00 \mathrm{ft} \\ \text { G.W.T. (earthq.): } & 6.00 \mathrm{ft} \\ \text { Average results interval: } & 3\end{array}$
Ic cut-off value: $\quad 2.60$ Unit weight calculation: Based on SBT

## Location : West Hills College



Use fill:
Fill height:
No N/A N/A
Yes
Trans. detect. applied: Yes $\mathrm{K}_{\sigma}$ applied:

Clay like behavior applied: All soil Limit depth applied: No Limit depth:

N/A


Zone $\mathrm{A}_{1}$ : Cyclic liquefaction likely depending on size and duration of cyclic loading Zone $A_{2}$ : Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening Zone C : Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

## Liquefaction analysis overall plots




Input parameters and analysis data

| Analysis method: | NCEER 1998 |
| :--- | :--- |
| Fines correction method: | Robertson \& Wride |
| Points to test: | Based on Ic value |
| Earthquake magnitude $\mathrm{M}_{\mathrm{w}}$ : | 7.10 |
| Peak ground acceleration: | 0.25 |

Depth to water table (erthq.): 6.00 ft
Fines correction method: Points to test:
$\begin{array}{ll}\text { Use fill: } & \text { Based } \\ \text { Fill height: } & \text { No }\end{array}$ Fill height:
CLiq v 1.4.1.22 - CPT Liquefaction Assessment Software - Report created on: 5/24/2011, 1.37:40 PM
Project file: J:\Geotechnical\Open Projects\G1100311B - Lemoore West Hills Col\liq-analysis-all4.clq

## Check for strength loss plots (Robertson (2010))




Corrected norm. cone resistance


SBTn Index


Liquefied Su/Sig'v


## Input parameters and analysis data

| Analysis method: | NCEER 1998 |
| :--- | :--- |
| Fines correction method: | Robertson \& Wride |
| Points to test: | Based on Ic value |
| Earthquake magnitude $M_{w}:$ | 7.10 |
| Peak ground acceleration: | 0.25 |

Depth to water table (erthq.): 6.00 ft Average results interval:
$\begin{array}{ll}\text { Ic cut-off value: } & 2.60\end{array}$
Unit weight calculation: $\quad \begin{aligned} & \text { Based on SBT }\end{aligned}$
Use fill:
$\begin{array}{ll}\text { Fill height: } & \text { No } \\ & \text { N/A }\end{array}$
Fill weight:
Transition N/A
Transition detect. applied:
$\mathrm{K}_{\mathrm{\sigma}}$ applied:
Clay like behavior applied:
Limit depth applied:
Limit depth:
Yes
No
Limit depth:
CLiq v.1.4.1.22 - CPT Liquefaction Assessment Software - Report created on: 5/24/2011, 1:37:40 PM
Project file: J:\Geotechnical\Open Projects\G1100311B - Lemoore West Hills Col\liq-analysis-all4.clq

# TRANSITION LAYER DETECTION ALGORITHM REPORT Summary Details \& Plots 

## Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of $\mathrm{I}_{\mathrm{c}}$ values over which the transition will be defined (typically somewhere between $1.80<\mathrm{I}_{\mathrm{c}}<3.0$ ) and a rate of change of $I_{c}$. Transitions typically occur when the rate of change of $I_{c}$ is fast (i.e. delta $I_{c}$ is small).

The $\mathrm{SBT}_{\mathrm{n}}$ plot below, displays in red the detected transition layers based on the parameters listed below the graphs.


## Transition layer algorithm properties

$\mathrm{I}_{\mathrm{c}}$ minimum check value:
2.10
$\mathrm{I}_{\mathrm{c}}$ maximum check value:
2.92
$I_{c}$ change ratio value: 0.0250
Minimum number of points in layer: 4

## General statistics

Total points in CPT file: 305
Total points excluded: 28
Exclusion percentage: $9.18 \%$
Number of layers detected: 6
:: Liquefaction Potential Index calculation data ::

| Depth (ft) | FS | FL | $\mathrm{w}_{\text {z }}$ | $\mathrm{d}_{2}$ | LPI | Depth <br> (ft) | FS | FL | $\mathrm{w}_{\text {z }}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.16 | 2.00 | 0.00 | 9.97 | 0.16 | 0.00 | 0.33 | 2.00 | 0.00 | 9.95 | 0.16 | 0.00 |
| 0.49 | 2.00 | 0.00 | 9.92 | 0.16 | 0.00 | 0.66 | 2.00 | 0.00 | 9.90 | 0.16 | 0.00 |
| 0.82 | 2.00 | 0.00 | 9.87 | 0.16 | 0.00 | 0.98 | 2.00 | 0.00 | 9.85 | 0.16 | 0.00 |
| 1.15 | 2.00 | 0.00 | 9.82 | 0.16 | 0.00 | 1.31 | 2.00 | 0.00 | 9.80 | 0.16 | 0.00 |
| 1.48 | 2.00 | 0.00 | 9.77 | 0.16 | 0.00 | 1.64 | 2.00 | 0.00 | 9.75 | 0.16 | 0.00 |
| 1.80 | 2.00 | 0.00 | 9.72 | 0.16 | 0.00 | 1.97 | 2.00 | 0.00 | 9.70 | 0.16 | 0.00 |
| 2.13 | 2.00 | 0.00 | 9.67 | 0.16 | 0.00 | 2.30 | 2.00 | 0.00 | 9.65 | 0.16 | 0.00 |
| 2.46 | 2.00 | 0.00 | 9.62 | 0.16 | 0.00 | 2.62 | 2.00 | 0.00 | 9.60 | 0.16 | 0.00 |
| 2.79 | 2.00 | 0.00 | 9.57 | 0.16 | 0.00 | 2.95 | 2.00 | 0.00 | 9.55 | 0.16 | 0.00 |
| 3.12 | 2.00 | 0.00 | 9.52 | 0.16 | 0.00 | 3.28 | 2.00 | 0.00 | 9.50 | 0.16 | 0.00 |
| 3.44 | 2.00 | 0.00 | 9.47 | 0.16 | 0.00 | 3.61 | 2.00 | 0.00 | 9.45 | 0.16 | 0.00 |
| 3.77 | 2.00 | 0.00 | 9.42 | 0.16 | 0.00 | 3.94 | 2.00 | 0.00 | 9.40 | 0.16 | 0.00 |
| 4.10 | 2.00 | 0.00 | 9.37 | 0.16 | 0.00 | 4.27 | 2.00 | 0.00 | 9.35 | 0.16 | 0.00 |
| 4.43 | 2.00 | 0.00 | 9.32 | 0.16 | 0.00 | 4.59 | 2.00 | 0.00 | 9.30 | 0.16 | 0.00 |
| 4.76 | 2.00 | 0.00 | 9.27 | 0.16 | 0.00 | 4.92 | 2.00 | 0.00 | 9.25 | 0.16 | 0.00 |
| 5.09 | 2.00 | 0.00 | 9.22 | 0.16 | 0.00 | 5.25 | 2.00 | 0.00 | 9.20 | 0.16 | 0.00 |
| 5.41 | 2.00 | 0.00 | 9.17 | 0.16 | 0.00 | 5.58 | 2.00 | 0.00 | 9.15 | 0.16 | 0.00 |
| 5.74 | 2.00 | 0.00 | 9.12 | 0.16 | 0.00 | 5.91 | 2.00 | 0.00 | 9.10 | 0.16 | 0.00 |
| 6.07 | 2.00 | 0.00 | 9.07 | 0.16 | 0.00 | 6.23 | 2.00 | 0.00 | 9.05 | 0.16 | 0.00 |
| 6.40 | 2.00 | 0.00 | 9.02 | 0.16 | 0.00 | 6.56 | 2.00 | 0.00 | 9.00 | 0.16 | 0.00 |
| 6.73 | 2.00 | 0.00 | 8.97 | 0.16 | 0.00 | 6.89 | 2.00 | 0.00 | 8.95 | 0.16 | 0.00 |
| 7.05 | 2.00 | 0.00 | 8.92 | 0.16 | 0.00 | 7.22 | 2.00 | 0.00 | 8.90 | 0.16 | 0.00 |
| 7.38 | 2.00 | 0.00 | 8.87 | 0.16 | 0.00 | 7.55 | 2.00 | 0.00 | 8.85 | 0.16 | 0.00 |
| 7.71 | 2.00 | 0.00 | 8.82 | 0.16 | 0.00 | 7.87 | 2.00 | 0.00 | 8.80 | 0.16 | 0.00 |
| 8.04 | 2.00 | 0.00 | 8.77 | 0.16 | 0.00 | 8.20 | 2.00 | 0.00 | 8.75 | 0.16 | 0.00 |
| 8.37 | 2.00 | 0.00 | 8.72 | 0.16 | 0.00 | 8.53 | 2.00 | 0.00 | 8.70 | 0.16 | 0.00 |
| 8.69 | 1.27 | 0.00 | 8.67 | 0.16 | 0.00 | 8.86 | 1.35 | 0.00 | 8.65 | 0.16 | 0.00 |
| 9.02 | 1.53 | 0.00 | 8.62 | 0.16 | 0.00 | 9.19 | 1.92 | 0.00 | 8.60 | 0.16 | 0.00 |
| 9.35 | 2.00 | 0.00 | 8.57 | 0.16 | 0.00 | 9.51 | 2.00 | 0.00 | 8.55 | 0.16 | 0.00 |
| 9.68 | 2.00 | 0.00 | 8.52 | 0.16 | 0.00 | 9.84 | 2.00 | 0.00 | 8.50 | 0.16 | 0.00 |
| 10.01 | 2.00 | 0.00 | 8.47 | 0.16 | 0.00 | 10.17 | 2.00 | 0.00 | 8.45 | 0.16 | 0.00 |
| 10.33 | 2.00 | 0.00 | 8.42 | 0.16 | 0.00 | 10.50 | 1.61 | 0.00 | 8.40 | 0.16 | 0.00 |
| 10.66 | 1.25 | 0.00 | 8.37 | 0.16 | 0.00 | 10.83 | 1.17 | 0.00 | 8.35 | 0.16 | 0.00 |
| 10.99 | 1.20 | 0.00 | 8.32 | 0.16 | 0.00 | 11.15 | 1.21 | 0.00 | 8.30 | 0.16 | 0.00 |
| 11.32 | 1.20 | 0.00 | 8.27 | 0.16 | 0.00 | 11.48 | 1.18 | 0.00 | 8.25 | 0.16 | 0.00 |
| 11.65 | 1.09 | 0.00 | 8.22 | 0.16 | 0.00 | 11.81 | 0.97 | 0.03 | 8.20 | 0.16 | 0.01 |
| 11.98 | 0.85 | 0.15 | 8.17 | 0.16 | 0.06 | 12.14 | 0.80 | 0.20 | 8.15 | 0.16 | 0.08 |
| 12.30 | 0.84 | 0.16 | 8.12 | 0.16 | 0.07 | 12.47 | 1.03 | 0.00 | 8.10 | 0.16 | 0.00 |
| 12.63 | 1.55 | 0.00 | 8.07 | 0.16 | 0.00 | 12.80 | 2.00 | 0.00 | 8.05 | 0.16 | 0.00 |
| 12.96 | 2.00 | 0.00 | 8.02 | 0.16 | 0.00 | 13.12 | 2.00 | 0.00 | 8.00 | 0.16 | 0.00 |
| 13.29 | 2.00 | 0.00 | 7.97 | 0.16 | 0.00 | 13.45 | 2.00 | 0.00 | 7.95 | 0.16 | 0.00 |
| 13.62 | 2.00 | 0.00 | 7.92 | 0.16 | 0.00 | 13.78 | 2.00 | 0.00 | 7.90 | 0.16 | 0.00 |
| 13.94 | 2.00 | 0.00 | 7.87 | 0.16 | 0.00 | 14.11 | 2.00 | 0.00 | 7.85 | 0.16 | 0.00 |
| 14.27 | 2.00 | 0.00 | 7.82 | 0.16 | 0.00 | 14.44 | 1.57 | 0.00 | 7.80 | 0.16 | 0.00 |
| 14.60 | 1.14 | 0.00 | 7.77 | 0.16 | 0.00 | 14.76 | 2.00 | 0.00 | 7.75 | 0.16 | 0.00 |
| 14.93 | 2.00 | 0.00 | 7.72 | 0.16 | 0.00 | 15.09 | 2.00 | 0.00 | 7.70 | 0.16 | 0.00 |
| 15.26 | 2.00 | 0.00 | 7.67 | 0.16 | 0.00 | 15.42 | 2.00 | 0.00 | 7.65 | 0.16 | 0.00 |
| 15.58 | 2.00 | 0.00 | 7.62 | 0.16 | 0.00 | 15.75 | 2.00 | 0.00 | 7.60 | 0.16 | 0.00 |

## :: Liquefaction Potential Index calculation data :: (continued)

| Depth (ft) | FS | FL | $\mathrm{w}_{\text {z }}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI | Depth <br> (ft) | FS | FL | $\mathrm{w}_{\text {z }}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15.91 | 2.00 | 0.00 | 7.57 | 0.16 | 0.00 | 16.08 | 2.00 | 0.00 | 7.55 | 0.16 | 0.00 |
| 16.24 | 1.94 | 0.00 | 7.52 | 0.16 | 0.00 | 16.40 | 1.76 | 0.00 | 7.50 | 0.16 | 0.00 |
| 16.57 | 1.57 | 0.00 | 7.47 | 0.16 | 0.00 | 16.73 | 1.40 | 0.00 | 7.45 | 0.16 | 0.00 |
| 16.90 | 1.32 | 0.00 | 7.42 | 0.16 | 0.00 | 17.06 | 1.32 | 0.00 | 7.40 | 0.16 | 0.00 |
| 17.22 | 1.35 | 0.00 | 7.37 | 0.16 | 0.00 | 17.39 | 1.39 | 0.00 | 7.35 | 0.16 | 0.00 |
| 17.55 | 1.35 | 0.00 | 7.32 | 0.16 | 0.00 | 17.72 | 1.34 | 0.00 | 7.30 | 0.16 | 0.00 |
| 17.88 | 1.35 | 0.00 | 7.27 | 0.16 | 0.00 | 18.04 | 1.42 | 0.00 | 7.25 | 0.16 | 0.00 |
| 18.21 | 1.48 | 0.00 | 7.22 | 0.16 | 0.00 | 18.37 | 1.59 | 0.00 | 7.20 | 0.16 | 0.00 |
| 18.54 | 1.70 | 0.00 | 7.17 | 0.16 | 0.00 | 18.70 | 1.78 | 0.00 | 7.15 | 0.16 | 0.00 |
| 18.86 | 1.86 | 0.00 | 7.12 | 0.16 | 0.00 | 19.03 | 1.98 | 0.00 | 7.10 | 0.16 | 0.00 |
| 19.19 | 2.00 | 0.00 | 7.07 | 0.16 | 0.00 | 19.36 | 2.00 | 0.00 | 7.05 | 0.16 | 0.00 |
| 19.52 | 2.00 | 0.00 | 7.02 | 0.16 | 0.00 | 19.69 | 2.00 | 0.00 | 7.00 | 0.16 | 0.00 |
| 19.85 | 2.00 | 0.00 | 6.97 | 0.16 | 0.00 | 20.01 | 2.00 | 0.00 | 6.95 | 0.16 | 0.00 |
| 20.18 | 2.00 | 0.00 | 6.92 | 0.16 | 0.00 | 20.34 | 2.00 | 0.00 | 6.90 | 0.16 | 0.00 |
| 20.51 | 1.98 | 0.00 | 6.87 | 0.16 | 0.00 | 20.67 | 1.76 | 0.00 | 6.85 | 0.16 | 0.00 |
| 20.83 | 1.60 | 0.00 | 6.82 | 0.16 | 0.00 | 21.00 | 1.57 | 0.00 | 6.80 | 0.16 | 0.00 |
| 21.16 | 1.55 | 0.00 | 6.77 | 0.16 | 0.00 | 21.33 | 2.00 | 0.00 | 6.75 | 0.16 | 0.00 |
| 21.49 | 2.00 | 0.00 | 6.72 | 0.16 | 0.00 | 21.65 | 2.00 | 0.00 | 6.70 | 0.16 | 0.00 |
| 21.82 | 2.00 | 0.00 | 6.67 | 0.16 | 0.00 | 21.98 | 2.00 | 0.00 | 6.65 | 0.16 | 0.00 |
| 22.15 | 2.00 | 0.00 | 6.62 | 0.16 | 0.00 | 22.31 | 2.00 | 0.00 | 6.60 | 0.16 | 0.00 |
| 22.47 | 2.00 | 0.00 | 6.57 | 0.16 | 0.00 | 22.64 | 2.00 | 0.00 | 6.55 | 0.16 | 0.00 |
| 22.80 | 2.00 | 0.00 | 6.52 | 0.16 | 0.00 | 22.97 | 2.00 | 0.00 | 6.50 | 0.16 | 0.00 |
| 23.13 | 2.00 | 0.00 | 6.47 | 0.16 | 0.00 | 23.29 | 2.00 | 0.00 | 6.45 | 0.16 | 0.00 |
| 23.46 | 2.00 | 0.00 | 6.42 | 0.16 | 0.00 | 23.62 | 2.00 | 0.00 | 6.40 | 0.16 | 0.00 |
| 23.79 | 2.00 | 0.00 | 6.37 | 0.16 | 0.00 | 23.95 | 2.00 | 0.00 | 6.35 | 0.16 | 0.00 |
| 24.11 | 2.00 | 0.00 | 6.32 | 0.16 | 0.00 | 24.28 | 2.00 | 0.00 | 6.30 | 0.16 | 0.00 |
| 24.44 | 1.97 | 0.00 | 6.27 | 0.16 | 0.00 | 24.61 | 1.87 | 0.00 | 6.25 | 0.16 | 0.00 |
| 24.77 | 1.70 | 0.00 | 6.22 | 0.16 | 0.00 | 24.93 | 1.50 | 0.00 | 6.20 | 0.16 | 0.00 |
| 25.10 | 1.24 | 0.00 | 6.17 | 0.16 | 0.00 | 25.26 | 1.03 | 0.00 | 6.15 | 0.16 | 0.00 |
| 25.43 | 0.90 | 0.10 | 6.12 | 0.16 | 0.03 | 25.59 | 0.85 | 0.15 | 6.10 | 0.16 | 0.05 |
| 25.75 | 0.89 | 0.11 | 6.07 | 0.16 | 0.03 | 25.92 | 1.00 | 0.00 | 6.05 | 0.16 | 0.00 |
| 26.08 | 1.23 | 0.00 | 6.02 | 0.16 | 0.00 | 26.25 | 1.38 | 0.00 | 6.00 | 0.16 | 0.00 |
| 26.41 | 1.32 | 0.00 | 5.97 | 0.16 | 0.00 | 26.57 | 1.18 | 0.00 | 5.95 | 0.16 | 0.00 |
| 26.74 | 1.07 | 0.00 | 5.92 | 0.16 | 0.00 | 26.90 | 1.11 | 0.00 | 5.90 | 0.16 | 0.00 |
| 27.07 | 1.08 | 0.00 | 5.87 | 0.16 | 0.00 | 27.23 | 1.07 | 0.00 | 5.85 | 0.16 | 0.00 |
| 27.40 | 1.06 | 0.00 | 5.82 | 0.16 | 0.00 | 27.56 | 1.05 | 0.00 | 5.80 | 0.16 | 0.00 |
| 27.72 | 1.05 | 0.00 | 5.77 | 0.16 | 0.00 | 27.89 | 1.14 | 0.00 | 5.75 | 0.16 | 0.00 |
| 28.05 | 1.40 | 0.00 | 5.72 | 0.16 | 0.00 | 28.22 | 1.77 | 0.00 | 5.70 | 0.16 | 0.00 |
| 28.38 | 2.00 | 0.00 | 5.67 | 0.16 | 0.00 | 28.54 | 2.00 | 0.00 | 5.65 | 0.16 | 0.00 |
| 28.71 | 2.00 | 0.00 | 5.62 | 0.16 | 0.00 | 28.87 | 2.00 | 0.00 | 5.60 | 0.16 | 0.00 |
| 29.04 | 2.00 | 0.00 | 5.57 | 0.16 | 0.00 | 29.20 | 2.00 | 0.00 | 5.55 | 0.16 | 0.00 |
| 29.36 | 2.00 | 0.00 | 5.52 | 0.16 | 0.00 | 29.53 | 2.00 | 0.00 | 5.50 | 0.16 | 0.00 |
| 29.69 | 2.00 | 0.00 | 5.47 | 0.16 | 0.00 | 29.86 | 2.00 | 0.00 | 5.45 | 0.16 | 0.00 |
| 30.02 | 2.00 | 0.00 | 5.42 | 0.16 | 0.00 | 30.18 | 2.00 | 0.00 | 5.40 | 0.16 | 0.00 |
| 30.35 | 2.00 | 0.00 | 5.37 | 0.16 | 0.00 | 30.51 | 2.00 | 0.00 | 5.35 | 0.16 | 0.00 |
| 30.68 | 2.00 | 0.00 | 5.32 | 0.16 | 0.00 | 30.84 | 2.00 | 0.00 | 5.30 | 0.16 | 0.00 |
| 31.00 | 2.00 | 0.00 | 5.27 | 0.16 | 0.00 | 31.17 | 2.00 | 0.00 | 5.25 | 0.16 | 0.00 |
| 31.33 | 2.00 | 0.00 | 5.22 | 0.16 | 0.00 | 31.50 | 2.00 | 0.00 | 5.20 | 0.16 | 0.00 |

## :: Liquefaction Potential Index calculation data :: (continued)

| Depth (ft) | FS | FL | $\mathrm{w}_{\mathrm{z}}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI | Depth <br> (ft) | FS | FL | $\mathrm{w}_{\text {z }}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 31.66 | 1.91 | 0.00 | 5.17 | 0.16 | 0.00 | 31.82 | 1.98 | 0.00 | 5.15 | 0.16 | 0.00 |
| 31.99 | 2.00 | 0.00 | 5.12 | 0.16 | 0.00 | 32.15 | 2.00 | 0.00 | 5.10 | 0.16 | 0.00 |
| 32.32 | 2.00 | 0.00 | 5.07 | 0.16 | 0.00 | 32.48 | 2.00 | 0.00 | 5.05 | 0.16 | 0.00 |
| 32.64 | 2.00 | 0.00 | 5.02 | 0.16 | 0.00 | 32.81 | 2.00 | 0.00 | 5.00 | 0.16 | 0.00 |
| 32.97 | 2.00 | 0.00 | 4.97 | 0.16 | 0.00 | 33.14 | 2.00 | 0.00 | 4.95 | 0.16 | 0.00 |
| 33.30 | 2.00 | 0.00 | 4.92 | 0.16 | 0.00 | 33.46 | 1.95 | 0.00 | 4.90 | 0.16 | 0.00 |
| 33.63 | 1.53 | 0.00 | 4.87 | 0.16 | 0.00 | 33.79 | 1.23 | 0.00 | 4.85 | 0.16 | 0.00 |
| 33.96 | 1.07 | 0.00 | 4.82 | 0.16 | 0.00 | 34.12 | 1.03 | 0.00 | 4.80 | 0.16 | 0.00 |
| 34.28 | 1.06 | 0.00 | 4.77 | 0.16 | 0.00 | 34.45 | 1.10 | 0.00 | 4.75 | 0.16 | 0.00 |
| 34.61 | 1.16 | 0.00 | 4.72 | 0.16 | 0.00 | 34.78 | 1.24 | 0.00 | 4.70 | 0.16 | 0.00 |
| 34.94 | 1.34 | 0.00 | 4.67 | 0.16 | 0.00 | 35.10 | 1.47 | 0.00 | 4.65 | 0.16 | 0.00 |
| 35.27 | 1.66 | 0.00 | 4.62 | 0.16 | 0.00 | 35.43 | 1.85 | 0.00 | 4.60 | 0.16 | 0.00 |
| 35.60 | 1.86 | 0.00 | 4.57 | 0.16 | 0.00 | 35.76 | 1.72 | 0.00 | 4.55 | 0.16 | 0.00 |
| 35.93 | 1.57 | 0.00 | 4.52 | 0.16 | 0.00 | 36.09 | 1.42 | 0.00 | 4.50 | 0.16 | 0.00 |
| 36.25 | 1.28 | 0.00 | 4.47 | 0.16 | 0.00 | 36.42 | 1.22 | 0.00 | 4.45 | 0.16 | 0.00 |
| 36.58 | 1.32 | 0.00 | 4.42 | 0.16 | 0.00 | 36.75 | 1.56 | 0.00 | 4.40 | 0.16 | 0.00 |
| 36.91 | 1.82 | 0.00 | 4.37 | 0.16 | 0.00 | 37.07 | 2.00 | 0.00 | 4.35 | 0.16 | 0.00 |
| 37.24 | 2.00 | 0.00 | 4.32 | 0.16 | 0.00 | 37.40 | 2.00 | 0.00 | 4.30 | 0.16 | 0.00 |
| 37.57 | 2.00 | 0.00 | 4.27 | 0.16 | 0.00 | 37.73 | 2.00 | 0.00 | 4.25 | 0.16 | 0.00 |
| 37.89 | 1.66 | 0.00 | 4.22 | 0.16 | 0.00 | 38.06 | 1.24 | 0.00 | 4.20 | 0.16 | 0.00 |
| 38.22 | 0.97 | 0.03 | 4.17 | 0.16 | 0.01 | 38.39 | 0.80 | 0.20 | 4.15 | 0.16 | 0.04 |
| 38.55 | 0.74 | 0.26 | 4.12 | 0.16 | 0.05 | 38.71 | 0.72 | 0.28 | 4.10 | 0.16 | 0.06 |
| 38.88 | 0.72 | 0.28 | 4.07 | 0.16 | 0.06 | 39.04 | 0.69 | 0.31 | 4.05 | 0.16 | 0.06 |
| 39.21 | 0.61 | 0.39 | 4.02 | 0.16 | 0.08 | 39.37 | 0.57 | 0.43 | 4.00 | 0.16 | 0.09 |
| 39.53 | 0.57 | 0.43 | 3.97 | 0.16 | 0.08 | 39.70 | 0.60 | 0.40 | 3.95 | 0.16 | 0.08 |
| 39.86 | 0.59 | 0.41 | 3.92 | 0.16 | 0.08 | 40.03 | 0.59 | 0.41 | 3.90 | 0.16 | 0.08 |
| 40.19 | 2.00 | 0.00 | 3.87 | 0.16 | 0.00 | 40.35 | 2.00 | 0.00 | 3.85 | 0.16 | 0.00 |
| 40.52 | 2.00 | 0.00 | 3.82 | 0.16 | 0.00 | 40.68 | 2.00 | 0.00 | 3.80 | 0.16 | 0.00 |
| 40.85 | 2.00 | 0.00 | 3.77 | 0.16 | 0.00 | 41.01 | 2.00 | 0.00 | 3.75 | 0.16 | 0.00 |
| 41.17 | 2.00 | 0.00 | 3.72 | 0.16 | 0.00 | 41.34 | 2.00 | 0.00 | 3.70 | 0.16 | 0.00 |
| 41.50 | 2.00 | 0.00 | 3.67 | 0.16 | 0.00 | 41.67 | 2.00 | 0.00 | 3.65 | 0.16 | 0.00 |
| 41.83 | 2.00 | 0.00 | 3.62 | 0.16 | 0.00 | 41.99 | 1.94 | 0.00 | 3.60 | 0.16 | 0.00 |
| 42.16 | 1.79 | 0.00 | 3.57 | 0.16 | 0.00 | 42.32 | 1.73 | 0.00 | 3.55 | 0.16 | 0.00 |
| 42.49 | 1.71 | 0.00 | 3.52 | 0.16 | 0.00 | 42.65 | 1.73 | 0.00 | 3.50 | 0.16 | 0.00 |
| 42.81 | 1.72 | 0.00 | 3.47 | 0.16 | 0.00 | 42.98 | 1.77 | 0.00 | 3.45 | 0.16 | 0.00 |
| 43.14 | 1.78 | 0.00 | 3.42 | 0.16 | 0.00 | 43.31 | 1.78 | 0.00 | 3.40 | 0.16 | 0.00 |
| 43.47 | 1.68 | 0.00 | 3.37 | 0.16 | 0.00 | 43.64 | 1.71 | 0.00 | 3.35 | 0.16 | 0.00 |
| 43.80 | 1.91 | 0.00 | 3.32 | 0.16 | 0.00 | 43.96 | 2.00 | 0.00 | 3.30 | 0.16 | 0.00 |
| 44.13 | 2.00 | 0.00 | 3.27 | 0.16 | 0.00 | 44.29 | 2.00 | 0.00 | 3.25 | 0.16 | 0.00 |
| 44.46 | 2.00 | 0.00 | 3.22 | 0.16 | 0.00 | 44.62 | 1.61 | 0.00 | 3.20 | 0.16 | 0.00 |
| 44.78 | 0.61 | 0.39 | 3.17 | 0.16 | 0.06 | 44.95 | 0.83 | 0.17 | 3.15 | 0.16 | 0.03 |
| 45.11 | 2.00 | 0.00 | 3.12 | 0.16 | 0.00 | 45.28 | 2.00 | 0.00 | 3.10 | 0.16 | 0.00 |
| 45.44 | 2.00 | 0.00 | 3.07 | 0.16 | 0.00 | 45.60 | 2.00 | 0.00 | 3.05 | 0.16 | 0.00 |
| 45.77 | 0.84 | 0.16 | 3.02 | 0.16 | 0.02 | 45.93 | 0.93 | 0.07 | 3.00 | 0.16 | 0.01 |
| 46.10 | 2.00 | 0.00 | 2.97 | 0.16 | 0.00 | 46.26 | 2.00 | 0.00 | 2.95 | 0.16 | 0.00 |
| 46.42 | 2.00 | 0.00 | 2.92 | 0.16 | 0.00 | 46.59 | 2.00 | 0.00 | 2.90 | 0.16 | 0.00 |
| 46.75 | 2.00 | 0.00 | 2.87 | 0.16 | 0.00 | 46.92 | 2.00 | 0.00 | 2.85 | 0.16 | 0.00 |
| 47.08 | 2.00 | 0.00 | 2.82 | 0.16 | 0.00 | 47.24 | 2.00 | 0.00 | 2.80 | 0.16 | 0.00 |


| : Liquefaction Potential Index calculation data :: (continued) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth <br> (ft) | FS | FL | $\mathrm{W}_{\mathrm{z}}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI | Depth (ft) | FS | FL | $\mathrm{w}_{\text {z }}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| 47.41 | 2.00 | 0.00 | 2.77 | 0.16 | 0.00 | 47.57 | 2.00 | 0.00 | 2.75 | 0.16 | 0.00 |
| 47.74 | 2.00 | 0.00 | 2.72 | 0.16 | 0.00 | 47.90 | 2.00 | 0.00 | 2.70 | 0.16 | 0.00 |
| 48.06 | 2.00 | 0.00 | 2.67 | 0.16 | 0.00 | 48.23 | 2.00 | 0.00 | 2.65 | 0.16 | 0.00 |
| 48.39 | 2.00 | 0.00 | 2.62 | 0.16 | 0.00 | 48.56 | 2.00 | 0.00 | 2.60 | 0.16 | 0.00 |
| 48.72 | 2.00 | 0.00 | 2.57 | 0.16 | 0.00 | 48.88 | 1.90 | 0.00 | 2.55 | 0.16 | 0.00 |
| 49.05 | 1.65 | 0.00 | 2.52 | 0.16 | 0.00 | 49.21 | 1.53 | 0.00 | 2.50 | 0.16 | 0.00 |
| 49.38 | 1.59 | 0.00 | 2.47 | 0.16 | 0.00 | 49.54 | 2.00 | 0.00 | 2.45 | 0.16 | 0.00 |
| 49.70 | 2.00 | 0.00 | 2.42 | 0.16 | 0.00 | 49.87 | 2.00 | 0.00 | 2.40 | 0.16 | 0.00 |
| 50.03 | 0.66 | 0.34 | 2.37 | 0.16 | 0.04 |  |  |  |  |  |  |

LPI $=0.00$ - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low LPI between 5.00 and 15.00 - Liquefaction risk high LPI > 15.00 - Liquefaction risk very high

## Abbreviations

FS: Calculated factor of safety for test point
FL: 1 - FS
$W_{z}$ : Function value of the extend of soil liquefaction according to depth
$\mathrm{d}_{\mathrm{z}}$ : $\quad$ Layer thickness (ft)
LPI: Liquefaction potential index value for test point

## :: Post-earthquake settlement of dry sands ::

| Depth <br> (ft) | Ic | Kc | Qc1n | Qc1n,cs | $\begin{aligned} & \mathrm{N} 1,60 \\ & \text { (blows) } \end{aligned}$ | Vs (ft/s) | Gmax (tsf) | CSR | Shear, Y <br> (\%) | Svol,15 <br> (\%) | Nc | ev <br> (\%) | Settle. <br> (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.16 | 1.60 | 1.00 | 122.15 | 122.15 | 22 | 227.9 | 77 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.33 | 1.56 | 1.00 | 185.72 | 185.72 | 33 | 326.7 | 177 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.49 | 1.54 | 1.00 | 201.72 | 201.72 | 36 | 380.7 | 248 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.66 | 1.58 | 1.00 | 233.76 | 233.76 | 42 | 434.0 | 334 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.82 | 1.74 | 1.07 | 234.76 | 250.66 | 48 | 464.7 | 393 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.98 | 1.94 | 1.23 | 214.81 | 263.48 | 54 | 472.7 | 413 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.15 | 2.12 | 1.49 | 183.12 | 273.70 | 60 | 464.6 | 400 | 0.14 | 0.003 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.31 | 2.26 | 1.83 | 147.14 | 268.56 | 62 | 444.1 | 363 | 0.14 | 0.003 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.48 | 2.35 | 2.13 | 116.74 | 248.40 | 60 | 418.8 | 318 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.64 | 2.38 | 2.24 | 94.37 | 210.94 | 51 | 393.7 | 276 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.80 | 2.40 | 2.31 | 78.56 | 181.18 | 45 | 373.5 | 244 | 0.14 | 0.008 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.97 | 2.41 | 2.36 | 67.87 | 160.02 | 40 | 359.5 | 223 | 0.14 | 0.011 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.13 | 2.44 | 2.47 | 59.74 | 147.49 | 37 | 349.5 | 209 | 0.14 | 0.013 | 0.01 | 11.65 | 0.01 | 0.000 |
| 2.30 | 2.46 | 2.55 | 53.51 | 136.62 | 34 | 341.5 | 197 | 0.14 | 0.017 | 0.01 | 11.65 | 0.01 | 0.000 |
| 2.46 | 2.47 | 2.64 | 48.97 | 129.34 | 33 | 336.9 | 191 | 0.14 | 0.020 | 0.01 | 11.65 | 0.01 | 0.000 |
| 2.62 | 2.47 | 2.61 | 45.77 | 119.25 | 30 | 333.1 | 185 | 0.14 | 0.023 | 0.01 | 11.65 | 0.01 | 0.000 |
| 2.79 | 2.41 | 2.35 | 46.55 | 109.52 | 27 | 338.4 | 190 | 0.14 | 0.024 | 0.02 | 11.65 | 0.01 | 0.001 |
| 2.95 | 2.33 | 2.03 | 46.98 | 95.55 | 23 | 339.0 | 189 | 0.14 | 0.026 | 0.02 | 11.65 | 0.02 | 0.001 |
| 3.12 | 2.30 | 1.94 | 45.60 | 88.68 | 21 | 337.7 | 187 | 0.14 | 0.029 | 0.03 | 11.65 | 0.02 | 0.001 |
| 3.28 | 2.32 | 2.02 | 40.96 | 82.67 | 20 | 327.8 | 174 | 0.14 | 0.038 | 0.04 | 11.65 | 0.03 | 0.001 |
| 3.44 | 2.40 | 2.31 | 36.56 | 84.52 | 21 | 322.7 | 168 | 0.14 | 0.046 | 0.04 | 11.65 | 0.04 | 0.002 |
| 3.61 | 2.45 | 2.54 | 34.37 | 87.21 | 22 | 323.4 | 169 | 0.14 | 0.048 | 0.04 | 11.65 | 0.04 | 0.002 |
| 3.77 | 2.49 | 2.72 | 34.94 | 95.15 | 24 | 336.5 | 186 | 0.14 | 0.040 | 0.03 | 11.65 | 0.03 | 0.001 |
| 3.94 | 2.52 | 2.85 | 36.84 | 105.06 | 27 | 354.1 | 209 | 0.14 | 0.031 | 0.02 | 11.65 | 0.02 | 0.001 |
| 4.10 | 2.54 | 2.97 | 38.16 | 113.43 | 30 | 369.0 | 230 | 0.14 | 0.027 | 0.02 | 11.65 | 0.01 | 0.001 |
| 4.27 | 2.56 | 3.07 | 38.54 | 118.40 | 31 | 379.1 | 245 | 0.14 | 0.025 | 0.01 | 11.65 | 0.01 | 0.001 |
| 4.43 | 2.54 | 3.00 | 40.58 | 121.73 | 32 | 393.2 | 266 | 0.14 | 0.022 | 0.01 | 11.65 | 0.01 | 0.000 |
| 4.59 | 2.47 | 2.62 | 49.25 | 129.23 | 33 | 428.4 | 322 | 0.14 | 0.016 | 0.01 | 11.65 | 0.01 | 0.000 |
| 4.76 | 2.41 | 2.37 | 58.77 | 139.33 | 34 | 465.0 | 387 | 0.14 | 0.013 | 0.01 | 11.65 | 0.01 | 0.000 |
| 4.92 | 2.40 | 2.32 | 65.99 | 152.83 | 38 | 497.1 | 449 | 0.14 | 0.011 | 0.01 | 11.65 | 0.00 | 0.000 |
| 5.09 | 2.41 | 2.37 | 67.06 | 159.15 | 39 | 510.4 | 477 | 0.14 | 0.010 | 0.00 | 11.65 | 0.00 | 0.000 |
| 5.25 | 2.43 | 2.43 | 68.48 | 166.64 | 42 | 525.4 | 509 | 0.14 | 0.010 | 0.00 | 11.65 | 0.00 | 0.000 |
| 5.41 | 2.42 | 2.40 | 70.69 | 169.62 | 42 | 539.0 | 539 | 0.14 | 0.010 | 0.00 | 11.65 | 0.00 | 0.000 |
| 5.58 | 2.44 | 2.50 | 70.27 | 176.00 | 44 | 549.3 | 562 | 0.14 | 0.009 | 0.00 | 11.65 | 0.00 | 0.000 |
| 5.74 | 2.46 | 2.57 | 65.85 | 169.00 | 43 | 541.1 | 543 | 0.14 | 0.010 | 0.00 | 11.65 | 0.00 | 0.000 |
| 5.91 | 2.50 | 2.77 | 59.21 | 164.00 | 42 | 528.2 | 514 | 0.14 | 0.011 | 0.00 | 11.65 | 0.00 | 0.000 |

Total estimated settlement: 0.01
:: Post-earthquake settlement due to soil liquefaction ::

| Depth <br> (ft) | $\mathrm{Q}_{\mathrm{tn}, \mathrm{cs}}$ | FS | $\mathrm{e}_{\mathrm{v}}(\%)$ | Settlement <br> (in) |  | Depth <br> (ft) | $\mathrm{Q}_{\mathrm{tn}, \mathrm{cs}}$ | FS | $\mathrm{e}_{\mathrm{v}}(\%)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## :: Post-earthquake settlement due to soil liquefaction :: (continued)

| Depth <br> (ft) | $Q_{\text {tr,cs }}$ | FS | $e_{\mathrm{v}}(\%)$ | Settlement <br> (in) | Depth <br> (ft) | $\mathrm{Q}_{\text {tr, }}$ cs | FS | $e_{\mathrm{v}}(\%)$ | Settlement <br> (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8.04 | 158.42 | 2.00 | 0.00 | 0.00 | 8.20 | 128.38 | 2.00 | 0.00 | 0.00 |
| 8.37 | 118.47 | 2.00 | 0.00 | 0.00 | 8.53 | 114.39 | 2.00 | 0.00 | 0.00 |
| 8.69 | 112.35 | 1.27 | 0.27 | 0.01 | 8.86 | 116.65 | 1.35 | 0.00 | 0.00 |
| 9.02 | 124.78 | 1.53 | 0.00 | 0.00 | 9.19 | 138.67 | 1.92 | 0.00 | 0.00 |
| 9.35 | 152.26 | 2.00 | 0.00 | 0.00 | 9.51 | 166.50 | 2.00 | 0.00 | 0.00 |
| 9.68 | 179.49 | 2.00 | 0.00 | 0.00 | 9.84 | 184.13 | 2.00 | 0.00 | 0.00 |
| 10.01 | 181.91 | 2.00 | 0.00 | 0.00 | 10.17 | 171.53 | 2.00 | 0.00 | 0.00 |
| 10.33 | 152.27 | 2.00 | 0.00 | 0.00 | 10.50 | 131.14 | 1.61 | 0.00 | 0.00 |
| 10.66 | 116.19 | 1.25 | 0.36 | 0.01 | 10.83 | 112.64 | 1.17 | 0.37 | 0.01 |
| 10.99 | 114.76 | 1.20 | 0.37 | 0.01 | 11.15 | 115.24 | 1.21 | 0.37 | 0.01 |
| 11.32 | 115.37 | 1.20 | 0.37 | 0.01 | 11.48 | 114.40 | 1.18 | 0.37 | 0.01 |
| 11.65 | 109.85 | 1.09 | 0.52 | 0.01 | 11.81 | 103.25 | 0.97 | 0.86 | 0.02 |
| 11.98 | 94.96 | 0.85 | 2.19 | 0.04 | 12.14 | 91.64 | 0.80 | 2.31 | 0.05 |
| 12.30 | 94.87 | 0.84 | 2.19 | 0.04 | 12.47 | 108.27 | 1.03 | 0.82 | 0.02 |
| 12.63 | 132.76 | 1.55 | 0.00 | 0.00 | 12.80 | 165.32 | 2.00 | 0.00 | 0.00 |
| 12.96 | 196.35 | 2.00 | 0.00 | 0.00 | 13.12 | 220.33 | 2.00 | 0.00 | 0.00 |
| 13.29 | 227.44 | 2.00 | 0.00 | 0.00 | 13.45 | 217.00 | 2.00 | 0.00 | 0.00 |
| 13.62 | 201.34 | 2.00 | 0.00 | 0.00 | 13.78 | 335.84 | 2.00 | 0.00 | 0.00 |
| 13.94 | 307.90 | 2.00 | 0.00 | 0.00 | 14.11 | 203.15 | 2.00 | 0.00 | 0.00 |
| 14.27 | 155.78 | 2.00 | 0.00 | 0.00 | 14.44 | 136.06 | 1.57 | 0.00 | 0.00 |
| 14.60 | 116.78 | 1.14 | 0.50 | 0.01 | 14.76 | 190.38 | 2.00 | 0.00 | 0.00 |
| 14.93 | 307.66 | 2.00 | 0.00 | 0.00 | 15.09 | 317.59 | 2.00 | 0.00 | 0.00 |
| 15.26 | 237.91 | 2.00 | 0.00 | 0.00 | 15.42 | 181.53 | 2.00 | 0.00 | 0.00 |
| 15.58 | 180.13 | 2.00 | 0.00 | 0.00 | 15.75 | 171.46 | 2.00 | 0.00 | 0.00 |
| 15.91 | 163.15 | 2.00 | 0.00 | 0.00 | 16.08 | 158.17 | 2.00 | 0.00 | 0.00 |
| 16.24 | 150.86 | 1.94 | 0.00 | 0.00 | 16.40 | 144.76 | 1.76 | 0.00 | 0.00 |
| 16.57 | 137.86 | 1.57 | 0.00 | 0.00 | 16.73 | 131.15 | 1.40 | 0.00 | 0.00 |
| 16.90 | 127.76 | 1.32 | 0.24 | 0.00 | 17.06 | 127.88 | 1.32 | 0.24 | 0.00 |
| 17.22 | 129.50 | 1.35 | 0.00 | 0.00 | 17.39 | 131.10 | 1.39 | 0.00 | 0.00 |
| 17.55 | 129.40 | 1.35 | 0.24 | 0.00 | 17.72 | 129.40 | 1.34 | 0.24 | 0.00 |
| 17.88 | 129.66 | 1.35 | 0.24 | 0.00 | 18.04 | 132.97 | 1.42 | 0.00 | 0.00 |
| 18.21 | 135.81 | 1.48 | 0.00 | 0.00 | 18.37 | 140.12 | 1.59 | 0.00 | 0.00 |
| 18.54 | 144.28 | 1.70 | 0.00 | 0.00 | 18.70 | 147.45 | 1.78 | 0.00 | 0.00 |
| 18.86 | 150.22 | 1.86 | 0.00 | 0.00 | 19.03 | 154.07 | 1.98 | 0.00 | 0.00 |
| 19.19 | 158.71 | 2.00 | 0.00 | 0.00 | 19.36 | 162.51 | 2.00 | 0.00 | 0.00 |
| 19.52 | 164.29 | 2.00 | 0.00 | 0.00 | 19.69 | 165.05 | 2.00 | 0.00 | 0.00 |
| 19.85 | 165.74 | 2.00 | 0.00 | 0.00 | 20.01 | 166.13 | 2.00 | 0.00 | 0.00 |
| 20.18 | 164.89 | 2.00 | 0.00 | 0.00 | 20.34 | 161.55 | 2.00 | 0.00 | 0.00 |
| 20.51 | 154.86 | 1.98 | 0.00 | 0.00 | 20.67 | 147.79 | 1.76 | 0.00 | 0.00 |
| 20.83 | 141.66 | 1.60 | 0.00 | 0.00 | 21.00 | 140.54 | 1.57 | 0.00 | 0.00 |
| 21.16 | 140.15 | 1.55 | 0.00 | 0.00 | 21.33 | 138.53 | 2.00 | 0.00 | 0.00 |
| 21.49 | 137.50 | 2.00 | 0.00 | 0.00 | 21.65 | 306.84 | 2.00 | 0.00 | 0.00 |
| 21.82 | 117.13 | 2.00 | 0.00 | 0.00 | 21.98 | 130.84 | 2.00 | 0.00 | 0.00 |
| 22.15 | 135.43 | 2.00 | 0.00 | 0.00 | 22.31 | 162.47 | 2.00 | 0.00 | 0.00 |
| 22.47 | 183.14 | 2.00 | 0.00 | 0.00 | 22.64 | 188.92 | 2.00 | 0.00 | 0.00 |
| 22.80 | 191.04 | 2.00 | 0.00 | 0.00 | 22.97 | 192.61 | 2.00 | 0.00 | 0.00 |
| 23.13 | 199.90 | 2.00 | 0.00 | 0.00 | 23.29 | 208.59 | 2.00 | 0.00 | 0.00 |
| 23.46 | 204.19 | 2.00 | 0.00 | 0.00 | 23.62 | 194.40 | 2.00 | 0.00 | 0.00 |


| :: Post-earthquake settlement due to soil liquefaction :: (continued) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth (ft) | $Q_{t n, c s}$ | FS | $\mathrm{e}_{\mathrm{V}}(\%)$ | Settlement (in) | Depth (ft) | $Q_{t n, c s}$ | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement (in) |
| 23.79 | 179.39 | 2.00 | 0.00 | 0.00 | 23.95 | 170.29 | 2.00 | 0.00 | 0.00 |
| 24.11 | 162.81 | 2.00 | 0.00 | 0.00 | 24.28 | 158.70 | 2.00 | 0.00 | 0.00 |
| 24.44 | 156.02 | 1.97 | 0.00 | 0.00 | 24.61 | 152.87 | 1.87 | 0.00 | 0.00 |
| 24.77 | 146.97 | 1.70 | 0.00 | 0.00 | 24.93 | 139.28 | 1.50 | 0.00 | 0.00 |
| 25.10 | 127.54 | 1.24 | 0.34 | 0.01 | 25.26 | 116.74 | 1.03 | 0.76 | 0.02 |
| 25.43 | 108.71 | 0.90 | 1.39 | 0.03 | 25.59 | 105.16 | 0.85 | 1.46 | 0.03 |
| 25.75 | 107.68 | 0.89 | 1.41 | 0.03 | 25.92 | 114.89 | 1.00 | 0.78 | 0.02 |
| 26.08 | 127.41 | 1.23 | 0.34 | 0.01 | 26.25 | 134.54 | 1.38 | 0.00 | 0.00 |
| 26.41 | 131.86 | 1.32 | 0.24 | 0.00 | 26.57 | 124.84 | 1.18 | 0.35 | 0.01 |
| 26.74 | 119.32 | 1.07 | 0.49 | 0.01 | 26.90 | 121.20 | 1.11 | 0.49 | 0.01 |
| 27.07 | 119.48 | 1.08 | 0.49 | 0.01 | 27.23 | 119.14 | 1.07 | 0.49 | 0.01 |
| 27.40 | 118.84 | 1.06 | 0.49 | 0.01 | 27.56 | 118.16 | 1.05 | 0.49 | 0.01 |
| 27.72 | 118.30 | 1.05 | 0.49 | 0.01 | 27.89 | 123.18 | 1.14 | 0.48 | 0.01 |
| 28.05 | 135.27 | 1.40 | 0.00 | 0.00 | 28.22 | 149.83 | 1.77 | 0.00 | 0.00 |
| 28.38 | 164.91 | 2.00 | 0.00 | 0.00 | 28.54 | 179.56 | 2.00 | 0.00 | 0.00 |
| 28.71 | 193.67 | 2.00 | 0.00 | 0.00 | 28.87 | 204.77 | 2.00 | 0.00 | 0.00 |
| 29.04 | 210.52 | 2.00 | 0.00 | 0.00 | 29.20 | 213.08 | 2.00 | 0.00 | 0.00 |
| 29.36 | 211.61 | 2.00 | 0.00 | 0.00 | 29.53 | 209.62 | 2.00 | 0.00 | 0.00 |
| 29.69 | 207.65 | 2.00 | 0.00 | 0.00 | 29.86 | 208.61 | 2.00 | 0.00 | 0.00 |
| 30.02 | 208.20 | 2.00 | 0.00 | 0.00 | 30.18 | 205.74 | 2.00 | 0.00 | 0.00 |
| 30.35 | 202.95 | 2.00 | 0.00 | 0.00 | 30.51 | 201.22 | 2.00 | 0.00 | 0.00 |
| 30.68 | 198.74 | 2.00 | 0.00 | 0.00 | 30.84 | 194.03 | 2.00 | 0.00 | 0.00 |
| 31.00 | 187.62 | 2.00 | 0.00 | 0.00 | 31.17 | 179.16 | 2.00 | 0.00 | 0.00 |
| 31.33 | 168.00 | 2.00 | 0.00 | 0.00 | 31.50 | 158.15 | 2.00 | 0.00 | 0.00 |
| 31.66 | 154.27 | 1.91 | 0.00 | 0.00 | 31.82 | 156.84 | 1.98 | 0.00 | 0.00 |
| 31.99 | 164.18 | 2.00 | 0.00 | 0.00 | 32.15 | 173.51 | 2.00 | 0.00 | 0.00 |
| 32.32 | 178.82 | 2.00 | 0.00 | 0.00 | 32.48 | 181.07 | 2.00 | 0.00 | 0.00 |
| 32.64 | 178.27 | 2.00 | 0.00 | 0.00 | 32.81 | 177.83 | 2.00 | 0.00 | 0.00 |
| 32.97 | 176.24 | 2.00 | 0.00 | 0.00 | 33.14 | 174.60 | 2.00 | 0.00 | 0.00 |
| 33.30 | 167.88 | 2.00 | 0.00 | 0.00 | 33.46 | 155.34 | 1.95 | 0.00 | 0.00 |
| 33.63 | 140.11 | 1.53 | 0.00 | 0.00 | 33.79 | 126.73 | 1.23 | 0.34 | 0.01 |
| 33.96 | 118.40 | 1.07 | 0.49 | 0.01 | 34.12 | 116.23 | 1.03 | 0.77 | 0.02 |
| 34.28 | 117.73 | 1.06 | 0.50 | 0.01 | 34.45 | 120.18 | 1.10 | 0.49 | 0.01 |
| 34.61 | 123.13 | 1.16 | 0.35 | 0.01 | 34.78 | 127.31 | 1.24 | 0.34 | 0.01 |
| 34.94 | 131.69 | 1.34 | 0.24 | 0.00 | 35.10 | 137.58 | 1.47 | 0.00 | 0.00 |
| 35.27 | 144.86 | 1.66 | 0.00 | 0.00 | 35.43 | 151.61 | 1.85 | 0.00 | 0.00 |
| 35.60 | 151.78 | 1.86 | 0.00 | 0.00 | 35.76 | 146.99 | 1.72 | 0.00 | 0.00 |
| 35.93 | 141.37 | 1.57 | 0.00 | 0.00 | 36.09 | 134.99 | 1.42 | 0.00 | 0.00 |
| 36.25 | 128.57 | 1.28 | 0.24 | 0.00 | 36.42 | 125.82 | 1.22 | 0.35 | 0.01 |
| 36.58 | 130.49 | 1.32 | 0.24 | 0.00 | 36.75 | 140.49 | 1.56 | 0.00 | 0.00 |
| 36.91 | 150.20 | 1.82 | 0.00 | 0.00 | 37.07 | 156.92 | 2.00 | 0.00 | 0.00 |
| 37.24 | 160.90 | 2.00 | 0.00 | 0.00 | 37.40 | 163.65 | 2.00 | 0.00 | 0.00 |
| 37.57 | 163.56 | 2.00 | 0.00 | 0.00 | 37.73 | 157.09 | 2.00 | 0.00 | 0.00 |
| 37.89 | 144.01 | 1.66 | 0.00 | 0.00 | 38.06 | 126.42 | 1.24 | 0.34 | 0.01 |
| 38.22 | 111.34 | 0.97 | 0.80 | 0.02 | 38.39 | 99.74 | 0.80 | 2.04 | 0.04 |
| 38.55 | 95.01 | 0.74 | 2.44 | 0.05 | 38.71 | 93.12 | 0.72 | 2.48 | 0.05 |
| 38.88 | 92.72 | 0.72 | 2.49 | 0.05 | 39.04 | 89.69 | 0.69 | 2.55 | 0.05 |
| 39.21 | 81.91 | 0.61 | 2.75 | 0.05 | 39.37 | 76.62 | 0.57 | 2.91 | 0.06 |


| :: Post-earthquake settlement due to soil liquefaction :: (continued) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth <br> (ft) | $\mathrm{Q}_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement (in) | Depth <br> (ft) | $\mathrm{Q}_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement (in) |
| 39.53 | 76.88 | 0.57 | 2.90 | 0.06 | 39.70 | 80.20 | 0.60 | 2.80 | 0.06 |
| 39.86 | 78.90 | 0.59 | 2.84 | 0.06 | 40.03 | 78.31 | 0.59 | 2.86 | 0.06 |
| 40.19 | 83.19 | 2.00 | 0.00 | 0.00 | 40.35 | 88.56 | 2.00 | 0.00 | 0.00 |
| 40.52 | 91.52 | 2.00 | 0.00 | 0.00 | 40.68 | 84.14 | 2.00 | 0.00 | 0.00 |
| 40.85 | 75.30 | 2.00 | 0.00 | 0.00 | 41.01 | 69.13 | 2.00 | 0.00 | 0.00 |
| 41.17 | 65.31 | 2.00 | 0.00 | 0.00 | 41.34 | 61.63 | 2.00 | 0.00 | 0.00 |
| 41.50 | 58.66 | 2.00 | 0.00 | 0.00 | 41.67 | 59.09 | 2.00 | 0.00 | 0.00 |
| 41.83 | 62.11 | 2.00 | 0.00 | 0.00 | 41.99 | 64.85 | 1.94 | 0.00 | 0.00 |
| 42.16 | 64.75 | 1.79 | 0.01 | 0.00 | 42.32 | 62.45 | 1.73 | 0.02 | 0.00 |
| 42.49 | 61.25 | 1.71 | 0.02 | 0.00 | 42.65 | 61.88 | 1.73 | 0.02 | 0.00 |
| 42.81 | 64.12 | 1.72 | 0.02 | 0.00 | 42.98 | 65.58 | 1.77 | 0.01 | 0.00 |
| 43.14 | 66.32 | 1.78 | 0.01 | 0.00 | 43.31 | 64.44 | 1.78 | 0.01 | 0.00 |
| 43.47 | 62.91 | 1.68 | 0.02 | 0.00 | 43.64 | 61.66 | 1.71 | 0.02 | 0.00 |
| 43.80 | 61.46 | 1.91 | 0.00 | 0.00 | 43.96 | 62.40 | 2.00 | 0.00 | 0.00 |
| 44.13 | 67.86 | 2.00 | 0.00 | 0.00 | 44.29 | 74.23 | 2.00 | 0.00 | 0.00 |
| 44.46 | 78.18 | 2.00 | 0.00 | 0.00 | 44.62 | 139.41 | 1.61 | 0.00 | 0.00 |
| 44.78 | 79.34 | 0.61 | 2.82 | 0.06 | 44.95 | 99.21 | 0.83 | 2.06 | 0.04 |
| 45.11 | 190.64 | 2.00 | 0.00 | 0.00 | 45.28 | 94.42 | 2.00 | 0.00 | 0.00 |
| 45.44 | 101.97 | 2.00 | 0.00 | 0.00 | 45.60 | 167.61 | 2.00 | 0.00 | 0.00 |
| 45.77 | 99.40 | 0.84 | 2.05 | 0.04 | 45.93 | 105.51 | 0.93 | 1.45 | 0.03 |
| 46.10 | 191.47 | 2.00 | 0.00 | 0.00 | 46.26 | 75.75 | 2.00 | 0.00 | 0.00 |
| 46.42 | 69.41 | 2.00 | 0.00 | 0.00 | 46.59 | 67.22 | 2.00 | 0.00 | 0.00 |
| 46.75 | 69.06 | 2.00 | 0.00 | 0.00 | 46.92 | 73.64 | 2.00 | 0.00 | 0.00 |
| 47.08 | 75.60 | 2.00 | 0.00 | 0.00 | 47.24 | 76.56 | 2.00 | 0.00 | 0.00 |
| 47.41 | 76.22 | 2.00 | 0.00 | 0.00 | 47.57 | 78.28 | 2.00 | 0.00 | 0.00 |
| 47.74 | 80.47 | 2.00 | 0.00 | 0.00 | 47.90 | 82.05 | 2.00 | 0.00 | 0.00 |
| 48.06 | 81.31 | 2.00 | 0.00 | 0.00 | 48.23 | 79.51 | 2.00 | 0.00 | 0.00 |
| 48.39 | 77.71 | 2.00 | 0.00 | 0.00 | 48.56 | 77.02 | 2.00 | 0.00 | 0.00 |
| 48.72 | 75.69 | 2.00 | 0.00 | 0.00 | 48.88 | 73.23 | 1.90 | 0.01 | 0.00 |
| 49.05 | 68.77 | 1.65 | 0.03 | 0.00 | 49.21 | 64.35 | 1.53 | 0.05 | 0.00 |
| 49.38 | 63.18 | 1.59 | 0.04 | 0.00 | 49.54 | 67.13 | 2.00 | 0.00 | 0.00 |
| 49.70 | 72.15 | 2.00 | 0.00 | 0.00 | 49.87 | 74.48 | 2.00 | 0.00 | 0.00 |

Total estimated settlement: 1.38

## Abbreviations

Qtn,cs: $\quad$ Equivalent clean sand normalized cone resistance
FS: Factor of safety against liquefaction
ev (\%):
Post-liquefaction volumentric strain
Settlement: Calculated settlement

## LIQUEFACTION ANALYSIS REPORT

## Project title : Lemoore Student Center

## CPT file : NW Corner

Input parameters and analysis data
Fines correction method: Points to test:
Earthquake magnitude $M_{w}$ :
Peak ground acceleration:

NCEER 1998
Robertson \& Wride
Based on Ic value

| G.W.T. (in-situ): | 6.00 ft |
| :--- | :--- |
| G.W.T. (earthq.): | 6.00 ft |
| Average results interval: | 3 |
| Ic cut-off value: | 2.60 |

Ic cut-off value: 2.60 Unit weight calculation: Based on SBT

## Location : West Hills College



Use fill:
Fill height:
No N/A N/A
Trans. detect. applied: Yes $\mathrm{K}_{\sigma}$ applied:

Clay like behavior applied: All soils Limit depth applied: No Limit depth:

N/A

Summary of liquefaction potential


Normalized friction ratio (\%)
Zone $A_{1}$ : Cyclic liquefaction likely depending on size and duration of cyclic loading Zone $A_{2}$ : Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

## Liquefaction analysis overall plots




Input parameters and analysis data

| Analysis method: | NCEER 1998 |
| :--- | :--- |
| Fines correction method: | Robertson \& Wride |
| Points to test: | Based on Ic value |
| Earthquake magnitude $\mathrm{M}_{\text {w }}:$ | 7.10 |
| Peak ground acceleration: | 0.25 |
| Depth to water tab |  |

Depth to water table (erthq.): 6.00 ft
Fines correction meth Points to test:

Average results interval:
Ic cut-off value:
Unit weight calculation:
Unit weight calculation: $\quad 2.60$
Unit weight calculation: Based on SBT
$\begin{array}{ll}\text { Use fill: } & \text { No } \\ \text { Fill height: } & \text { N/A }\end{array}$
Depth to water table (insitu): $\begin{aligned} & 0.25 \\ & 6.00 \mathrm{ft}\end{aligned}$
CLiq v.1.4.1.22 - CPT Liquefaction Assessment Software - Report created on: 5/24/2011, 1:37:41 PM Project file: J:\Geotechnical\Open Projects\G1100311B - Lemoore West Hills Col\liq-analysis-all4.clq



## Check for strength loss plots (Robertson (2010))







Input parameters and analysis data

| Analysis method: | NCEER 1998 |
| :--- | :--- |
| Fines correction method: | Robertson \& Wride |
| Points to test: | Based on Ic value |
| Earthquake magnitude $M_{\text {w }}:$ | 7.10 |
| Peak ground acceleration: | 0.25 |
| Depth to water table (insitu): | reo ft |

Depth to water table (erthq.): 6.00 ft
Average results interval:
$\begin{array}{ll}\text { Ic cut-off value: } & 2.60\end{array}$
Unit weight calculation: $\quad \begin{aligned} & \text { Based on SBT }\end{aligned}$
Use fill: Based
No
N/A
Fill height:
CLiq v.1.4.1.22-CPT Liquefaction Assessment Software - Report created on: 5/24/2011, 1:37:41 PM

Fill weight:
Transition detect applied N/A $\mathrm{K}_{\sigma}$ applied:
Clay like behavior applied: Limit depth applied: Limit depth:

Project file: J:\Geotechnical\Open Projects\G1100311B - Lemoore West Hills Col\liq-analysis-all4.clq

# TRANSITION LAYER DETECTION ALGORITHM REPORT Summary Details \& Plots 

## Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of $\mathrm{I}_{\mathrm{c}}$ values over which the transition will be defined (typically somewhere between $1.80<\mathrm{I}_{\mathrm{c}}<3.0$ ) and a rate of change of $I_{c}$. Transitions typically occur when the rate of change of $I_{c}$ is fast (i.e. delta $I_{c}$ is small).

The $\mathrm{SBT}_{\mathrm{n}}$ plot below, displays in red the detected transition layers based on the parameters listed below the graphs.


## Transition layer algorithm properties

$\mathrm{I}_{\mathrm{c}}$ minimum check value:
2.10
$\mathrm{I}_{\mathrm{c}}$ maximum check value:
2.92
$\mathrm{I}_{\mathrm{c}}$ change ratio value: 0.0250
Minimum number of points in layer: 4

## General statistics

Total points in CPT file: 305
Total points excluded: 41
Exclusion percentage: $13.44 \%$
Number of layers detected: 8
:: Liquefaction Potential Index calculation data ::

| Depth (ft) | FS | FL | $\mathrm{W}_{\mathrm{z}}$ | $\mathrm{d}_{2}$ | LPI | Depth <br> (ft) | FS | FL | $\mathrm{w}_{z}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.16 | 2.00 | 0.00 | 9.97 | 0.16 | 0.00 | 0.33 | 2.00 | 0.00 | 9.95 | 0.16 | 0.00 |
| 0.49 | 2.00 | 0.00 | 9.92 | 0.16 | 0.00 | 0.66 | 2.00 | 0.00 | 9.90 | 0.16 | 0.00 |
| 0.82 | 2.00 | 0.00 | 9.87 | 0.16 | 0.00 | 0.98 | 2.00 | 0.00 | 9.85 | 0.16 | 0.00 |
| 1.15 | 2.00 | 0.00 | 9.82 | 0.16 | 0.00 | 1.31 | 2.00 | 0.00 | 9.80 | 0.16 | 0.00 |
| 1.48 | 2.00 | 0.00 | 9.77 | 0.16 | 0.00 | 1.64 | 2.00 | 0.00 | 9.75 | 0.16 | 0.00 |
| 1.80 | 2.00 | 0.00 | 9.72 | 0.16 | 0.00 | 1.97 | 2.00 | 0.00 | 9.70 | 0.16 | 0.00 |
| 2.13 | 2.00 | 0.00 | 9.67 | 0.16 | 0.00 | 2.30 | 2.00 | 0.00 | 9.65 | 0.16 | 0.00 |
| 2.46 | 2.00 | 0.00 | 9.62 | 0.16 | 0.00 | 2.62 | 2.00 | 0.00 | 9.60 | 0.16 | 0.00 |
| 2.79 | 2.00 | 0.00 | 9.57 | 0.16 | 0.00 | 2.95 | 2.00 | 0.00 | 9.55 | 0.16 | 0.00 |
| 3.12 | 2.00 | 0.00 | 9.52 | 0.16 | 0.00 | 3.28 | 2.00 | 0.00 | 9.50 | 0.16 | 0.00 |
| 3.44 | 2.00 | 0.00 | 9.47 | 0.16 | 0.00 | 3.61 | 2.00 | 0.00 | 9.45 | 0.16 | 0.00 |
| 3.77 | 2.00 | 0.00 | 9.42 | 0.16 | 0.00 | 3.94 | 2.00 | 0.00 | 9.40 | 0.16 | 0.00 |
| 4.10 | 2.00 | 0.00 | 9.37 | 0.16 | 0.00 | 4.27 | 2.00 | 0.00 | 9.35 | 0.16 | 0.00 |
| 4.43 | 2.00 | 0.00 | 9.32 | 0.16 | 0.00 | 4.59 | 2.00 | 0.00 | 9.30 | 0.16 | 0.00 |
| 4.76 | 2.00 | 0.00 | 9.27 | 0.16 | 0.00 | 4.92 | 2.00 | 0.00 | 9.25 | 0.16 | 0.00 |
| 5.09 | 2.00 | 0.00 | 9.22 | 0.16 | 0.00 | 5.25 | 2.00 | 0.00 | 9.20 | 0.16 | 0.00 |
| 5.41 | 2.00 | 0.00 | 9.17 | 0.16 | 0.00 | 5.58 | 2.00 | 0.00 | 9.15 | 0.16 | 0.00 |
| 5.74 | 2.00 | 0.00 | 9.12 | 0.16 | 0.00 | 5.91 | 2.00 | 0.00 | 9.10 | 0.16 | 0.00 |
| 6.07 | 2.00 | 0.00 | 9.07 | 0.16 | 0.00 | 6.23 | 1.68 | 0.00 | 9.05 | 0.16 | 0.00 |
| 6.40 | 1.54 | 0.00 | 9.02 | 0.16 | 0.00 | 6.56 | 1.37 | 0.00 | 9.00 | 0.16 | 0.00 |
| 6.73 | 1.27 | 0.00 | 8.97 | 0.16 | 0.00 | 6.89 | 1.24 | 0.00 | 8.95 | 0.16 | 0.00 |
| 7.05 | 1.24 | 0.00 | 8.92 | 0.16 | 0.00 | 7.22 | 1.28 | 0.00 | 8.90 | 0.16 | 0.00 |
| 7.38 | 1.37 | 0.00 | 8.87 | 0.16 | 0.00 | 7.55 | 1.52 | 0.00 | 8.85 | 0.16 | 0.00 |
| 7.71 | 1.70 | 0.00 | 8.82 | 0.16 | 0.00 | 7.87 | 1.80 | 0.00 | 8.80 | 0.16 | 0.00 |
| 8.04 | 1.73 | 0.00 | 8.77 | 0.16 | 0.00 | 8.20 | 1.47 | 0.00 | 8.75 | 0.16 | 0.00 |
| 8.37 | 1.27 | 0.00 | 8.72 | 0.16 | 0.00 | 8.53 | 1.15 | 0.00 | 8.70 | 0.16 | 0.00 |
| 8.69 | 1.16 | 0.00 | 8.67 | 0.16 | 0.00 | 8.86 | 1.10 | 0.00 | 8.65 | 0.16 | 0.00 |
| 9.02 | 1.17 | 0.00 | 8.62 | 0.16 | 0.00 | 9.19 | 1.26 | 0.00 | 8.60 | 0.16 | 0.00 |
| 9.35 | 1.51 | 0.00 | 8.57 | 0.16 | 0.00 | 9.51 | 1.85 | 0.00 | 8.55 | 0.16 | 0.00 |
| 9.68 | 2.00 | 0.00 | 8.52 | 0.16 | 0.00 | 9.84 | 2.00 | 0.00 | 8.50 | 0.16 | 0.00 |
| 10.01 | 2.00 | 0.00 | 8.47 | 0.16 | 0.00 | 10.17 | 2.00 | 0.00 | 8.45 | 0.16 | 0.00 |
| 10.33 | 2.00 | 0.00 | 8.42 | 0.16 | 0.00 | 10.50 | 2.00 | 0.00 | 8.40 | 0.16 | 0.00 |
| 10.66 | 2.00 | 0.00 | 8.37 | 0.16 | 0.00 | 10.83 | 2.00 | 0.00 | 8.35 | 0.16 | 0.00 |
| 10.99 | 2.00 | 0.00 | 8.32 | 0.16 | 0.00 | 11.15 | 2.00 | 0.00 | 8.30 | 0.16 | 0.00 |
| 11.32 | 2.00 | 0.00 | 8.27 | 0.16 | 0.00 | 11.48 | 2.00 | 0.00 | 8.25 | 0.16 | 0.00 |
| 11.65 | 2.00 | 0.00 | 8.22 | 0.16 | 0.00 | 11.81 | 2.00 | 0.00 | 8.20 | 0.16 | 0.00 |
| 11.98 | 2.00 | 0.00 | 8.17 | 0.16 | 0.00 | 12.14 | 2.00 | 0.00 | 8.15 | 0.16 | 0.00 |
| 12.30 | 2.00 | 0.00 | 8.12 | 0.16 | 0.00 | 12.47 | 2.00 | 0.00 | 8.10 | 0.16 | 0.00 |
| 12.63 | 2.00 | 0.00 | 8.07 | 0.16 | 0.00 | 12.80 | 2.00 | 0.00 | 8.05 | 0.16 | 0.00 |
| 12.96 | 2.00 | 0.00 | 8.02 | 0.16 | 0.00 | 13.12 | 2.00 | 0.00 | 8.00 | 0.16 | 0.00 |
| 13.29 | 2.00 | 0.00 | 7.97 | 0.16 | 0.00 | 13.45 | 2.00 | 0.00 | 7.95 | 0.16 | 0.00 |
| 13.62 | 2.00 | 0.00 | 7.92 | 0.16 | 0.00 | 13.78 | 1.22 | 0.00 | 7.90 | 0.16 | 0.00 |
| 13.94 | 1.13 | 0.00 | 7.87 | 0.16 | 0.00 | 14.11 | 1.15 | 0.00 | 7.85 | 0.16 | 0.00 |
| 14.27 | 1.18 | 0.00 | 7.82 | 0.16 | 0.00 | 14.44 | 1.20 | 0.00 | 7.80 | 0.16 | 0.00 |
| 14.60 | 1.21 | 0.00 | 7.77 | 0.16 | 0.00 | 14.76 | 1.25 | 0.00 | 7.75 | 0.16 | 0.00 |
| 14.93 | 1.40 | 0.00 | 7.72 | 0.16 | 0.00 | 15.09 | 1.68 | 0.00 | 7.70 | 0.16 | 0.00 |
| 15.26 | 1.88 | 0.00 | 7.67 | 0.16 | 0.00 | 15.42 | 1.75 | 0.00 | 7.65 | 0.16 | 0.00 |
| 15.58 | 1.79 | 0.00 | 7.62 | 0.16 | 0.00 | 15.75 | 2.00 | 0.00 | 7.60 | 0.16 | 0.00 |

## :: Liquefaction Potential Index calculation data :: (continued)

| Depth (ft) | FS | FL | $\mathrm{w}_{2}$ | $\mathrm{d}_{2}$ | LPI | Depth <br> (ft) | FS | FL | $\mathrm{W}_{\mathrm{z}}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15.91 | 2.00 | 0.00 | 7.57 | 0.16 | 0.00 | 16.08 | 2.00 | 0.00 | 7.55 | 0.16 | 0.00 |
| 16.24 | 2.00 | 0.00 | 7.52 | 0.16 | 0.00 | 16.40 | 2.00 | 0.00 | 7.50 | 0.16 | 0.00 |
| 16.57 | 2.00 | 0.00 | 7.47 | 0.16 | 0.00 | 16.73 | 2.00 | 0.00 | 7.45 | 0.16 | 0.00 |
| 16.90 | 2.00 | 0.00 | 7.42 | 0.16 | 0.00 | 17.06 | 2.00 | 0.00 | 7.40 | 0.16 | 0.00 |
| 17.22 | 2.00 | 0.00 | 7.37 | 0.16 | 0.00 | 17.39 | 2.00 | 0.00 | 7.35 | 0.16 | 0.00 |
| 17.55 | 2.00 | 0.00 | 7.32 | 0.16 | 0.00 | 17.72 | 2.00 | 0.00 | 7.30 | 0.16 | 0.00 |
| 17.88 | 2.00 | 0.00 | 7.27 | 0.16 | 0.00 | 18.04 | 2.00 | 0.00 | 7.25 | 0.16 | 0.00 |
| 18.21 | 2.00 | 0.00 | 7.22 | 0.16 | 0.00 | 18.37 | 1.09 | 0.00 | 7.20 | 0.16 | 0.00 |
| 18.54 | 1.36 | 0.00 | 7.17 | 0.16 | 0.00 | 18.70 | 1.39 | 0.00 | 7.15 | 0.16 | 0.00 |
| 18.86 | 1.26 | 0.00 | 7.12 | 0.16 | 0.00 | 19.03 | 1.14 | 0.00 | 7.10 | 0.16 | 0.00 |
| 19.19 | 1.09 | 0.00 | 7.07 | 0.16 | 0.00 | 19.36 | 1.08 | 0.00 | 7.05 | 0.16 | 0.00 |
| 19.52 | 1.12 | 0.00 | 7.02 | 0.16 | 0.00 | 19.69 | 1.18 | 0.00 | 7.00 | 0.16 | 0.00 |
| 19.85 | 1.16 | 0.00 | 6.97 | 0.16 | 0.00 | 20.01 | 1.10 | 0.00 | 6.95 | 0.16 | 0.00 |
| 20.18 | 1.06 | 0.00 | 6.92 | 0.16 | 0.00 | 20.34 | 1.08 | 0.00 | 6.90 | 0.16 | 0.00 |
| 20.51 | 1.13 | 0.00 | 6.87 | 0.16 | 0.00 | 20.67 | 1.19 | 0.00 | 6.85 | 0.16 | 0.00 |
| 20.83 | 1.26 | 0.00 | 6.82 | 0.16 | 0.00 | 21.00 | 1.29 | 0.00 | 6.80 | 0.16 | 0.00 |
| 21.16 | 1.33 | 0.00 | 6.77 | 0.16 | 0.00 | 21.33 | 1.33 | 0.00 | 6.75 | 0.16 | 0.00 |
| 21.49 | 1.29 | 0.00 | 6.72 | 0.16 | 0.00 | 21.65 | 1.11 | 0.00 | 6.70 | 0.16 | 0.00 |
| 21.82 | 0.95 | 0.05 | 6.67 | 0.16 | 0.02 | 21.98 | 0.86 | 0.14 | 6.65 | 0.16 | 0.05 |
| 22.15 | 0.87 | 0.13 | 6.62 | 0.16 | 0.04 | 22.31 | 0.90 | 0.10 | 6.60 | 0.16 | 0.03 |
| 22.47 | 0.93 | 0.07 | 6.57 | 0.16 | 0.02 | 22.64 | 1.09 | 0.00 | 6.55 | 0.16 | 0.00 |
| 22.80 | 1.54 | 0.00 | 6.52 | 0.16 | 0.00 | 22.97 | 2.00 | 0.00 | 6.50 | 0.16 | 0.00 |
| 23.13 | 2.00 | 0.00 | 6.47 | 0.16 | 0.00 | 23.29 | 2.00 | 0.00 | 6.45 | 0.16 | 0.00 |
| 23.46 | 2.00 | 0.00 | 6.42 | 0.16 | 0.00 | 23.62 | 1.96 | 0.00 | 6.40 | 0.16 | 0.00 |
| 23.79 | 1.46 | 0.00 | 6.37 | 0.16 | 0.00 | 23.95 | 1.22 | 0.00 | 6.35 | 0.16 | 0.00 |
| 24.11 | 1.27 | 0.00 | 6.32 | 0.16 | 0.00 | 24.28 | 1.38 | 0.00 | 6.30 | 0.16 | 0.00 |
| 24.44 | 1.45 | 0.00 | 6.27 | 0.16 | 0.00 | 24.61 | 1.44 | 0.00 | 6.25 | 0.16 | 0.00 |
| 24.77 | 1.42 | 0.00 | 6.22 | 0.16 | 0.00 | 24.93 | 1.47 | 0.00 | 6.20 | 0.16 | 0.00 |
| 25.10 | 1.53 | 0.00 | 6.17 | 0.16 | 0.00 | 25.26 | 1.67 | 0.00 | 6.15 | 0.16 | 0.00 |
| 25.43 | 1.81 | 0.00 | 6.12 | 0.16 | 0.00 | 25.59 | 1.92 | 0.00 | 6.10 | 0.16 | 0.00 |
| 25.75 | 2.00 | 0.00 | 6.07 | 0.16 | 0.00 | 25.92 | 2.00 | 0.00 | 6.05 | 0.16 | 0.00 |
| 26.08 | 2.00 | 0.00 | 6.02 | 0.16 | 0.00 | 26.25 | 2.00 | 0.00 | 6.00 | 0.16 | 0.00 |
| 26.41 | 2.00 | 0.00 | 5.97 | 0.16 | 0.00 | 26.57 | 1.86 | 0.00 | 5.95 | 0.16 | 0.00 |
| 26.74 | 1.83 | 0.00 | 5.92 | 0.16 | 0.00 | 26.90 | 1.84 | 0.00 | 5.90 | 0.16 | 0.00 |
| 27.07 | 1.90 | 0.00 | 5.87 | 0.16 | 0.00 | 27.23 | 1.89 | 0.00 | 5.85 | 0.16 | 0.00 |
| 27.40 | 1.93 | 0.00 | 5.82 | 0.16 | 0.00 | 27.56 | 1.90 | 0.00 | 5.80 | 0.16 | 0.00 |
| 27.72 | 1.79 | 0.00 | 5.77 | 0.16 | 0.00 | 27.89 | 1.58 | 0.00 | 5.75 | 0.16 | 0.00 |
| 28.05 | 1.37 | 0.00 | 5.72 | 0.16 | 0.00 | 28.22 | 1.31 | 0.00 | 5.70 | 0.16 | 0.00 |
| 28.38 | 1.44 | 0.00 | 5.67 | 0.16 | 0.00 | 28.54 | 1.76 | 0.00 | 5.65 | 0.16 | 0.00 |
| 28.71 | 2.00 | 0.00 | 5.62 | 0.16 | 0.00 | 28.87 | 2.00 | 0.00 | 5.60 | 0.16 | 0.00 |
| 29.04 | 2.00 | 0.00 | 5.57 | 0.16 | 0.00 | 29.20 | 1.96 | 0.00 | 5.55 | 0.16 | 0.00 |
| 29.36 | 1.77 | 0.00 | 5.52 | 0.16 | 0.00 | 29.53 | 1.78 | 0.00 | 5.50 | 0.16 | 0.00 |
| 29.69 | 1.91 | 0.00 | 5.47 | 0.16 | 0.00 | 29.86 | 2.00 | 0.00 | 5.45 | 0.16 | 0.00 |
| 30.02 | 2.00 | 0.00 | 5.42 | 0.16 | 0.00 | 30.18 | 2.00 | 0.00 | 5.40 | 0.16 | 0.00 |
| 30.35 | 2.00 | 0.00 | 5.37 | 0.16 | 0.00 | 30.51 | 2.00 | 0.00 | 5.35 | 0.16 | 0.00 |
| 30.68 | 2.00 | 0.00 | 5.32 | 0.16 | 0.00 | 30.84 | 2.00 | 0.00 | 5.30 | 0.16 | 0.00 |
| 31.00 | 2.00 | 0.00 | 5.27 | 0.16 | 0.00 | 31.17 | 2.00 | 0.00 | 5.25 | 0.16 | 0.00 |
| 31.33 | 2.00 | 0.00 | 5.22 | 0.16 | 0.00 | 31.50 | 2.00 | 0.00 | 5.20 | 0.16 | 0.00 |

:: Liquefaction Potential Index calculation data :: (continued)

| Depth (ft) | FS | FL | $\mathrm{W}_{\mathrm{z}}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI | Depth (ft) | FS | FL | Wz | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 31.66 | 2.00 | 0.00 | 5.17 | 0.16 | 0.00 | 31.82 | 1.99 | 0.00 | 5.15 | 0.16 | 0.00 |
| 31.99 | 1.82 | 0.00 | 5.12 | 0.16 | 0.00 | 32.15 | 1.75 | 0.00 | 5.10 | 0.16 | 0.00 |
| 32.32 | 1.80 | 0.00 | 5.07 | 0.16 | 0.00 | 32.48 | 1.86 | 0.00 | 5.05 | 0.16 | 0.00 |
| 32.64 | 1.87 | 0.00 | 5.02 | 0.16 | 0.00 | 32.81 | 1.84 | 0.00 | 5.00 | 0.16 | 0.00 |
| 32.97 | 1.77 | 0.00 | 4.97 | 0.16 | 0.00 | 33.14 | 1.67 | 0.00 | 4.95 | 0.16 | 0.00 |
| 33.30 | 1.51 | 0.00 | 4.92 | 0.16 | 0.00 | 33.46 | 1.31 | 0.00 | 4.90 | 0.16 | 0.00 |
| 33.63 | 1.13 | 0.00 | 4.87 | 0.16 | 0.00 | 33.79 | 1.01 | 0.00 | 4.85 | 0.16 | 0.00 |
| 33.96 | 0.91 | 0.09 | 4.82 | 0.16 | 0.02 | 34.12 | 0.82 | 0.18 | 4.80 | 0.16 | 0.04 |
| 34.28 | 0.75 | 0.25 | 4.77 | 0.16 | 0.06 | 34.45 | 0.71 | 0.29 | 4.75 | 0.16 | 0.07 |
| 34.61 | 0.71 | 0.29 | 4.72 | 0.16 | 0.07 | 34.78 | 0.76 | 0.24 | 4.70 | 0.16 | 0.06 |
| 34.94 | 0.84 | 0.16 | 4.67 | 0.16 | 0.04 | 35.10 | 0.94 | 0.06 | 4.65 | 0.16 | 0.01 |
| 35.27 | 1.06 | 0.00 | 4.62 | 0.16 | 0.00 | 35.43 | 1.24 | 0.00 | 4.60 | 0.16 | 0.00 |
| 35.60 | 1.44 | 0.00 | 4.57 | 0.16 | 0.00 | 35.76 | 1.50 | 0.00 | 4.55 | 0.16 | 0.00 |
| 35.93 | 1.41 | 0.00 | 4.52 | 0.16 | 0.00 | 36.09 | 1.29 | 0.00 | 4.50 | 0.16 | 0.00 |
| 36.25 | 1.24 | 0.00 | 4.47 | 0.16 | 0.00 | 36.42 | 2.00 | 0.00 | 4.45 | 0.16 | 0.00 |
| 36.58 | 2.00 | 0.00 | 4.42 | 0.16 | 0.00 | 36.75 | 2.00 | 0.00 | 4.40 | 0.16 | 0.00 |
| 36.91 | 2.00 | 0.00 | 4.37 | 0.16 | 0.00 | 37.07 | 2.00 | 0.00 | 4.35 | 0.16 | 0.00 |
| 37.24 | 2.00 | 0.00 | 4.32 | 0.16 | 0.00 | 37.40 | 2.00 | 0.00 | 4.30 | 0.16 | 0.00 |
| 37.57 | 2.00 | 0.00 | 4.27 | 0.16 | 0.00 | 37.73 | 1.91 | 0.00 | 4.25 | 0.16 | 0.00 |
| 37.89 | 1.86 | 0.00 | 4.22 | 0.16 | 0.00 | 38.06 | 2.00 | 0.00 | 4.20 | 0.16 | 0.00 |
| 38.22 | 2.00 | 0.00 | 4.17 | 0.16 | 0.00 | 38.39 | 2.00 | 0.00 | 4.15 | 0.16 | 0.00 |
| 38.55 | 2.00 | 0.00 | 4.12 | 0.16 | 0.00 | 38.71 | 2.00 | 0.00 | 4.10 | 0.16 | 0.00 |
| 38.88 | 2.00 | 0.00 | 4.07 | 0.16 | 0.00 | 39.04 | 2.00 | 0.00 | 4.05 | 0.16 | 0.00 |
| 39.21 | 2.00 | 0.00 | 4.02 | 0.16 | 0.00 | 39.37 | 2.00 | 0.00 | 4.00 | 0.16 | 0.00 |
| 39.53 | 2.00 | 0.00 | 3.97 | 0.16 | 0.00 | 39.70 | 2.00 | 0.00 | 3.95 | 0.16 | 0.00 |
| 39.86 | 1.68 | 0.00 | 3.92 | 0.16 | 0.00 | 40.03 | 1.54 | 0.00 | 3.90 | 0.16 | 0.00 |
| 40.19 | 1.59 | 0.00 | 3.87 | 0.16 | 0.00 | 40.35 | 1.63 | 0.00 | 3.85 | 0.16 | 0.00 |
| 40.52 | 1.57 | 0.00 | 3.82 | 0.16 | 0.00 | 40.68 | 1.43 | 0.00 | 3.80 | 0.16 | 0.00 |
| 40.85 | 1.31 | 0.00 | 3.77 | 0.16 | 0.00 | 41.01 | 1.28 | 0.00 | 3.75 | 0.16 | 0.00 |
| 41.17 | 1.72 | 0.00 | 3.72 | 0.16 | 0.00 | 41.34 | 2.00 | 0.00 | 3.70 | 0.16 | 0.00 |
| 41.50 | 2.00 | 0.00 | 3.67 | 0.16 | 0.00 | 41.67 | 2.00 | 0.00 | 3.65 | 0.16 | 0.00 |
| 41.83 | 1.88 | 0.00 | 3.62 | 0.16 | 0.00 | 41.99 | 1.61 | 0.00 | 3.60 | 0.16 | 0.00 |
| 42.16 | 1.62 | 0.00 | 3.57 | 0.16 | 0.00 | 42.32 | 1.71 | 0.00 | 3.55 | 0.16 | 0.00 |
| 42.49 | 1.95 | 0.00 | 3.52 | 0.16 | 0.00 | 42.65 | 2.00 | 0.00 | 3.50 | 0.16 | 0.00 |
| 42.81 | 2.00 | 0.00 | 3.47 | 0.16 | 0.00 | 42.98 | 2.00 | 0.00 | 3.45 | 0.16 | 0.00 |
| 43.14 | 2.00 | 0.00 | 3.42 | 0.16 | 0.00 | 43.31 | 2.00 | 0.00 | 3.40 | 0.16 | 0.00 |
| 43.47 | 2.00 | 0.00 | 3.37 | 0.16 | 0.00 | 43.64 | 2.00 | 0.00 | 3.35 | 0.16 | 0.00 |
| 43.80 | 0.80 | 0.20 | 3.32 | 0.16 | 0.03 | 43.96 | 1.15 | 0.00 | 3.30 | 0.16 | 0.00 |
| 44.13 | 1.86 | 0.00 | 3.27 | 0.16 | 0.00 | 44.29 | 1.84 | 0.00 | 3.25 | 0.16 | 0.00 |
| 44.46 | 1.56 | 0.00 | 3.22 | 0.16 | 0.00 | 44.62 | 2.00 | 0.00 | 3.20 | 0.16 | 0.00 |
| 44.78 | 2.00 | 0.00 | 3.17 | 0.16 | 0.00 | 44.95 | 2.00 | 0.00 | 3.15 | 0.16 | 0.00 |
| 45.11 | 2.00 | 0.00 | 3.12 | 0.16 | 0.00 | 45.28 | 2.00 | 0.00 | 3.10 | 0.16 | 0.00 |
| 45.44 | 2.00 | 0.00 | 3.07 | 0.16 | 0.00 | 45.60 | 2.00 | 0.00 | 3.05 | 0.16 | 0.00 |
| 45.77 | 2.00 | 0.00 | 3.02 | 0.16 | 0.00 | 45.93 | 2.00 | 0.00 | 3.00 | 0.16 | 0.00 |
| 46.10 | 2.00 | 0.00 | 2.97 | 0.16 | 0.00 | 46.26 | 2.00 | 0.00 | 2.95 | 0.16 | 0.00 |
| 46.42 | 2.00 | 0.00 | 2.92 | 0.16 | 0.00 | 46.59 | 2.00 | 0.00 | 2.90 | 0.16 | 0.00 |
| 46.75 | 2.00 | 0.00 | 2.87 | 0.16 | 0.00 | 46.92 | 2.00 | 0.00 | 2.85 | 0.16 | 0.00 |
| 47.08 | 2.00 | 0.00 | 2.82 | 0.16 | 0.00 | 47.24 | 2.00 | 0.00 | 2.80 | 0.16 | 0.00 |


| :: Liquefaction Potential Index calculation data :: (continued) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth <br> (ft) | FS | FL | $\mathrm{W}_{\mathrm{z}}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI | Depth (ft) | FS | FL | $\mathrm{w}_{\mathrm{z}}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| 47.41 | 2.00 | 0.00 | 2.77 | 0.16 | 0.00 | 47.57 | 2.00 | 0.00 | 2.75 | 0.16 | 0.00 |
| 47.74 | 2.00 | 0.00 | 2.72 | 0.16 | 0.00 | 47.90 | 2.00 | 0.00 | 2.70 | 0.16 | 0.00 |
| 48.06 | 1.95 | 0.00 | 2.67 | 0.16 | 0.00 | 48.23 | 1.89 | 0.00 | 2.65 | 0.16 | 0.00 |
| 48.39 | 1.88 | 0.00 | 2.62 | 0.16 | 0.00 | 48.56 | 1.89 | 0.00 | 2.60 | 0.16 | 0.00 |
| 48.72 | 2.00 | 0.00 | 2.57 | 0.16 | 0.00 | 48.88 | 2.00 | 0.00 | 2.55 | 0.16 | 0.00 |
| 49.05 | 2.00 | 0.00 | 2.52 | 0.16 | 0.00 | 49.21 | 2.00 | 0.00 | 2.50 | 0.16 | 0.00 |
| 49.38 | 2.00 | 0.00 | 2.47 | 0.16 | 0.00 | 49.54 | 2.00 | 0.00 | 2.45 | 0.16 | 0.00 |
| 49.70 | 2.00 | 0.00 | 2.42 | 0.16 | 0.00 | 49.87 | 2.00 | 0.00 | 2.40 | 0.16 | 0.00 |
| 50.03 | 0.29 | 0.71 | 2.37 | 0.16 | 0.08 |  |  |  |  |  |  |

LPI $=0.00$ - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low LPI between 5.00 and 15.00 - Liquefaction risk high LPI > 15.00 - Liquefaction risk very high

## Abbreviations

FS: Calculated factor of safety for test point
FL: 1 - FS
$\mathrm{w}_{z}$ : Function value of the extend of soil liquefaction according to depth
$\mathrm{d}_{\mathrm{z}}$ : $\quad$ Layer thickness (ft)
LPI: Liquefaction potential index value for test point
:: Post-earthquake settlement of dry sands ::

| Depth <br> (ft) | Ic | Kc | Qc1n | Qc1n,cs | $\begin{aligned} & \mathrm{N} 1,60 \\ & \text { (blows) } \end{aligned}$ | $\begin{gathered} \mathrm{Vs} \\ (\mathrm{ft} / \mathrm{s}) \end{gathered}$ | Gmax (tsf) | CSR | Shear, Y (\%) | Svol,15 (\%) | Nc | ev <br> (\%) | Settle. <br> (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.16 | 1.17 | 1.00 | 252.37 | 252.37 | 40 | 365.7 | 218 | 0.14 | 0.001 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.33 | 1.39 | 1.00 | 299.58 | 299.58 | 50 | 439.1 | 342 | 0.14 | 0.001 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.49 | 1.49 | 1.00 | 285.39 | 285.39 | 50 | 456.2 | 374 | 0.14 | 0.001 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.66 | 1.60 | 1.00 | 262.21 | 262.21 | 47 | 469.9 | 401 | 0.14 | 0.001 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.82 | 1.67 | 1.02 | 242.40 | 246.68 | 46 | 476.4 | 413 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.98 | 1.73 | 1.06 | 228.04 | 240.68 | 45 | 484.9 | 430 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.15 | 1.79 | 1.10 | 219.25 | 240.55 | 46 | 497.6 | 456 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.31 | 1.84 | 1.14 | 204.60 | 233.31 | 46 | 501.9 | 465 | 0.14 | 0.003 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.48 | 1.88 | 1.17 | 183.25 | 214.77 | 43 | 491.7 | 444 | 0.14 | 0.003 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.64 | 1.92 | 1.21 | 163.36 | 197.66 | 40 | 481.9 | 424 | 0.14 | 0.004 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.80 | 2.02 | 1.32 | 152.64 | 202.21 | 42 | 488.5 | 438 | 0.14 | 0.004 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.97 | 2.15 | 1.56 | 144.04 | 224.46 | 50 | 502.0 | 469 | 0.14 | 0.004 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.13 | 2.27 | 1.86 | 129.46 | 240.98 | 56 | 502.7 | 472 | 0.14 | 0.004 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.30 | 2.34 | 2.07 | 115.51 | 239.54 | 57 | 495.6 | 457 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.46 | 2.35 | 2.13 | 106.20 | 225.78 | 54 | 489.4 | 444 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.62 | 2.35 | 2.11 | 101.68 | 214.22 | 51 | 490.0 | 444 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.79 | 2.35 | 2.13 | 98.14 | 208.67 | 50 | 493.1 | 449 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.95 | 2.37 | 2.20 | 92.99 | 204.98 | 50 | 494.4 | 451 | 0.14 | 0.007 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.12 | 2.38 | 2.24 | 90.54 | 202.76 | 49 | 499.2 | 461 | 0.14 | 0.007 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.28 | 2.33 | 2.07 | 95.90 | 198.11 | 47 | 516.3 | 495 | 0.14 | 0.007 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.44 | 2.26 | 1.84 | 107.07 | 196.57 | 46 | 543.1 | 552 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.61 | 2.20 | 1.67 | 119.52 | 199.35 | 45 | 571.7 | 617 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.77 | 2.16 | 1.58 | 128.76 | 202.85 | 45 | 594.7 | 673 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.94 | 2.17 | 1.59 | 129.91 | 206.12 | 46 | 607.2 | 704 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.10 | 2.20 | 1.66 | 125.01 | 207.50 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 4.27 | 2.26 | 1.82 | 113.18 | 205.61 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 4.43 | 2.33 | 2.03 | 98.13 | 199.56 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 4.59 | 2.42 | 2.40 | 79.81 | 191.26 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 4.76 | 2.54 | 2.98 | 62.16 | 185.34 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 4.92 | 2.63 | 3.51 | 51.67 | 181.52 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 5.09 | 2.66 | 3.70 | 48.47 | 179.28 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 5.25 | 2.65 | 3.65 | 50.01 | 182.49 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 5.41 | 2.61 | 3.36 | 54.87 | 184.39 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 5.58 | 2.55 | 3.02 | 61.66 | 186.06 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 5.74 | 2.44 | 2.50 | 71.42 | 178.38 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |
| 5.91 | 2.29 | 1.91 | 80.35 | 153.57 | 0 | 0.0 | 0 | 0.14 | 0.000 | 0.00 | 0.00 | 0.00 | 0.000 |

Total estimated settlement: 0.00

| :: Post-earthquake settlement due to soil liquefaction :: |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth (ft) | $\mathrm{Q}_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement (in) | Depth (ft) | $Q_{t n, c s}$ | FS | $\mathrm{e}_{\mathrm{V}}(\%)$ | Settlement (in) |
| 6.07 | 134.97 | 2.00 | 0.00 | 0.00 | 6.23 | 119.47 | 1.68 | 0.00 | 0.00 |
| 6.40 | 115.24 | 1.54 | 0.00 | 0.00 | 6.56 | 108.66 | 1.37 | 0.00 | 0.00 |
| 6.73 | 105.15 | 1.27 | 0.28 | 0.01 | 6.89 | 104.26 | 1.24 | 0.39 | 0.01 |
| 7.05 | 105.14 | 1.24 | 0.39 | 0.01 | 7.22 | 107.35 | 1.28 | 0.27 | 0.01 |
| 7.38 | 112.17 | 1.37 | 0.00 | 0.00 | 7.55 | 118.90 | 1.52 | 0.00 | 0.00 |
| 7.71 | 126.36 | 1.70 | 0.00 | 0.00 | 7.87 | 130.51 | 1.80 | 0.00 | 0.00 |

## :: Post-earthquake settlement due to soil liquefaction :: (continued)

| Depth <br> (ft) | $Q_{t n, c s}$ | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement <br> (in) | Depth <br> (ft) | $\mathrm{Q}_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}(\%)$ | Settlement (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8.04 | 128.57 | 1.73 | 0.00 | 0.00 | 8.20 | 119.11 | 1.47 | 0.00 | 0.00 |
| 8.37 | 110.98 | 1.27 | 0.27 | 0.01 | 8.53 | 105.63 | 1.15 | 0.39 | 0.01 |
| 8.69 | 106.60 | 1.16 | 0.39 | 0.01 | 8.86 | 103.87 | 1.10 | 0.54 | 0.01 |
| 9.02 | 107.76 | 1.17 | 0.38 | 0.01 | 9.19 | 112.74 | 1.26 | 0.27 | 0.01 |
| 9.35 | 124.18 | 1.51 | 0.00 | 0.00 | 9.51 | 136.86 | 1.85 | 0.00 | 0.00 |
| 9.68 | 153.80 | 2.00 | 0.00 | 0.00 | 9.84 | 166.09 | 2.00 | 0.00 | 0.00 |
| 10.01 | 170.03 | 2.00 | 0.00 | 0.00 | 10.17 | 168.42 | 2.00 | 0.00 | 0.00 |
| 10.33 | 162.64 | 2.00 | 0.00 | 0.00 | 10.50 | 160.78 | 2.00 | 0.00 | 0.00 |
| 10.66 | 166.28 | 2.00 | 0.00 | 0.00 | 10.83 | 174.45 | 2.00 | 0.00 | 0.00 |
| 10.99 | 186.44 | 2.00 | 0.00 | 0.00 | 11.15 | 202.10 | 2.00 | 0.00 | 0.00 |
| 11.32 | 219.08 | 2.00 | 0.00 | 0.00 | 11.48 | 395.32 | 2.00 | 0.00 | 0.00 |
| 11.65 | 198.27 | 2.00 | 0.00 | 0.00 | 11.81 | 179.09 | 2.00 | 0.00 | 0.00 |
| 11.98 | 390.78 | 2.00 | 0.00 | 0.00 | 12.14 | 406.80 | 2.00 | 0.00 | 0.00 |
| 12.30 | 179.27 | 2.00 | 0.00 | 0.00 | 12.47 | 473.23 | 2.00 | 0.00 | 0.00 |
| 12.63 | 455.26 | 2.00 | 0.00 | 0.00 | 12.80 | 430.54 | 2.00 | 0.00 | 0.00 |
| 12.96 | 277.60 | 2.00 | 0.00 | 0.00 | 13.12 | 174.35 | 2.00 | 0.00 | 0.00 |
| 13.29 | 160.46 | 2.00 | 0.00 | 0.00 | 13.45 | 144.12 | 2.00 | 0.00 | 0.00 |
| 13.62 | 128.47 | 2.00 | 0.00 | 0.00 | 13.78 | 119.05 | 1.22 | 0.36 | 0.01 |
| 13.94 | 114.91 | 1.13 | 0.50 | 0.01 | 14.11 | 116.12 | 1.15 | 0.36 | 0.01 |
| 14.27 | 117.99 | 1.18 | 0.36 | 0.01 | 14.44 | 118.87 | 1.20 | 0.36 | 0.01 |
| 14.60 | 119.76 | 1.21 | 0.36 | 0.01 | 14.76 | 121.51 | 1.25 | 0.35 | 0.01 |
| 14.93 | 128.80 | 1.40 | 0.00 | 0.00 | 15.09 | 139.89 | 1.68 | 0.00 | 0.00 |
| 15.26 | 147.00 | 1.88 | 0.00 | 0.00 | 15.42 | 142.71 | 1.75 | 0.00 | 0.00 |
| 15.58 | 144.24 | 1.79 | 0.00 | 0.00 | 15.75 | 152.30 | 2.00 | 0.00 | 0.00 |
| 15.91 | 165.29 | 2.00 | 0.00 | 0.00 | 16.08 | 177.39 | 2.00 | 0.00 | 0.00 |
| 16.24 | 185.55 | 2.00 | 0.00 | 0.00 | 16.40 | 184.72 | 2.00 | 0.00 | 0.00 |
| 16.57 | 176.76 | 2.00 | 0.00 | 0.00 | 16.73 | 177.11 | 2.00 | 0.00 | 0.00 |
| 16.90 | 240.36 | 2.00 | 0.00 | 0.00 | 17.06 | 171.06 | 2.00 | 0.00 | 0.00 |
| 17.22 | 176.92 | 2.00 | 0.00 | 0.00 | 17.39 | 185.96 | 2.00 | 0.00 | 0.00 |
| 17.55 | 191.65 | 2.00 | 0.00 | 0.00 | 17.72 | 187.39 | 2.00 | 0.00 | 0.00 |
| 17.88 | 164.30 | 2.00 | 0.00 | 0.00 | 18.04 | 134.92 | 2.00 | 0.00 | 0.00 |
| 18.21 | 114.07 | 2.00 | 0.00 | 0.00 | 18.37 | 116.41 | 1.09 | 0.50 | 0.01 |
| 18.54 | 129.93 | 1.36 | 0.00 | 0.00 | 18.70 | 131.37 | 1.39 | 0.00 | 0.00 |
| 18.86 | 125.28 | 1.26 | 0.25 | 0.00 | 19.03 | 119.65 | 1.14 | 0.49 | 0.01 |
| 19.19 | 116.96 | 1.09 | 0.50 | 0.01 | 19.36 | 116.32 | 1.08 | 0.50 | 0.01 |
| 19.52 | 118.66 | 1.12 | 0.49 | 0.01 | 19.69 | 122.27 | 1.18 | 0.35 | 0.01 |
| 19.85 | 120.90 | 1.16 | 0.35 | 0.01 | 20.01 | 117.82 | 1.10 | 0.50 | 0.01 |
| 20.18 | 116.14 | 1.06 | 0.50 | 0.01 | 20.34 | 117.37 | 1.08 | 0.50 | 0.01 |
| 20.51 | 120.07 | 1.13 | 0.49 | 0.01 | 20.67 | 123.11 | 1.19 | 0.35 | 0.01 |
| 20.83 | 126.70 | 1.26 | 0.24 | 0.00 | 21.00 | 128.23 | 1.29 | 0.24 | 0.00 |
| 21.16 | 130.00 | 1.33 | 0.24 | 0.00 | 21.33 | 130.28 | 1.33 | 0.24 | 0.00 |
| 21.49 | 128.44 | 1.29 | 0.24 | 0.00 | 21.65 | 119.56 | 1.11 | 0.49 | 0.01 |
| 21.82 | 109.85 | 0.95 | 1.36 | 0.03 | 21.98 | 104.26 | 0.86 | 1.47 | 0.03 |
| 22.15 | 104.96 | 0.87 | 1.46 | 0.03 | 22.31 | 107.39 | 0.90 | 1.41 | 0.03 |
| 22.47 | 109.31 | 0.93 | 1.37 | 0.03 | 22.64 | 119.00 | 1.09 | 0.49 | 0.01 |
| 22.80 | 139.52 | 1.54 | 0.00 | 0.00 | 22.97 | 164.85 | 2.00 | 0.00 | 0.00 |
| 23.13 | 183.35 | 2.00 | 0.00 | 0.00 | 23.29 | 185.46 | 2.00 | 0.00 | 0.00 |
| 23.46 | 174.02 | 2.00 | 0.00 | 0.00 | 23.62 | 155.07 | 1.96 | 0.00 | 0.00 |


| ost- | uake | ne | to so | uefaction |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth (ft) | $\mathrm{Qtn}_{\text {n,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement (in) | Depth (ft) | $Q_{t n, c s}$ | FS | $\mathrm{e}_{\mathrm{V}}(\%)$ | Settlement <br> (in) |
| 23.79 | 136.73 | 1.46 | 0.00 | 0.00 | 23.95 | 125.87 | 1.22 | 0.35 | 0.01 |
| 24.11 | 128.11 | 1.27 | 0.24 | 0.00 | 24.28 | 133.19 | 1.38 | 0.00 | 0.00 |
| 24.44 | 136.44 | 1.45 | 0.00 | 0.00 | 24.61 | 136.08 | 1.44 | 0.00 | 0.00 |
| 24.77 | 135.14 | 1.42 | 0.00 | 0.00 | 24.93 | 137.21 | 1.47 | 0.00 | 0.00 |
| 25.10 | 139.83 | 1.53 | 0.00 | 0.00 | 25.26 | 145.27 | 1.67 | 0.00 | 0.00 |
| 25.43 | 150.34 | 1.81 | 0.00 | 0.00 | 25.59 | 154.07 | 1.92 | 0.00 | 0.00 |
| 25.75 | 157.96 | 2.00 | 0.00 | 0.00 | 25.92 | 161.96 | 2.00 | 0.00 | 0.00 |
| 26.08 | 163.93 | 2.00 | 0.00 | 0.00 | 26.25 | 162.01 | 2.00 | 0.00 | 0.00 |
| 26.41 | 157.16 | 2.00 | 0.00 | 0.00 | 26.57 | 152.28 | 1.86 | 0.00 | 0.00 |
| 26.74 | 151.14 | 1.83 | 0.00 | 0.00 | 26.90 | 151.46 | 1.84 | 0.00 | 0.00 |
| 27.07 | 153.70 | 1.90 | 0.00 | 0.00 | 27.23 | 153.19 | 1.89 | 0.00 | 0.00 |
| 27.40 | 154.57 | 1.93 | 0.00 | 0.00 | 27.56 | 153.73 | 1.90 | 0.00 | 0.00 |
| 27.72 | 150.11 | 1.79 | 0.00 | 0.00 | 27.89 | 142.13 | 1.58 | 0.00 | 0.00 |
| 28.05 | 133.72 | 1.37 | 0.00 | 0.00 | 28.22 | 130.71 | 1.31 | 0.24 | 0.00 |
| 28.38 | 136.57 | 1.44 | 0.00 | 0.00 | 28.54 | 149.08 | 1.76 | 0.00 | 0.00 |
| 28.71 | 160.70 | 2.00 | 0.00 | 0.00 | 28.87 | 165.81 | 2.00 | 0.00 | 0.00 |
| 29.04 | 162.67 | 2.00 | 0.00 | 0.00 | 29.20 | 155.69 | 1.96 | 0.00 | 0.00 |
| 29.36 | 149.23 | 1.77 | 0.00 | 0.00 | 29.53 | 149.59 | 1.78 | 0.00 | 0.00 |
| 29.69 | 154.03 | 1.91 | 0.00 | 0.00 | 29.86 | 160.91 | 2.00 | 0.00 | 0.00 |
| 30.02 | 168.18 | 2.00 | 0.00 | 0.00 | 30.18 | 172.76 | 2.00 | 0.00 | 0.00 |
| 30.35 | 173.68 | 2.00 | 0.00 | 0.00 | 30.51 | 171.61 | 2.00 | 0.00 | 0.00 |
| 30.68 | 170.69 | 2.00 | 0.00 | 0.00 | 30.84 | 171.91 | 2.00 | 0.00 | 0.00 |
| 31.00 | 173.29 | 2.00 | 0.00 | 0.00 | 31.17 | 174.25 | 2.00 | 0.00 | 0.00 |
| 31.33 | 172.96 | 2.00 | 0.00 | 0.00 | 31.50 | 169.67 | 2.00 | 0.00 | 0.00 |
| 31.66 | 163.64 | 2.00 | 0.00 | 0.00 | 31.82 | 156.69 | 1.99 | 0.00 | 0.00 |
| 31.99 | 150.78 | 1.82 | 0.00 | 0.00 | 32.15 | 148.48 | 1.75 | 0.00 | 0.00 |
| 32.32 | 149.99 | 1.80 | 0.00 | 0.00 | 32.48 | 152.01 | 1.86 | 0.00 | 0.00 |
| 32.64 | 152.62 | 1.87 | 0.00 | 0.00 | 32.81 | 151.47 | 1.84 | 0.00 | 0.00 |
| 32.97 | 149.14 | 1.77 | 0.00 | 0.00 | 33.14 | 145.24 | 1.67 | 0.00 | 0.00 |
| 33.30 | 138.95 | 1.51 | 0.00 | 0.00 | 33.46 | 130.59 | 1.31 | 0.24 | 0.00 |
| 33.63 | 121.68 | 1.13 | 0.49 | 0.01 | 33.79 | 114.61 | 1.01 | 0.78 | 0.02 |
| 33.96 | 108.42 | 0.91 | 1.39 | 0.03 | 34.12 | 102.34 | 0.82 | 1.96 | 0.04 |
| 34.28 | 96.24 | 0.75 | 2.41 | 0.05 | 34.45 | 92.55 | 0.71 | 2.49 | 0.05 |
| 34.61 | 93.17 | 0.71 | 2.48 | 0.05 | 34.78 | 97.54 | 0.76 | 2.11 | 0.04 |
| 34.94 | 103.64 | 0.84 | 1.93 | 0.04 | 35.10 | 109.96 | 0.94 | 1.36 | 0.03 |
| 35.27 | 117.40 | 1.06 | 0.50 | 0.01 | 35.43 | 126.96 | 1.24 | 0.34 | 0.01 |
| 35.60 | 135.55 | 1.44 | 0.00 | 0.00 | 35.76 | 138.19 | 1.50 | 0.00 | 0.00 |
| 35.93 | 134.50 | 1.41 | 0.00 | 0.00 | 36.09 | 128.75 | 1.29 | 0.24 | 0.00 |
| 36.25 | 126.35 | 1.24 | 0.34 | 0.01 | 36.42 | 125.67 | 2.00 | 0.00 | 0.00 |
| 36.58 | 126.45 | 2.00 | 0.00 | 0.00 | 36.75 | 192.67 | 2.00 | 0.00 | 0.00 |
| 36.91 | 113.04 | 2.00 | 0.00 | 0.00 | 37.07 | 92.74 | 2.00 | 0.00 | 0.00 |
| 37.24 | 74.57 | 2.00 | 0.00 | 0.00 | 37.40 | 61.48 | 2.00 | 0.00 | 0.00 |
| 37.57 | 56.29 | 2.00 | 0.00 | 0.00 | 37.73 | 56.82 | 1.91 | 0.00 | 0.00 |
| 37.89 | 59.67 | 1.86 | 0.01 | 0.00 | 38.06 | 63.93 | 2.00 | 0.00 | 0.00 |
| 38.22 | 67.51 | 2.00 | 0.00 | 0.00 | 38.39 | 71.34 | 2.00 | 0.00 | 0.00 |
| 38.55 | 72.40 | 2.00 | 0.00 | 0.00 | 38.71 | 78.26 | 2.00 | 0.00 | 0.00 |
| 38.88 | 82.39 | 2.00 | 0.00 | 0.00 | 39.04 | 85.25 | 2.00 | 0.00 | 0.00 |
| 39.21 | 81.33 | 2.00 | 0.00 | 0.00 | 39.37 | 76.68 | 2.00 | 0.00 | 0.00 |

:: Post-earthquake settlement due to soil liquefaction :: (continued)

| Depth (ft) | $\mathrm{Q}_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement (in) | Depth (ft) | $Q_{t n, c s}$ | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39.53 | 71.39 | 2.00 | 0.00 | 0.00 | 39.70 | 66.30 | 2.00 | 0.00 | 0.00 |
| 39.86 | 60.77 | 1.68 | 0.02 | 0.00 | 40.03 | 58.75 | 1.54 | 0.04 | 0.00 |
| 40.19 | 59.27 | 1.59 | 0.03 | 0.00 | 40.35 | 60.24 | 1.63 | 0.03 | 0.00 |
| 40.52 | 58.62 | 1.57 | 0.04 | 0.00 | 40.68 | 55.01 | 1.43 | 0.06 | 0.00 |
| 40.85 | 52.25 | 1.31 | 0.10 | 0.00 | 41.01 | 53.86 | 1.28 | 0.11 | 0.00 |
| 41.17 | 57.45 | 1.72 | 0.02 | 0.00 | 41.34 | 59.08 | 2.00 | 0.00 | 0.00 |
| 41.50 | 56.93 | 2.00 | 0.00 | 0.00 | 41.67 | 57.88 | 2.00 | 0.00 | 0.00 |
| 41.83 | 58.61 | 1.88 | 0.01 | 0.00 | 41.99 | 61.58 | 1.61 | 0.03 | 0.00 |
| 42.16 | 63.44 | 1.62 | 0.03 | 0.00 | 42.32 | 66.25 | 1.71 | 0.02 | 0.00 |
| 42.49 | 69.46 | 1.95 | 0.00 | 0.00 | 42.65 | 72.82 | 2.00 | 0.00 | 0.00 |
| 42.81 | 72.51 | 2.00 | 0.00 | 0.00 | 42.98 | 75.24 | 2.00 | 0.00 | 0.00 |
| 43.14 | 82.84 | 2.00 | 0.00 | 0.00 | 43.31 | 90.04 | 2.00 | 0.00 | 0.00 |
| 43.47 | 106.49 | 2.00 | 0.00 | 0.00 | 43.64 | 92.46 | 2.00 | 0.00 | 0.00 |
| 43.80 | 97.31 | 0.80 | 2.11 | 0.04 | 43.96 | 119.25 | 1.15 | 0.49 | 0.01 |
| 44.13 | 148.71 | 1.86 | 0.00 | 0.00 | 44.29 | 147.86 | 1.84 | 0.00 | 0.00 |
| 44.46 | 137.46 | 1.56 | 0.00 | 0.00 | 44.62 | 85.84 | 2.00 | 0.00 | 0.00 |
| 44.78 | 85.00 | 2.00 | 0.00 | 0.00 | 44.95 | 84.41 | 2.00 | 0.00 | 0.00 |
| 45.11 | 87.35 | 2.00 | 0.00 | 0.00 | 45.28 | 87.87 | 2.00 | 0.00 | 0.00 |
| 45.44 | 188.38 | 2.00 | 0.00 | 0.00 | 45.60 | 79.82 | 2.00 | 0.00 | 0.00 |
| 45.77 | 76.00 | 2.00 | 0.00 | 0.00 | 45.93 | 73.00 | 2.00 | 0.00 | 0.00 |
| 46.10 | 69.86 | 2.00 | 0.00 | 0.00 | 46.26 | 68.00 | 2.00 | 0.00 | 0.00 |
| 46.42 | 69.84 | 2.00 | 0.00 | 0.00 | 46.59 | 74.12 | 2.00 | 0.00 | 0.00 |
| 46.75 | 77.84 | 2.00 | 0.00 | 0.00 | 46.92 | 80.64 | 2.00 | 0.00 | 0.00 |
| 47.08 | 82.15 | 2.00 | 0.00 | 0.00 | 47.24 | 82.92 | 2.00 | 0.00 | 0.00 |
| 47.41 | 82.43 | 2.00 | 0.00 | 0.00 | 47.57 | 80.20 | 2.00 | 0.00 | 0.00 |
| 47.74 | 76.31 | 2.00 | 0.00 | 0.00 | 47.90 | 72.36 | 2.00 | 0.00 | 0.00 |
| 48.06 | 70.80 | 1.95 | 0.00 | 0.00 | 48.23 | 70.07 | 1.89 | 0.01 | 0.00 |
| 48.39 | 69.46 | 1.88 | 0.01 | 0.00 | 48.56 | 67.88 | 1.89 | 0.01 | 0.00 |
| 48.72 | 67.79 | 2.00 | 0.00 | 0.00 | 48.88 | 69.14 | 2.00 | 0.00 | 0.00 |
| 49.05 | 71.29 | 2.00 | 0.00 | 0.00 | 49.21 | 73.64 | 2.00 | 0.00 | 0.00 |
| 49.38 | 76.84 | 2.00 | 0.00 | 0.00 | 49.54 | 80.14 | 2.00 | 0.00 | 0.00 |
| 49.70 | 69.21 | 2.00 | 0.00 | 0.00 | 49.87 | 53.37 | 2.00 | 0.00 | 0.00 |

## Abbreviations

| Qttn,cs: $^{\text {FS: }}$ | Equivalent clean sand normalized cone resistance |
| :--- | :--- |
| $\mathrm{e}_{\mathrm{v}}(\%):$ | Factor of safety against liquefaction |
| Settlement: | Post-liquefaction volumentric strain |
| Calculated settlement |  |

## LIQUEFACTION ANALYSIS REPORT

## Project title : Lemoore Student Center

## CPT file: SE Corner

Input parameters and analysis data
Fines correction method: Points to test:
Earthquake magnitude M
Peak ground acceleration:

NCEER 1998
Robertson \& Wride
Based on Ic value
0.25

| G.W.T. (in-situ): | 6.00 ft |
| :--- | :--- |
| G.W.T. (earthq.): | 6.00 ft |
| Average results interval: | 3 |
| Ic cut-off value: | 2.60 |

Ic cut-off value: 260 Unit weight calculation: Based on SBT

## Location : West Hills College

## Cone resistance



Friction Ratio


SBTn Plot


Use fill:
Fill height:
Trans, detect. applied:
$\mathrm{K}_{\sigma}$ applied:

Clay like behavior applied: All soil Limit depth applied: No Limit depth:

CRR plot


FS Plot


Summary of liquefaction potential


Normalized friction ratio (\%)
Zone $\mathrm{A}_{1}$ : Cyclic liquefaction likely depending on size and duration of cyclic loading Zone $A_{2}$ : Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

## Liquefaction analysis overall plots



## Input parameters and analysis data

## Analysis method: <br> Fines correction method: Points to test: <br> NCEER 1998 Robertson \& Wride Based on Ic value 7.10 0.25 <br> Earthquake magnitude $M_{w}$ :

Depth to water table (insitu): $\begin{aligned} & 0.00 \mathrm{ft}\end{aligned}$


Factor of safety

Depth to water table (erthq.): 6.00 ft
Average results interval:
$\begin{array}{ll}\text { Ic cut-off value: } & \begin{array}{ll}3 \\ & \end{array} .60\end{array}$
Unit weight calculation: $\quad \begin{aligned} & \text { Based on SBT }\end{aligned}$
$\begin{array}{ll}\text { Use fill: } & \text { No } \\ \text { Fill height: } & \text { N/A }\end{array}$

CLiq v.1.4.1.22 - CPT Liquefaction Assessment Software - Report created on: 5/24/2011, 1:37:42 PM Project file: J:\Geotechnical\Open Projects\G1100311B - Lemoore West Hills Col<br>iq-analysis-all4.clq


## F.S. color scheme

Fill weight:
Transition detect N/A
$\mathrm{K}_{\sigma}$ applied:
Clay like behavior applied: Limit depth applied: Limit depth:

Yes
No
All soils
No
N/A

Almost certain it will liquefy

| $\square$ | Very likely to liquefy |
| :--- | :--- |
| $\square$ | Liquefaction and no liquefaction are equally likely |
| $\square$ | Unlike to liquefy |
| $\square$ | Almost certain it will not liquefy |Liquefaction and no liquefaction are equally likely

Almost certain it will not liquefy


LPI color scheme
$\square$ Very high risk
High riskLow risk

## Check for strength loss plots (Robertson (2010))



## Input parameters and analysis data

| Analysis method: | NCEER 1998 |
| :--- | :--- |
| Fines correction method: | Robertson \& Wride |
| Points to test: | Based on Ic value |
| Earthquake magnitude $M_{w}:$ | 7.10 |
| Peak ground acceleration: | 0.25 |
| Depth to water table (insitu): | 60 ft |

Earthquake magnitude $M_{w}$ :
Peak ground acceleration:
Depth to water table (insitu): $\begin{aligned} & 0.25 \\ & 6.00 \mathrm{ft}\end{aligned}$
Project file: J:\Geotechnical\Open Projects\G1100311B -
Project file: J:\Geotechnical\Open Projects\G1100311B - Lemoore West Hills Col \liq-analysis-all4.clq

SBTn Index



N/A
Transition detect. applied: $\mathrm{K}_{\sigma}$ applied:
Clay like behavior applied:
Limit depth applied:
Limit depth:
imit depth:
Depth to water table (erthq.): 6.00 ft
Average results interval:
Ic cut-off value: $\quad 2.60$
Unit weight calculation: $\quad$ Based on SB
$\begin{array}{ll}\text { Use fill: } & \text { No } \\ \text { Fill height: } & \text { N/A }\end{array}$
1:37:42 PM
No
All soils No
N/A

# TRANSITION LAYER DETECTION ALGORITHM REPORT Summary Details \& Plots 

## Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of $\mathrm{I}_{\mathrm{c}}$ values over which the transition will be defined (typically somewhere between $1.80<\mathrm{I}_{\mathrm{c}}<3.0$ ) and a rate of change of $I_{c}$. Transitions typically occur when the rate of change of $I_{c}$ is fast (i.e. delta $I_{c}$ is small).

The $\mathrm{SBT}_{\mathrm{n}}$ plot below, displays in red the detected transition layers based on the parameters listed below the graphs.


## Transition layer algorithm properties

$\mathrm{I}_{\mathrm{c}}$ minimum check value:
2.10
$\mathrm{I}_{\mathrm{c}}$ maximum check value:
2.92
$I_{c}$ change ratio value: 0.0250
Minimum number of points in layer: 4

## General statistics

Total points in CPT file: 305
Total points excluded: 36
Exclusion percentage: $11.80 \%$
Number of layers detected: 8
:: Liquefaction Potential Index calculation data ::

| Depth (ft) | FS | FL | $\mathrm{W}_{2}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI | Depth (ft) | FS | FL | $\mathrm{W}_{\mathrm{z}}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.16 | 2.00 | 0.00 | 9.97 | 0.16 | 0.00 | 0.33 | 2.00 | 0.00 | 9.95 | 0.16 | 0.00 |
| 0.49 | 2.00 | 0.00 | 9.92 | 0.16 | 0.00 | 0.66 | 2.00 | 0.00 | 9.90 | 0.16 | 0.00 |
| 0.82 | 2.00 | 0.00 | 9.87 | 0.16 | 0.00 | 0.98 | 2.00 | 0.00 | 9.85 | 0.16 | 0.00 |
| 1.15 | 2.00 | 0.00 | 9.82 | 0.16 | 0.00 | 1.31 | 2.00 | 0.00 | 9.80 | 0.16 | 0.00 |
| 1.48 | 2.00 | 0.00 | 9.77 | 0.16 | 0.00 | 1.64 | 2.00 | 0.00 | 9.75 | 0.16 | 0.00 |
| 1.80 | 2.00 | 0.00 | 9.72 | 0.16 | 0.00 | 1.97 | 2.00 | 0.00 | 9.70 | 0.16 | 0.00 |
| 2.13 | 2.00 | 0.00 | 9.67 | 0.16 | 0.00 | 2.30 | 2.00 | 0.00 | 9.65 | 0.16 | 0.00 |
| 2.46 | 2.00 | 0.00 | 9.62 | 0.16 | 0.00 | 2.62 | 2.00 | 0.00 | 9.60 | 0.16 | 0.00 |
| 2.79 | 2.00 | 0.00 | 9.57 | 0.16 | 0.00 | 2.95 | 2.00 | 0.00 | 9.55 | 0.16 | 0.00 |
| 3.12 | 2.00 | 0.00 | 9.52 | 0.16 | 0.00 | 3.28 | 2.00 | 0.00 | 9.50 | 0.16 | 0.00 |
| 3.44 | 2.00 | 0.00 | 9.47 | 0.16 | 0.00 | 3.61 | 2.00 | 0.00 | 9.45 | 0.16 | 0.00 |
| 3.77 | 2.00 | 0.00 | 9.42 | 0.16 | 0.00 | 3.94 | 2.00 | 0.00 | 9.40 | 0.16 | 0.00 |
| 4.10 | 2.00 | 0.00 | 9.37 | 0.16 | 0.00 | 4.27 | 2.00 | 0.00 | 9.35 | 0.16 | 0.00 |
| 4.43 | 2.00 | 0.00 | 9.32 | 0.16 | 0.00 | 4.59 | 2.00 | 0.00 | 9.30 | 0.16 | 0.00 |
| 4.76 | 2.00 | 0.00 | 9.27 | 0.16 | 0.00 | 4.92 | 2.00 | 0.00 | 9.25 | 0.16 | 0.00 |
| 5.09 | 2.00 | 0.00 | 9.22 | 0.16 | 0.00 | 5.25 | 2.00 | 0.00 | 9.20 | 0.16 | 0.00 |
| 5.41 | 2.00 | 0.00 | 9.17 | 0.16 | 0.00 | 5.58 | 2.00 | 0.00 | 9.15 | 0.16 | 0.00 |
| 5.74 | 2.00 | 0.00 | 9.12 | 0.16 | 0.00 | 5.91 | 2.00 | 0.00 | 9.10 | 0.16 | 0.00 |
| 6.07 | 1.21 | 0.00 | 9.07 | 0.16 | 0.00 | 6.23 | 1.22 | 0.00 | 9.05 | 0.16 | 0.00 |
| 6.40 | 1.23 | 0.00 | 9.02 | 0.16 | 0.00 | 6.56 | 1.02 | 0.00 | 9.00 | 0.16 | 0.00 |
| 6.73 | 1.00 | 0.00 | 8.97 | 0.16 | 0.00 | 6.89 | 1.13 | 0.00 | 8.95 | 0.16 | 0.00 |
| 7.05 | 1.28 | 0.00 | 8.92 | 0.16 | 0.00 | 7.22 | 1.24 | 0.00 | 8.90 | 0.16 | 0.00 |
| 7.38 | 1.37 | 0.00 | 8.87 | 0.16 | 0.00 | 7.55 | 1.38 | 0.00 | 8.85 | 0.16 | 0.00 |
| 7.71 | 1.41 | 0.00 | 8.82 | 0.16 | 0.00 | 7.87 | 1.80 | 0.00 | 8.80 | 0.16 | 0.00 |
| 8.04 | 1.94 | 0.00 | 8.77 | 0.16 | 0.00 | 8.20 | 1.35 | 0.00 | 8.75 | 0.16 | 0.00 |
| 8.37 | 1.39 | 0.00 | 8.72 | 0.16 | 0.00 | 8.53 | 2.00 | 0.00 | 8.70 | 0.16 | 0.00 |
| 8.69 | 2.00 | 0.00 | 8.67 | 0.16 | 0.00 | 8.86 | 2.00 | 0.00 | 8.65 | 0.16 | 0.00 |
| 9.02 | 2.00 | 0.00 | 8.62 | 0.16 | 0.00 | 9.19 | 1.05 | 0.00 | 8.60 | 0.16 | 0.00 |
| 9.35 | 1.16 | 0.00 | 8.57 | 0.16 | 0.00 | 9.51 | 1.11 | 0.00 | 8.55 | 0.16 | 0.00 |
| 9.68 | 0.97 | 0.03 | 8.52 | 0.16 | 0.01 | 9.84 | 0.89 | 0.11 | 8.50 | 0.16 | 0.05 |
| 10.01 | 2.00 | 0.00 | 8.47 | 0.16 | 0.00 | 10.17 | 2.00 | 0.00 | 8.45 | 0.16 | 0.00 |
| 10.33 | 2.00 | 0.00 | 8.42 | 0.16 | 0.00 | 10.50 | 2.00 | 0.00 | 8.40 | 0.16 | 0.00 |
| 10.66 | 2.00 | 0.00 | 8.37 | 0.16 | 0.00 | 10.83 | 2.00 | 0.00 | 8.35 | 0.16 | 0.00 |
| 10.99 | 2.00 | 0.00 | 8.32 | 0.16 | 0.00 | 11.15 | 2.00 | 0.00 | 8.30 | 0.16 | 0.00 |
| 11.32 | 1.82 | 0.00 | 8.27 | 0.16 | 0.00 | 11.48 | 1.47 | 0.00 | 8.25 | 0.16 | 0.00 |
| 11.65 | 1.48 | 0.00 | 8.22 | 0.16 | 0.00 | 11.81 | 1.76 | 0.00 | 8.20 | 0.16 | 0.00 |
| 11.98 | 1.92 | 0.00 | 8.17 | 0.16 | 0.00 | 12.14 | 2.00 | 0.00 | 8.15 | 0.16 | 0.00 |
| 12.30 | 2.00 | 0.00 | 8.12 | 0.16 | 0.00 | 12.47 | 2.00 | 0.00 | 8.10 | 0.16 | 0.00 |
| 12.63 | 2.00 | 0.00 | 8.07 | 0.16 | 0.00 | 12.80 | 2.00 | 0.00 | 8.05 | 0.16 | 0.00 |
| 12.96 | 2.00 | 0.00 | 8.02 | 0.16 | 0.00 | 13.12 | 2.00 | 0.00 | 8.00 | 0.16 | 0.00 |
| 13.29 | 1.87 | 0.00 | 7.97 | 0.16 | 0.00 | 13.45 | 1.72 | 0.00 | 7.95 | 0.16 | 0.00 |
| 13.62 | 1.56 | 0.00 | 7.92 | 0.16 | 0.00 | 13.78 | 1.34 | 0.00 | 7.90 | 0.16 | 0.00 |
| 13.94 | 1.06 | 0.00 | 7.87 | 0.16 | 0.00 | 14.11 | 0.87 | 0.13 | 7.85 | 0.16 | 0.05 |
| 14.27 | 0.91 | 0.09 | 7.82 | 0.16 | 0.04 | 14.44 | 1.05 | 0.00 | 7.80 | 0.16 | 0.00 |
| 14.60 | 1.20 | 0.00 | 7.77 | 0.16 | 0.00 | 14.76 | 1.41 | 0.00 | 7.75 | 0.16 | 0.00 |
| 14.93 | 1.61 | 0.00 | 7.72 | 0.16 | 0.00 | 15.09 | 1.71 | 0.00 | 7.70 | 0.16 | 0.00 |
| 15.26 | 1.60 | 0.00 | 7.67 | 0.16 | 0.00 | 15.42 | 1.34 | 0.00 | 7.65 | 0.16 | 0.00 |
| 15.58 | 1.06 | 0.00 | 7.62 | 0.16 | 0.00 | 15.75 | 2.00 | 0.00 | 7.60 | 0.16 | 0.00 |

## :: Liquefaction Potential Index calculation data :: (continued)

| Depth <br> (ft) | FS | FL | $\mathrm{w}_{\mathrm{z}}$ | $\mathrm{d}_{2}$ | LPI | Depth <br> (ft) | FS | FL | $\mathrm{w}_{2}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15.91 | 2.00 | 0.00 | 7.57 | 0.16 | 0.00 | 16.08 | 2.00 | 0.00 | 7.55 | 0.16 | 0.00 |
| 16.24 | 2.00 | 0.00 | 7.52 | 0.16 | 0.00 | 16.40 | 2.00 | 0.00 | 7.50 | 0.16 | 0.00 |
| 16.57 | 2.00 | 0.00 | 7.47 | 0.16 | 0.00 | 16.73 | 2.00 | 0.00 | 7.45 | 0.16 | 0.00 |
| 16.90 | 0.96 | 0.04 | 7.42 | 0.16 | 0.02 | 17.06 | 1.23 | 0.00 | 7.40 | 0.16 | 0.00 |
| 17.22 | 1.77 | 0.00 | 7.37 | 0.16 | 0.00 | 17.39 | 1.95 | 0.00 | 7.35 | 0.16 | 0.00 |
| 17.55 | 2.00 | 0.00 | 7.32 | 0.16 | 0.00 | 17.72 | 2.00 | 0.00 | 7.30 | 0.16 | 0.00 |
| 17.88 | 2.00 | 0.00 | 7.27 | 0.16 | 0.00 | 18.04 | 2.00 | 0.00 | 7.25 | 0.16 | 0.00 |
| 18.21 | 2.00 | 0.00 | 7.22 | 0.16 | 0.00 | 18.37 | 2.00 | 0.00 | 7.20 | 0.16 | 0.00 |
| 18.54 | 2.00 | 0.00 | 7.17 | 0.16 | 0.00 | 18.70 | 2.00 | 0.00 | 7.15 | 0.16 | 0.00 |
| 18.86 | 2.00 | 0.00 | 7.12 | 0.16 | 0.00 | 19.03 | 2.00 | 0.00 | 7.10 | 0.16 | 0.00 |
| 19.19 | 2.00 | 0.00 | 7.07 | 0.16 | 0.00 | 19.36 | 2.00 | 0.00 | 7.05 | 0.16 | 0.00 |
| 19.52 | 2.00 | 0.00 | 7.02 | 0.16 | 0.00 | 19.69 | 2.00 | 0.00 | 7.00 | 0.16 | 0.00 |
| 19.85 | 2.00 | 0.00 | 6.97 | 0.16 | 0.00 | 20.01 | 2.00 | 0.00 | 6.95 | 0.16 | 0.00 |
| 20.18 | 2.00 | 0.00 | 6.92 | 0.16 | 0.00 | 20.34 | 2.00 | 0.00 | 6.90 | 0.16 | 0.00 |
| 20.51 | 1.72 | 0.00 | 6.87 | 0.16 | 0.00 | 20.67 | 1.45 | 0.00 | 6.85 | 0.16 | 0.00 |
| 20.83 | 1.23 | 0.00 | 6.82 | 0.16 | 0.00 | 21.00 | 0.97 | 0.03 | 6.80 | 0.16 | 0.01 |
| 21.16 | 0.85 | 0.15 | 6.77 | 0.16 | 0.05 | 21.33 | 0.95 | 0.05 | 6.75 | 0.16 | 0.02 |
| 21.49 | 1.01 | 0.00 | 6.72 | 0.16 | 0.00 | 21.65 | 1.02 | 0.00 | 6.70 | 0.16 | 0.00 |
| 21.82 | 0.93 | 0.07 | 6.67 | 0.16 | 0.02 | 21.98 | 0.89 | 0.11 | 6.65 | 0.16 | 0.04 |
| 22.15 | 0.86 | 0.14 | 6.62 | 0.16 | 0.05 | 22.31 | 0.90 | 0.10 | 6.60 | 0.16 | 0.03 |
| 22.47 | 1.00 | 0.00 | 6.57 | 0.16 | 0.00 | 22.64 | 1.16 | 0.00 | 6.55 | 0.16 | 0.00 |
| 22.80 | 1.32 | 0.00 | 6.52 | 0.16 | 0.00 | 22.97 | 1.43 | 0.00 | 6.50 | 0.16 | 0.00 |
| 23.13 | 1.32 | 0.00 | 6.47 | 0.16 | 0.00 | 23.29 | 1.18 | 0.00 | 6.45 | 0.16 | 0.00 |
| 23.46 | 1.17 | 0.00 | 6.42 | 0.16 | 0.00 | 23.62 | 1.34 | 0.00 | 6.40 | 0.16 | 0.00 |
| 23.79 | 1.48 | 0.00 | 6.37 | 0.16 | 0.00 | 23.95 | 1.39 | 0.00 | 6.35 | 0.16 | 0.00 |
| 24.11 | 1.17 | 0.00 | 6.32 | 0.16 | 0.00 | 24.28 | 1.04 | 0.00 | 6.30 | 0.16 | 0.00 |
| 24.44 | 1.04 | 0.00 | 6.27 | 0.16 | 0.00 | 24.61 | 1.15 | 0.00 | 6.25 | 0.16 | 0.00 |
| 24.77 | 1.25 | 0.00 | 6.22 | 0.16 | 0.00 | 24.93 | 1.38 | 0.00 | 6.20 | 0.16 | 0.00 |
| 25.10 | 1.43 | 0.00 | 6.17 | 0.16 | 0.00 | 25.26 | 1.40 | 0.00 | 6.15 | 0.16 | 0.00 |
| 25.43 | 1.30 | 0.00 | 6.12 | 0.16 | 0.00 | 25.59 | 1.21 | 0.00 | 6.10 | 0.16 | 0.00 |
| 25.75 | 1.18 | 0.00 | 6.07 | 0.16 | 0.00 | 25.92 | 1.21 | 0.00 | 6.05 | 0.16 | 0.00 |
| 26.08 | 1.26 | 0.00 | 6.02 | 0.16 | 0.00 | 26.25 | 1.37 | 0.00 | 6.00 | 0.16 | 0.00 |
| 26.41 | 1.47 | 0.00 | 5.97 | 0.16 | 0.00 | 26.57 | 1.55 | 0.00 | 5.95 | 0.16 | 0.00 |
| 26.74 | 1.61 | 0.00 | 5.92 | 0.16 | 0.00 | 26.90 | 1.65 | 0.00 | 5.90 | 0.16 | 0.00 |
| 27.07 | 1.75 | 0.00 | 5.87 | 0.16 | 0.00 | 27.23 | 1.96 | 0.00 | 5.85 | 0.16 | 0.00 |
| 27.40 | 2.00 | 0.00 | 5.82 | 0.16 | 0.00 | 27.56 | 2.00 | 0.00 | 5.80 | 0.16 | 0.00 |
| 27.72 | 2.00 | 0.00 | 5.77 | 0.16 | 0.00 | 27.89 | 2.00 | 0.00 | 5.75 | 0.16 | 0.00 |
| 28.05 | 2.00 | 0.00 | 5.72 | 0.16 | 0.00 | 28.22 | 2.00 | 0.00 | 5.70 | 0.16 | 0.00 |
| 28.38 | 2.00 | 0.00 | 5.67 | 0.16 | 0.00 | 28.54 | 2.00 | 0.00 | 5.65 | 0.16 | 0.00 |
| 28.71 | 2.00 | 0.00 | 5.62 | 0.16 | 0.00 | 28.87 | 2.00 | 0.00 | 5.60 | 0.16 | 0.00 |
| 29.04 | 2.00 | 0.00 | 5.57 | 0.16 | 0.00 | 29.20 | 2.00 | 0.00 | 5.55 | 0.16 | 0.00 |
| 29.36 | 1.91 | 0.00 | 5.52 | 0.16 | 0.00 | 29.53 | 1.98 | 0.00 | 5.50 | 0.16 | 0.00 |
| 29.69 | 2.00 | 0.00 | 5.47 | 0.16 | 0.00 | 29.86 | 2.00 | 0.00 | 5.45 | 0.16 | 0.00 |
| 30.02 | 2.00 | 0.00 | 5.42 | 0.16 | 0.00 | 30.18 | 2.00 | 0.00 | 5.40 | 0.16 | 0.00 |
| 30.35 | 2.00 | 0.00 | 5.37 | 0.16 | 0.00 | 30.51 | 2.00 | 0.00 | 5.35 | 0.16 | 0.00 |
| 30.68 | 2.00 | 0.00 | 5.32 | 0.16 | 0.00 | 30.84 | 2.00 | 0.00 | 5.30 | 0.16 | 0.00 |
| 31.00 | 2.00 | 0.00 | 5.27 | 0.16 | 0.00 | 31.17 | 2.00 | 0.00 | 5.25 | 0.16 | 0.00 |
| 31.33 | 1.98 | 0.00 | 5.22 | 0.16 | 0.00 | 31.50 | 1.72 | 0.00 | 5.20 | 0.16 | 0.00 |

:: Liquefaction Potential Index calculation data :: (continued)

| Depth (ft) | FS | FL | $\mathrm{w}_{\mathrm{z}}$ | $\mathrm{d}_{2}$ | LPI | Depth <br> (ft) | FS | FL | $\mathrm{w}_{\text {z }}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 31.66 | 1.48 | 0.00 | 5.17 | 0.16 | 0.00 | 31.82 | 1.22 | 0.00 | 5.15 | 0.16 | 0.00 |
| 31.99 | 2.00 | 0.00 | 5.12 | 0.16 | 0.00 | 32.15 | 2.00 | 0.00 | 5.10 | 0.16 | 0.00 |
| 32.32 | 2.00 | 0.00 | 5.07 | 0.16 | 0.00 | 32.48 | 2.00 | 0.00 | 5.05 | 0.16 | 0.00 |
| 32.64 | 2.00 | 0.00 | 5.02 | 0.16 | 0.00 | 32.81 | 2.00 | 0.00 | 5.00 | 0.16 | 0.00 |
| 32.97 | 2.00 | 0.00 | 4.97 | 0.16 | 0.00 | 33.14 | 2.00 | 0.00 | 4.95 | 0.16 | 0.00 |
| 33.30 | 2.00 | 0.00 | 4.92 | 0.16 | 0.00 | 33.46 | 1.01 | 0.00 | 4.90 | 0.16 | 0.00 |
| 33.63 | 0.83 | 0.17 | 4.87 | 0.16 | 0.04 | 33.79 | 2.00 | 0.00 | 4.85 | 0.16 | 0.00 |
| 33.96 | 2.00 | 0.00 | 4.82 | 0.16 | 0.00 | 34.12 | 0.50 | 0.50 | 4.80 | 0.16 | 0.12 |
| 34.28 | 0.59 | 0.41 | 4.77 | 0.16 | 0.10 | 34.45 | 0.75 | 0.25 | 4.75 | 0.16 | 0.06 |
| 34.61 | 0.86 | 0.14 | 4.72 | 0.16 | 0.03 | 34.78 | 0.86 | 0.14 | 4.70 | 0.16 | 0.03 |
| 34.94 | 0.79 | 0.21 | 4.67 | 0.16 | 0.05 | 35.10 | 0.77 | 0.23 | 4.65 | 0.16 | 0.05 |
| 35.27 | 2.00 | 0.00 | 4.62 | 0.16 | 0.00 | 35.43 | 2.00 | 0.00 | 4.60 | 0.16 | 0.00 |
| 35.60 | 2.00 | 0.00 | 4.57 | 0.16 | 0.00 | 35.76 | 2.00 | 0.00 | 4.55 | 0.16 | 0.00 |
| 35.93 | 2.00 | 0.00 | 4.52 | 0.16 | 0.00 | 36.09 | 0.55 | 0.45 | 4.50 | 0.16 | 0.10 |
| 36.25 | 0.55 | 0.45 | 4.47 | 0.16 | 0.10 | 36.42 | 0.56 | 0.44 | 4.45 | 0.16 | 0.10 |
| 36.58 | 0.56 | 0.44 | 4.42 | 0.16 | 0.10 | 36.75 | 2.00 | 0.00 | 4.40 | 0.16 | 0.00 |
| 36.91 | 2.00 | 0.00 | 4.37 | 0.16 | 0.00 | 37.07 | 2.00 | 0.00 | 4.35 | 0.16 | 0.00 |
| 37.24 | 2.00 | 0.00 | 4.32 | 0.16 | 0.00 | 37.40 | 1.91 | 0.00 | 4.30 | 0.16 | 0.00 |
| 37.57 | 1.83 | 0.00 | 4.27 | 0.16 | 0.00 | 37.73 | 1.70 | 0.00 | 4.25 | 0.16 | 0.00 |
| 37.89 | 1.59 | 0.00 | 4.22 | 0.16 | 0.00 | 38.06 | 1.56 | 0.00 | 4.20 | 0.16 | 0.00 |
| 38.22 | 1.65 | 0.00 | 4.17 | 0.16 | 0.00 | 38.39 | 1.80 | 0.00 | 4.15 | 0.16 | 0.00 |
| 38.55 | 1.95 | 0.00 | 4.12 | 0.16 | 0.00 | 38.71 | 2.00 | 0.00 | 4.10 | 0.16 | 0.00 |
| 38.88 | 2.00 | 0.00 | 4.07 | 0.16 | 0.00 | 39.04 | 2.00 | 0.00 | 4.05 | 0.16 | 0.00 |
| 39.21 | 2.00 | 0.00 | 4.02 | 0.16 | 0.00 | 39.37 | 2.00 | 0.00 | 4.00 | 0.16 | 0.00 |
| 39.53 | 2.00 | 0.00 | 3.97 | 0.16 | 0.00 | 39.70 | 2.00 | 0.00 | 3.95 | 0.16 | 0.00 |
| 39.86 | 2.00 | 0.00 | 3.92 | 0.16 | 0.00 | 40.03 | 2.00 | 0.00 | 3.90 | 0.16 | 0.00 |
| 40.19 | 2.00 | 0.00 | 3.87 | 0.16 | 0.00 | 40.35 | 2.00 | 0.00 | 3.85 | 0.16 | 0.00 |
| 40.52 | 2.00 | 0.00 | 3.82 | 0.16 | 0.00 | 40.68 | 2.00 | 0.00 | 3.80 | 0.16 | 0.00 |
| 40.85 | 2.00 | 0.00 | 3.77 | 0.16 | 0.00 | 41.01 | 2.00 | 0.00 | 3.75 | 0.16 | 0.00 |
| 41.17 | 2.00 | 0.00 | 3.72 | 0.16 | 0.00 | 41.34 | 2.00 | 0.00 | 3.70 | 0.16 | 0.00 |
| 41.50 | 2.00 | 0.00 | 3.67 | 0.16 | 0.00 | 41.67 | 2.00 | 0.00 | 3.65 | 0.16 | 0.00 |
| 41.83 | 1.87 | 0.00 | 3.62 | 0.16 | 0.00 | 41.99 | 1.73 | 0.00 | 3.60 | 0.16 | 0.00 |
| 42.16 | 1.89 | 0.00 | 3.57 | 0.16 | 0.00 | 42.32 | 2.00 | 0.00 | 3.55 | 0.16 | 0.00 |
| 42.49 | 2.00 | 0.00 | 3.52 | 0.16 | 0.00 | 42.65 | 2.00 | 0.00 | 3.50 | 0.16 | 0.00 |
| 42.81 | 2.00 | 0.00 | 3.47 | 0.16 | 0.00 | 42.98 | 2.00 | 0.00 | 3.45 | 0.16 | 0.00 |
| 43.14 | 2.00 | 0.00 | 3.42 | 0.16 | 0.00 | 43.31 | 2.00 | 0.00 | 3.40 | 0.16 | 0.00 |
| 43.47 | 2.00 | 0.00 | 3.37 | 0.16 | 0.00 | 43.64 | 2.00 | 0.00 | 3.35 | 0.16 | 0.00 |
| 43.80 | 2.00 | 0.00 | 3.32 | 0.16 | 0.00 | 43.96 | 2.00 | 0.00 | 3.30 | 0.16 | 0.00 |
| 44.13 | 2.00 | 0.00 | 3.27 | 0.16 | 0.00 | 44.29 | 2.00 | 0.00 | 3.25 | 0.16 | 0.00 |
| 44.46 | 2.00 | 0.00 | 3.22 | 0.16 | 0.00 | 44.62 | 2.00 | 0.00 | 3.20 | 0.16 | 0.00 |
| 44.78 | 1.03 | 0.00 | 3.17 | 0.16 | 0.00 | 44.95 | 0.61 | 0.39 | 3.15 | 0.16 | 0.06 |
| 45.11 | 0.70 | 0.30 | 3.12 | 0.16 | 0.05 | 45.28 | 2.00 | 0.00 | 3.10 | 0.16 | 0.00 |
| 45.44 | 2.00 | 0.00 | 3.07 | 0.16 | 0.00 | 45.60 | 2.00 | 0.00 | 3.05 | 0.16 | 0.00 |
| 45.77 | 2.00 | 0.00 | 3.02 | 0.16 | 0.00 | 45.93 | 2.00 | 0.00 | 3.00 | 0.16 | 0.00 |
| 46.10 | 2.00 | 0.00 | 2.97 | 0.16 | 0.00 | 46.26 | 2.00 | 0.00 | 2.95 | 0.16 | 0.00 |
| 46.42 | 2.00 | 0.00 | 2.92 | 0.16 | 0.00 | 46.59 | 2.00 | 0.00 | 2.90 | 0.16 | 0.00 |
| 46.75 | 2.00 | 0.00 | 2.87 | 0.16 | 0.00 | 46.92 | 2.00 | 0.00 | 2.85 | 0.16 | 0.00 |
| 47.08 | 2.00 | 0.00 | 2.82 | 0.16 | 0.00 | 47.24 | 2.00 | 0.00 | 2.80 | 0.16 | 0.00 |


| :: Liquefaction Potential Index calculation data :: (continued) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth <br> (ft) | FS | FL | $\mathrm{W}_{\mathrm{z}}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI | Depth <br> (ft) | FS | FL | Wz | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| 47.41 | 2.00 | 0.00 | 2.77 | 0.16 | 0.00 | 47.57 | 2.00 | 0.00 | 2.75 | 0.16 | 0.00 |
| 47.74 | 1.96 | 0.00 | 2.72 | 0.16 | 0.00 | 47.90 | 1.91 | 0.00 | 2.70 | 0.16 | 0.00 |
| 48.06 | 1.92 | 0.00 | 2.67 | 0.16 | 0.00 | 48.23 | 1.92 | 0.00 | 2.65 | 0.16 | 0.00 |
| 48.39 | 1.96 | 0.00 | 2.62 | 0.16 | 0.00 | 48.56 | 2.00 | 0.00 | 2.60 | 0.16 | 0.00 |
| 48.72 | 2.00 | 0.00 | 2.57 | 0.16 | 0.00 | 48.88 | 2.00 | 0.00 | 2.55 | 0.16 | 0.00 |
| 49.05 | 2.00 | 0.00 | 2.52 | 0.16 | 0.00 | 49.21 | 2.00 | 0.00 | 2.50 | 0.16 | 0.00 |
| 49.38 | 2.00 | 0.00 | 2.47 | 0.16 | 0.00 | 49.54 | 2.00 | 0.00 | 2.45 | 0.16 | 0.00 |
| 49.70 | 2.00 | 0.00 | 2.42 | 0.16 | 0.00 | 49.87 | 2.00 | 0.00 | 2.40 | 0.16 | 0.00 |
| 50.03 | 2.00 | 0.00 | 2.37 | 0.16 | 0.00 |  |  |  |  |  |  |

LPI $=0.00$ - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low LPI between 5.00 and 15.00 - Liquefaction risk high LPI > 15.00 - Liquefaction risk very high

## Abbreviations

FS: Calculated factor of safety for test point
FL: 1 - FS
$\mathrm{w}_{\mathrm{z}}$ : Function value of the extend of soil liquefaction according to depth
$\mathrm{d}_{z}$ : $\quad$ Layer thickness (ft)
LPI: Liquefaction potential index value for test point

## :: Post-earthquake settlement of dry sands ::

| Depth <br> (ft) | Ic | Kc | Qc1n | Qc1n,cs | N1,60 (blows) | Vs (ft/s) | Gmax (tsf) | CSR | Shear, y (\%) | Svol,15 (\%) | Nc | $\begin{gathered} \text { ev } \\ \text { (\%) } \end{gathered}$ | Settle. (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.16 | 1.54 | 1.00 | 143.11 | 143.11 | 25 | 251.5 | 97 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.33 | 1.53 | 1.00 | 207.47 | 207.47 | 37 | 349.5 | 206 | 0.14 | 0.001 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.49 | 1.51 | 1.00 | 219.14 | 219.14 | 38 | 398.7 | 275 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.66 | 1.57 | 1.00 | 250.68 | 250.68 | 45 | 451.4 | 365 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.82 | 1.72 | 1.05 | 260.74 | 274.65 | 52 | 491.0 | 445 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 0.98 | 1.89 | 1.18 | 251.40 | 295.71 | 59 | 509.2 | 486 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.15 | 2.00 | 1.30 | 231.44 | 301.71 | 63 | 518.9 | 508 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.31 | 2.09 | 1.43 | 203.87 | 291.26 | 63 | 514.2 | 499 | 0.14 | 0.002 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.48 | 2.13 | 1.50 | 178.03 | 267.77 | 59 | 503.2 | 475 | 0.14 | 0.003 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.64 | 2.17 | 1.60 | 149.72 | 239.90 | 53 | 482.1 | 431 | 0.14 | 0.004 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.80 | 2.22 | 1.73 | 125.21 | 216.10 | 49 | 460.0 | 387 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 1.97 | 2.27 | 1.85 | 105.03 | 194.75 | 45 | 438.5 | 347 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.13 | 2.25 | 1.80 | 98.08 | 176.98 | 41 | 434.2 | 338 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.30 | 2.23 | 1.75 | 97.11 | 169.56 | 39 | 441.2 | 349 | 0.14 | 0.007 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.46 | 2.23 | 1.74 | 101.62 | 177.16 | 40 | 462.3 | 388 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.62 | 2.23 | 1.74 | 104.03 | 181.26 | 41 | 478.5 | 418 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.79 | 2.14 | 1.53 | 126.39 | 193.66 | 43 | 525.9 | 514 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.95 | 2.12 | 1.49 | 144.36 | 215.48 | 47 | 570.0 | 615 | 0.14 | 0.004 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.12 | 2.16 | 1.56 | 157.91 | 246.98 | 55 | 613.9 | 727 | 0.14 | 0.004 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.28 | 2.25 | 1.80 | 147.11 | 264.33 | 61 | 622.1 | 751 | 0.14 | 0.004 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.44 | 2.29 | 1.91 | 134.91 | 258.00 | 60 | 614.1 | 729 | 0.14 | 0.004 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.61 | 2.19 | 1.65 | 134.23 | 221.64 | 50 | 604.4 | 700 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.77 | 2.06 | 1.38 | 140.42 | 193.76 | 41 | 598.6 | 680 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.94 | 1.99 | 1.29 | 144.02 | 185.53 | 38 | 601.0 | 683 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.10 | 2.03 | 1.33 | 139.24 | 185.87 | 39 | 605.9 | 696 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.27 | 1.99 | 1.29 | 143.25 | 184.79 | 38 | 614.8 | 717 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.43 | 1.85 | 1.15 | 155.88 | 178.54 | 35 | 615.9 | 714 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.59 | 1.69 | 1.03 | 168.54 | 173.41 | 32 | 608.4 | 688 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.76 | 1.60 | 1.00 | 171.08 | 171.08 | 31 | 597.1 | 655 | 0.14 | 0.007 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.92 | 1.60 | 1.00 | 167.33 | 167.33 | 30 | 595.1 | 649 | 0.14 | 0.007 | 0.00 | 11.65 | 0.00 | 0.000 |
| 5.09 | 1.62 | 1.00 | 158.41 | 158.41 | 29 | 589.5 | 635 | 0.14 | 0.008 | 0.01 | 11.65 | 0.00 | 0.000 |
| 5.25 | 1.65 | 1.00 | 144.19 | 144.81 | 27 | 573.1 | 595 | 0.14 | 0.009 | 0.01 | 11.65 | 0.01 | 0.000 |
| 5.41 | 1.68 | 1.03 | 128.76 | 132.00 | 24 | 552.1 | 546 | 0.14 | 0.010 | 0.01 | 11.65 | 0.01 | 0.000 |
| 5.58 | 1.72 | 1.05 | 113.44 | 119.03 | 22 | 529.6 | 496 | 0.14 | 0.012 | 0.01 | 11.65 | 0.01 | 0.000 |
| 5.74 | 1.77 | 1.08 | 99.91 | 108.28 | 21 | 511.1 | 457 | 0.14 | 0.014 | 0.01 | 11.65 | 0.01 | 0.000 |
| 5.91 | 1.87 | 1.16 | 86.77 | 100.79 | 20 | 500.8 | 438 | 0.14 | 0.015 | 0.02 | 11.65 | 0.01 | 0.001 |

Total estimated settlement: 0.00

| :: Post-earthquake settlement due to soil liquefaction :: |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth (ft) | $\mathrm{Q}_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}(\%)$ | Settlement (in) | Depth (ft) | $\mathrm{Qtm}_{\text {tn, }}$ | FS | $\mathrm{e}_{\mathrm{v}}(\%)$ | Settlement (in) |
| 6.07 | 98.86 | 1.21 | 0.41 | 0.01 | 6.23 | 100.43 | 1.22 | 0.40 | 0.01 |
| 6.40 | 101.60 | 1.23 | 0.40 | 0.01 | 6.56 | 90.27 | 1.02 | 0.97 | 0.02 |
| 6.73 | 89.72 | 1.00 | 0.98 | 0.02 | 6.89 | 98.35 | 1.13 | 0.56 | 0.01 |
| 7.05 | 107.04 | 1.28 | 0.28 | 0.01 | 7.22 | 105.52 | 1.24 | 0.39 | 0.01 |
| 7.38 | 112.15 | 1.37 | 0.00 | 0.00 | 7.55 | 113.30 | 1.38 | 0.00 | 0.00 |
| 7.71 | 115.25 | 1.41 | 0.00 | 0.00 | 7.87 | 130.63 | 1.80 | 0.00 | 0.00 |

## :: Post-earthquake settlement due to soil liquefaction :: (continued)

| Depth (ft) | $Q_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}(\%)$ | Settlement <br> (in) | Depth <br> (ft) | $Q_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{v}}(\%)$ | Settlement <br> (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8.04 | 135.53 | 1.94 | 0.00 | 0.00 | 8.20 | 114.53 | 1.35 | 0.00 | 0.00 |
| 8.37 | 116.67 | 1.39 | 0.00 | 0.00 | 8.53 | 107.56 | 2.00 | 0.00 | 0.00 |
| 8.69 | 77.11 | 2.00 | 0.00 | 0.00 | 8.86 | 82.37 | 2.00 | 0.00 | 0.00 |
| 9.02 | 92.39 | 2.00 | 0.00 | 0.00 | 9.19 | 102.38 | 1.05 | 0.54 | 0.01 |
| 9.35 | 108.78 | 1.16 | 0.38 | 0.01 | 9.51 | 106.74 | 1.11 | 0.53 | 0.01 |
| 9.68 | 98.64 | 0.97 | 0.89 | 0.02 | 9.84 | 93.62 | 0.89 | 1.73 | 0.03 |
| 10.01 | 93.94 | 2.00 | 0.00 | 0.00 | 10.17 | 100.26 | 2.00 | 0.00 | 0.00 |
| 10.33 | 113.24 | 2.00 | 0.00 | 0.00 | 10.50 | 130.94 | 2.00 | 0.00 | 0.00 |
| 10.66 | 170.31 | 2.00 | 0.00 | 0.00 | 10.83 | 359.34 | 2.00 | 0.00 | 0.00 |
| 10.99 | 173.03 | 2.00 | 0.00 | 0.00 | 11.15 | 328.18 | 2.00 | 0.00 | 0.00 |
| 11.32 | 140.15 | 1.82 | 0.00 | 0.00 | 11.48 | 127.46 | 1.47 | 0.00 | 0.00 |
| 11.65 | 128.22 | 1.48 | 0.00 | 0.00 | 11.81 | 139.30 | 1.76 | 0.00 | 0.00 |
| 11.98 | 144.79 | 1.92 | 0.00 | 0.00 | 12.14 | 152.68 | 2.00 | 0.00 | 0.00 |
| 12.30 | 158.39 | 2.00 | 0.00 | 0.00 | 12.47 | 164.52 | 2.00 | 0.00 | 0.00 |
| 12.63 | 169.05 | 2.00 | 0.00 | 0.00 | 12.80 | 169.49 | 2.00 | 0.00 | 0.00 |
| 12.96 | 163.85 | 2.00 | 0.00 | 0.00 | 13.12 | 153.66 | 2.00 | 0.00 | 0.00 |
| 13.29 | 145.05 | 1.87 | 0.00 | 0.00 | 13.45 | 140.07 | 1.72 | 0.00 | 0.00 |
| 13.62 | 134.64 | 1.56 | 0.00 | 0.00 | 13.78 | 125.70 | 1.34 | 0.25 | 0.00 |
| 13.94 | 111.78 | 1.06 | 0.51 | 0.01 | 14.11 | 99.93 | 0.87 | 1.57 | 0.03 |
| 14.27 | 102.56 | 0.91 | 1.51 | 0.03 | 14.44 | 111.95 | 1.05 | 0.51 | 0.01 |
| 14.60 | 119.78 | 1.20 | 0.36 | 0.01 | 14.76 | 130.06 | 1.41 | 0.00 | 0.00 |
| 14.93 | 138.17 | 1.61 | 0.00 | 0.00 | 15.09 | 141.91 | 1.71 | 0.00 | 0.00 |
| 15.26 | 138.02 | 1.60 | 0.00 | 0.00 | 15.42 | 127.44 | 1.34 | 0.24 | 0.00 |
| 15.58 | 113.55 | 1.06 | 0.51 | 0.01 | 15.75 | 106.10 | 2.00 | 0.00 | 0.00 |
| 15.91 | 110.81 | 2.00 | 0.00 | 0.00 | 16.08 | 249.38 | 2.00 | 0.00 | 0.00 |
| 16.24 | 113.71 | 2.00 | 0.00 | 0.00 | 16.40 | 106.33 | 2.00 | 0.00 | 0.00 |
| 16.57 | 99.37 | 2.00 | 0.00 | 0.00 | 16.73 | 233.44 | 2.00 | 0.00 | 0.00 |
| 16.90 | 108.84 | 0.96 | 0.82 | 0.02 | 17.06 | 124.00 | 1.23 | 0.35 | 0.01 |
| 17.22 | 146.09 | 1.77 | 0.00 | 0.00 | 17.39 | 152.47 | 1.95 | 0.00 | 0.00 |
| 17.55 | 155.36 | 2.00 | 0.00 | 0.00 | 17.72 | 156.14 | 2.00 | 0.00 | 0.00 |
| 17.88 | 156.49 | 2.00 | 0.00 | 0.00 | 18.04 | 156.19 | 2.00 | 0.00 | 0.00 |
| 18.21 | 157.17 | 2.00 | 0.00 | 0.00 | 18.37 | 255.04 | 2.00 | 0.00 | 0.00 |
| 18.54 | 140.86 | 2.00 | 0.00 | 0.00 | 18.70 | 138.54 | 2.00 | 0.00 | 0.00 |
| 18.86 | 142.30 | 2.00 | 0.00 | 0.00 | 19.03 | 156.36 | 2.00 | 0.00 | 0.00 |
| 19.19 | 158.30 | 2.00 | 0.00 | 0.00 | 19.36 | 243.95 | 2.00 | 0.00 | 0.00 |
| 19.52 | 144.74 | 2.00 | 0.00 | 0.00 | 19.69 | 150.75 | 2.00 | 0.00 | 0.00 |
| 19.85 | 162.66 | 2.00 | 0.00 | 0.00 | 20.01 | 169.29 | 2.00 | 0.00 | 0.00 |
| 20.18 | 169.49 | 2.00 | 0.00 | 0.00 | 20.34 | 156.56 | 2.00 | 0.00 | 0.00 |
| 20.51 | 146.40 | 1.72 | 0.00 | 0.00 | 20.67 | 136.08 | 1.45 | 0.00 | 0.00 |
| 20.83 | 126.12 | 1.23 | 0.34 | 0.01 | 21.00 | 112.26 | 0.97 | 0.79 | 0.02 |
| 21.16 | 104.21 | 0.85 | 1.48 | 0.03 | 21.33 | 110.62 | 0.95 | 1.35 | 0.03 |
| 21.49 | 114.45 | 1.01 | 0.78 | 0.02 | 21.65 | 115.17 | 1.02 | 0.77 | 0.02 |
| 21.82 | 110.10 | 0.93 | 1.36 | 0.03 | 21.98 | 107.34 | 0.89 | 1.41 | 0.03 |
| 22.15 | 105.36 | 0.86 | 1.45 | 0.03 | 22.31 | 107.87 | 0.90 | 1.40 | 0.03 |
| 22.47 | 114.42 | 1.00 | 0.78 | 0.02 | 22.64 | 123.51 | 1.16 | 0.35 | 0.01 |
| 22.80 | 131.45 | 1.32 | 0.24 | 0.00 | 22.97 | 136.05 | 1.43 | 0.00 | 0.00 |
| 23.13 | 131.21 | 1.32 | 0.24 | 0.00 | 23.29 | 124.94 | 1.18 | 0.35 | 0.01 |
| 23.46 | 124.05 | 1.17 | 0.35 | 0.01 | 23.62 | 132.49 | 1.34 | 0.24 | 0.00 |


| Post-e | quake s | ment | to soil | uefaction |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth <br> (ft) | $\mathrm{Q}_{\text {tn,cs }}$ | FS | $e_{\mathrm{V}}(\%)$ | Settlement <br> (in) | Depth <br> (ft) | $Q_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}(\%)$ | Settlement <br> (in) |
| 23.79 | 138.34 | 1.48 | 0.00 | 0.00 | 23.95 | 134.87 | 1.39 | 0.00 | 0.00 |
| 24.11 | 124.33 | 1.17 | 0.35 | 0.01 | 24.28 | 117.50 | 1.04 | 0.76 | 0.01 |
| 24.44 | 117.55 | 1.04 | 0.76 | 0.01 | 24.61 | 123.59 | 1.15 | 0.35 | 0.01 |
| 24.77 | 128.65 | 1.25 | 0.24 | 0.00 | 24.93 | 134.54 | 1.38 | 0.00 | 0.00 |
| 25.10 | 136.89 | 1.43 | 0.00 | 0.00 | 25.26 | 135.37 | 1.40 | 0.00 | 0.00 |
| 25.43 | 131.03 | 1.30 | 0.24 | 0.00 | 25.59 | 126.64 | 1.21 | 0.34 | 0.01 |
| 25.75 | 125.24 | 1.18 | 0.35 | 0.01 | 25.92 | 126.70 | 1.21 | 0.34 | 0.01 |
| 26.08 | 129.33 | 1.26 | 0.24 | 0.00 | 26.25 | 134.45 | 1.37 | 0.00 | 0.00 |
| 26.41 | 138.81 | 1.47 | 0.00 | 0.00 | 26.57 | 142.15 | 1.55 | 0.00 | 0.00 |
| 26.74 | 144.40 | 1.61 | 0.00 | 0.00 | 26.90 | 145.79 | 1.65 | 0.00 | 0.00 |
| 27.07 | 149.61 | 1.75 | 0.00 | 0.00 | 27.23 | 156.62 | 1.96 | 0.00 | 0.00 |
| 27.40 | 171.62 | 2.00 | 0.00 | 0.00 | 27.56 | 188.78 | 2.00 | 0.00 | 0.00 |
| 27.72 | 200.34 | 2.00 | 0.00 | 0.00 | 27.89 | 202.35 | 2.00 | 0.00 | 0.00 |
| 28.05 | 197.70 | 2.00 | 0.00 | 0.00 | 28.22 | 193.32 | 2.00 | 0.00 | 0.00 |
| 28.38 | 189.92 | 2.00 | 0.00 | 0.00 | 28.54 | 185.89 | 2.00 | 0.00 | 0.00 |
| 28.71 | 180.20 | 2.00 | 0.00 | 0.00 | 28.87 | 172.34 | 2.00 | 0.00 | 0.00 |
| 29.04 | 163.79 | 2.00 | 0.00 | 0.00 | 29.20 | 158.37 | 2.00 | 0.00 | 0.00 |
| 29.36 | 155.14 | 1.91 | 0.00 | 0.00 | 29.53 | 157.47 | 1.98 | 0.00 | 0.00 |
| 29.69 | 161.76 | 2.00 | 0.00 | 0.00 | 29.86 | 168.87 | 2.00 | 0.00 | 0.00 |
| 30.02 | 176.05 | 2.00 | 0.00 | 0.00 | 30.18 | 180.90 | 2.00 | 0.00 | 0.00 |
| 30.35 | 185.69 | 2.00 | 0.00 | 0.00 | 30.51 | 189.99 | 2.00 | 0.00 | 0.00 |
| 30.68 | 192.54 | 2.00 | 0.00 | 0.00 | 30.84 | 188.79 | 2.00 | 0.00 | 0.00 |
| 31.00 | 179.61 | 2.00 | 0.00 | 0.00 | 31.17 | 167.83 | 2.00 | 0.00 | 0.00 |
| 31.33 | 157.31 | 1.98 | 0.00 | 0.00 | 31.50 | 148.47 | 1.72 | 0.00 | 0.00 |
| 31.66 | 139.21 | 1.48 | 0.00 | 0.00 | 31.82 | 127.43 | 1.22 | 0.34 | 0.01 |
| 31.99 | 120.30 | 2.00 | 0.00 | 0.00 | 32.15 | 261.41 | 2.00 | 0.00 | 0.00 |
| 32.32 | 95.56 | 2.00 | 0.00 | 0.00 | 32.48 | 77.17 | 2.00 | 0.00 | 0.00 |
| 32.64 | 62.48 | 2.00 | 0.00 | 0.00 | 32.81 | 56.63 | 2.00 | 0.00 | 0.00 |
| 32.97 | 54.84 | 2.00 | 0.00 | 0.00 | 33.14 | 55.10 | 2.00 | 0.00 | 0.00 |
| 33.30 | 53.55 | 2.00 | 0.00 | 0.00 | 33.46 | 115.79 | 1.01 | 0.77 | 0.02 |
| 33.63 | 103.80 | 0.83 | 1.92 | 0.04 | 33.79 | 55.87 | 2.00 | 0.00 | 0.00 |
| 33.96 | 162.12 | 2.00 | 0.00 | 0.00 | 34.12 | 70.15 | 0.50 | 3.12 | 0.06 |
| 34.28 | 82.23 | 0.59 | 2.74 | 0.05 | 34.45 | 97.82 | 0.75 | 2.10 | 0.04 |
| 34.61 | 106.12 | 0.86 | 1.44 | 0.03 | 34.78 | 106.16 | 0.86 | 1.44 | 0.03 |
| 34.94 | 100.76 | 0.79 | 2.01 | 0.04 | 35.10 | 99.13 | 0.77 | 2.06 | 0.04 |
| 35.27 | 205.02 | 2.00 | 0.00 | 0.00 | 35.43 | 93.28 | 2.00 | 0.00 | 0.00 |
| 35.60 | 85.94 | 2.00 | 0.00 | 0.00 | 35.76 | 85.85 | 2.00 | 0.00 | 0.00 |
| 35.93 | 196.17 | 2.00 | 0.00 | 0.00 | 36.09 | 76.71 | 0.55 | 2.90 | 0.06 |
| 36.25 | 76.96 | 0.55 | 2.90 | 0.06 | 36.42 | 78.27 | 0.56 | 2.86 | 0.06 |
| 36.58 | 77.29 | 0.56 | 2.89 | 0.06 | 36.75 | 159.71 | 2.00 | 0.00 | 0.00 |
| 36.91 | 67.03 | 2.00 | 0.00 | 0.00 | 37.07 | 52.49 | 2.00 | 0.00 | 0.00 |
| 37.24 | 42.13 | 2.00 | 0.00 | 0.00 | 37.40 | 39.90 | 1.91 | 0.00 | 0.00 |
| 37.57 | 40.81 | 1.83 | 0.01 | 0.00 | 37.73 | 42.55 | 1.70 | 0.02 | 0.00 |
| 37.89 | 42.53 | 1.59 | 0.03 | 0.00 | 38.06 | 45.33 | 1.56 | 0.04 | 0.00 |
| 38.22 | 47.20 | 1.65 | 0.02 | 0.00 | 38.39 | 50.68 | 1.80 | 0.01 | 0.00 |
| 38.55 | 52.89 | 1.95 | 0.00 | 0.00 | 38.71 | 54.88 | 2.00 | 0.00 | 0.00 |
| 38.88 | 57.13 | 2.00 | 0.00 | 0.00 | 39.04 | 59.22 | 2.00 | 0.00 | 0.00 |
| 39.21 | 63.38 | 2.00 | 0.00 | 0.00 | 39.37 | 69.78 | 2.00 | 0.00 | 0.00 |

## :: Post-earthquake settlement due to soil liquefaction :: (continued)

| Depth (ft) | $\mathrm{Q}_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}(\%)$ | Settlement (in) | Depth (ft) | Qtn,cs | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39.53 | 73.49 | 2.00 | 0.00 | 0.00 | 39.70 | 74.24 | 2.00 | 0.00 | 0.00 |
| 39.86 | 71.39 | 2.00 | 0.00 | 0.00 | 40.03 | 70.37 | 2.00 | 0.00 | 0.00 |
| 40.19 | 70.58 | 2.00 | 0.00 | 0.00 | 40.35 | 70.71 | 2.00 | 0.00 | 0.00 |
| 40.52 | 69.87 | 2.00 | 0.00 | 0.00 | 40.68 | 68.63 | 2.00 | 0.00 | 0.00 |
| 40.85 | 73.31 | 2.00 | 0.00 | 0.00 | 41.01 | 81.17 | 2.00 | 0.00 | 0.00 |
| 41.17 | 86.59 | 2.00 | 0.00 | 0.00 | 41.34 | 84.64 | 2.00 | 0.00 | 0.00 |
| 41.50 | 77.29 | 2.00 | 0.00 | 0.00 | 41.67 | 67.96 | 2.00 | 0.00 | 0.00 |
| 41.83 | 59.51 | 1.87 | 0.01 | 0.00 | 41.99 | 53.70 | 1.73 | 0.02 | 0.00 |
| 42.16 | 55.96 | 1.89 | 0.01 | 0.00 | 42.32 | 63.56 | 2.00 | 0.00 | 0.00 |
| 42.49 | 72.89 | 2.00 | 0.00 | 0.00 | 42.65 | 79.18 | 2.00 | 0.00 | 0.00 |
| 42.81 | 81.81 | 2.00 | 0.00 | 0.00 | 42.98 | 82.06 | 2.00 | 0.00 | 0.00 |
| 43.14 | 81.58 | 2.00 | 0.00 | 0.00 | 43.31 | 80.94 | 2.00 | 0.00 | 0.00 |
| 43.47 | 79.94 | 2.00 | 0.00 | 0.00 | 43.64 | 78.19 | 2.00 | 0.00 | 0.00 |
| 43.80 | 75.84 | 2.00 | 0.00 | 0.00 | 43.96 | 76.30 | 2.00 | 0.00 | 0.00 |
| 44.13 | 78.17 | 2.00 | 0.00 | 0.00 | 44.29 | 80.13 | 2.00 | 0.00 | 0.00 |
| 44.46 | 79.48 | 2.00 | 0.00 | 0.00 | 44.62 | 77.74 | 2.00 | 0.00 | 0.00 |
| 44.78 | 113.81 | 1.03 | 0.78 | 0.02 | 44.95 | 80.90 | 0.61 | 2.78 | 0.05 |
| 45.11 | 89.75 | 0.70 | 2.55 | 0.05 | 45.28 | 159.87 | 2.00 | 0.00 | 0.00 |
| 45.44 | 96.65 | 2.00 | 0.00 | 0.00 | 45.60 | 218.85 | 2.00 | 0.00 | 0.00 |
| 45.77 | 170.26 | 2.00 | 0.00 | 0.00 | 45.93 | 224.32 | 2.00 | 0.00 | 0.00 |
| 46.10 | 91.63 | 2.00 | 0.00 | 0.00 | 46.26 | 94.19 | 2.00 | 0.00 | 0.00 |
| 46.42 | 119.47 | 2.00 | 0.00 | 0.00 | 46.59 | 97.44 | 2.00 | 0.00 | 0.00 |
| 46.75 | 98.51 | 2.00 | 0.00 | 0.00 | 46.92 | 199.19 | 2.00 | 0.00 | 0.00 |
| 47.08 | 87.37 | 2.00 | 0.00 | 0.00 | 47.24 | 78.96 | 2.00 | 0.00 | 0.00 |
| 47.41 | 71.62 | 2.00 | 0.00 | 0.00 | 47.57 | 65.79 | 2.00 | 0.00 | 0.00 |
| 47.74 | 63.30 | 1.96 | 0.00 | 0.00 | 47.90 | 63.99 | 1.91 | 0.00 | 0.00 |
| 48.06 | 65.91 | 1.92 | 0.00 | 0.00 | 48.23 | 66.61 | 1.92 | 0.00 | 0.00 |
| 48.39 | 68.30 | 1.96 | 0.00 | 0.00 | 48.56 | 70.89 | 2.00 | 0.00 | 0.00 |
| 48.72 | 73.23 | 2.00 | 0.00 | 0.00 | 48.88 | 74.18 | 2.00 | 0.00 | 0.00 |
| 49.05 | 74.22 | 2.00 | 0.00 | 0.00 | 49.21 | 74.34 | 2.00 | 0.00 | 0.00 |
| 49.38 | 75.22 | 2.00 | 0.00 | 0.00 | 49.54 | 76.60 | 2.00 | 0.00 | 0.00 |
| 49.70 | 78.93 | 2.00 | 0.00 | 0.00 | 49.87 | 80.49 | 2.00 | 0.00 | 0.00 |
| 50.03 | 51.91 | 2.00 | 0.00 | 0.00 |  |  |  |  |  |

## Abbreviations

| Qttn,cs: $^{\text {FS: }}$ | Equivalent clean sand normalized cone resistance |
| :--- | :--- |
| $\mathrm{e}_{\mathrm{v}}(\%):$ | Factor of safety against liquefaction |
| Settlement: | Post-liquefaction volumentric strain |
| Calculated settlement |  |

## LIQUEFACTION ANALYSIS REPORT

## Project title : Lemoore Student Center

## CPT file : SW Corner

Input parameters and analysis data
Fines correction method: Points to test:
Earthquake magnitude $\mathrm{M}_{\text {w }}$ :
Peak ground acceleration:

NCEER 1998
Robertson \& Wride
Based on Ic value
7.10
0.25

| G.W.T. (in-situ): | 6.00 ft |
| :--- | :--- |
| G.W.T. (earthq.): | 6.00 ft |
| Average results interval: | 3 |
| Ic cut-off value: | 2.60 |

Ic cut-off value: 2.60 Unit weight calculation: Based on SBT

## Location : West Hills College



Clay like behavior applied: All soil Limit depth applied: No Limit depth:

N/A


Zone $\mathrm{A}_{1}$ : Cyclic liquefaction likely depending on size and duration of cyclic loading Zone $A_{2}$ : Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening Zone C : Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

Liquefaction analysis overall plots



Input parameters and analysis data

| Analysis method: | NCEER 1998 |
| :--- | :--- |
| Fines correction method: | Robertson \& Wride |
| Points to test: | Based on Ic value |
| Earthquake magnitude $M_{\text {w }}:$ | 7.10 |
| Peak ground acceleration: | 0.25 |
| Depth to water table (insitu): | 60 ft |

Depth to water table (erthq.): 6.00 ft
Analysis method:
Fines correction method: Points to test:

Average results interval:
Ic cut-off value:
Unit weight calculation:
Unit weight calculation: $\quad 2.60$
Use fill: $\quad$ Based on SBT
$\begin{array}{ll}\text { Use fill: } & \text { No } \\ \text { Fill height: } & \text { N/A }\end{array}$
$\begin{array}{ll}\text { Depth to water table (insitu): } & 0.25 \\ 6.00 \mathrm{ft}\end{array}$
CLiq v.1.4.1.22 - CPT Liquefaction Assessment Software - Report created on: 5/24/2011, 1:37:43 PM Project file: J:\Geotechnical\Open Projects\G1100311B - Lemoore West Hills Col\liq-analysis-all4.clq


## F.S. color scheme

Fill weight:
Transition detect N/A
$K_{\sigma}$ applied:
Clay like behavior Limit depth applied: Limit depth:

Almost certain it will liquefy

| $\square$ | Very likely to liquefy |
| :--- | :--- |
| $\square$ | Liquefaction and no liquefaction are equally likely |
| $\square$ | Unlike to liquefy |
| $\square$ | Almost certain it will not liquefy |

Lateral displacements


LPI color scheme
$\square$ Very high risk
High risk
$\square$ Low risk

## Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

| Analysis method: | NCEER 1998 |
| :--- | :--- |
| Fines correction method: | Robertson \& Wride |
| Points to test: | Based on Ic value |
| Earthquake magnitude $M_{w}:$ | 7.10 |
| Peak ground acceleration: | 0.25 |
| Dept |  |

Earthquake magnitude $\mathrm{M}_{\mathrm{w}}$ :
Peak ground acceleration:
Depth to water table (insitu): $\begin{array}{ll}0.25 \\ 6.00 \mathrm{ft}\end{array}$
$\begin{array}{ll}\text { Fill height: } & \text { No } \\ & \text { N/A }\end{array}$
Project file: J:|Geotechnical\Open Projects\G1100311B -
Project file: J:\Geotechnical\Open Projects\G1100311B - Lemoore West Hills Col \liq-analysis-all4.clq

N/A
Transition detect. applied: $\mathrm{K}_{\sigma}$ applied:
Clay like behavior applied: Limit depth applied:
Limit depth: imit depth:

SBTn Index



|  |  |  |  |
| :--- | :--- | :--- | :--- |
| Depth to water table (erthq.) | 6.00 ft | Fill weight: | N/A |
| Average results interval: | 3 | Transition detect. applied: | Yes |
| Ic cut-off value: | 2.60 | K $_{\text {a }}$ applied: | No |
| Unit weight calculation: | Based on SBT | Clay like behavior applied: | All soils |
| Use fill: | No | Limit depth applied: | No |
| Fill height: | N/A | Limit depth: | N/A |



Corrected norm. cone resistance


# TRANSITION LAYER DETECTION ALGORITHM REPORT Summary Details \& Plots 

## Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of $\mathrm{I}_{\mathrm{c}}$ values over which the transition will be defined (typically somewhere between $1.80<\mathrm{I}_{\mathrm{c}}<3.0$ ) and a rate of change of $I_{c}$. Transitions typically occur when the rate of change of $I_{c}$ is fast (i.e. delta $I_{c}$ is small).

The $\mathrm{SBT}_{\mathrm{n}}$ plot below, displays in red the detected transition layers based on the parameters listed below the graphs.


## Transition layer algorithm properties

$\mathrm{I}_{\mathrm{c}}$ minimum check value:
2.10
$\mathrm{I}_{\mathrm{c}}$ maximum check value:
2.92
$\mathrm{I}_{\mathrm{c}}$ change ratio value: 0.0250
Minimum number of points in layer: 4

## General statistics

Total points in CPT file: 305
Total points excluded: 34
Exclusion percentage: $11.15 \%$
Number of layers detected: 7
:: Liquefaction Potential Index calculation data ::

| Depth (ft) | FS | FL | $\mathrm{w}_{2}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI | Depth <br> (ft) | FS | FL | $\mathrm{W}_{\text {z }}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.16 | 2.00 | 0.00 | 9.97 | 0.16 | 0.00 | 0.33 | 2.00 | 0.00 | 9.95 | 0.16 | 0.00 |
| 0.49 | 2.00 | 0.00 | 9.92 | 0.16 | 0.00 | 0.66 | 2.00 | 0.00 | 9.90 | 0.16 | 0.00 |
| 0.82 | 2.00 | 0.00 | 9.87 | 0.16 | 0.00 | 0.98 | 2.00 | 0.00 | 9.85 | 0.16 | 0.00 |
| 1.15 | 2.00 | 0.00 | 9.82 | 0.16 | 0.00 | 1.31 | 2.00 | 0.00 | 9.80 | 0.16 | 0.00 |
| 1.48 | 2.00 | 0.00 | 9.77 | 0.16 | 0.00 | 1.64 | 2.00 | 0.00 | 9.75 | 0.16 | 0.00 |
| 1.80 | 2.00 | 0.00 | 9.72 | 0.16 | 0.00 | 1.97 | 2.00 | 0.00 | 9.70 | 0.16 | 0.00 |
| 2.13 | 2.00 | 0.00 | 9.67 | 0.16 | 0.00 | 2.30 | 2.00 | 0.00 | 9.65 | 0.16 | 0.00 |
| 2.46 | 2.00 | 0.00 | 9.62 | 0.16 | 0.00 | 2.62 | 2.00 | 0.00 | 9.60 | 0.16 | 0.00 |
| 2.79 | 2.00 | 0.00 | 9.57 | 0.16 | 0.00 | 2.95 | 2.00 | 0.00 | 9.55 | 0.16 | 0.00 |
| 3.12 | 2.00 | 0.00 | 9.52 | 0.16 | 0.00 | 3.28 | 2.00 | 0.00 | 9.50 | 0.16 | 0.00 |
| 3.44 | 2.00 | 0.00 | 9.47 | 0.16 | 0.00 | 3.61 | 2.00 | 0.00 | 9.45 | 0.16 | 0.00 |
| 3.77 | 2.00 | 0.00 | 9.42 | 0.16 | 0.00 | 3.94 | 2.00 | 0.00 | 9.40 | 0.16 | 0.00 |
| 4.10 | 2.00 | 0.00 | 9.37 | 0.16 | 0.00 | 4.27 | 2.00 | 0.00 | 9.35 | 0.16 | 0.00 |
| 4.43 | 2.00 | 0.00 | 9.32 | 0.16 | 0.00 | 4.59 | 2.00 | 0.00 | 9.30 | 0.16 | 0.00 |
| 4.76 | 2.00 | 0.00 | 9.27 | 0.16 | 0.00 | 4.92 | 2.00 | 0.00 | 9.25 | 0.16 | 0.00 |
| 5.09 | 2.00 | 0.00 | 9.22 | 0.16 | 0.00 | 5.25 | 2.00 | 0.00 | 9.20 | 0.16 | 0.00 |
| 5.41 | 2.00 | 0.00 | 9.17 | 0.16 | 0.00 | 5.58 | 2.00 | 0.00 | 9.15 | 0.16 | 0.00 |
| 5.74 | 2.00 | 0.00 | 9.12 | 0.16 | 0.00 | 5.91 | 2.00 | 0.00 | 9.10 | 0.16 | 0.00 |
| 6.07 | 1.51 | 0.00 | 9.07 | 0.16 | 0.00 | 6.23 | 1.49 | 0.00 | 9.05 | 0.16 | 0.00 |
| 6.40 | 1.50 | 0.00 | 9.02 | 0.16 | 0.00 | 6.56 | 2.00 | 0.00 | 9.00 | 0.16 | 0.00 |
| 6.73 | 2.00 | 0.00 | 8.97 | 0.16 | 0.00 | 6.89 | 2.00 | 0.00 | 8.95 | 0.16 | 0.00 |
| 7.05 | 2.00 | 0.00 | 8.92 | 0.16 | 0.00 | 7.22 | 2.00 | 0.00 | 8.90 | 0.16 | 0.00 |
| 7.38 | 2.00 | 0.00 | 8.87 | 0.16 | 0.00 | 7.55 | 2.00 | 0.00 | 8.85 | 0.16 | 0.00 |
| 7.71 | 2.00 | 0.00 | 8.82 | 0.16 | 0.00 | 7.87 | 2.00 | 0.00 | 8.80 | 0.16 | 0.00 |
| 8.04 | 2.00 | 0.00 | 8.77 | 0.16 | 0.00 | 8.20 | 2.00 | 0.00 | 8.75 | 0.16 | 0.00 |
| 8.37 | 2.00 | 0.00 | 8.72 | 0.16 | 0.00 | 8.53 | 2.00 | 0.00 | 8.70 | 0.16 | 0.00 |
| 8.69 | 2.00 | 0.00 | 8.67 | 0.16 | 0.00 | 8.86 | 2.00 | 0.00 | 8.65 | 0.16 | 0.00 |
| 9.02 | 2.00 | 0.00 | 8.62 | 0.16 | 0.00 | 9.19 | 2.00 | 0.00 | 8.60 | 0.16 | 0.00 |
| 9.35 | 2.00 | 0.00 | 8.57 | 0.16 | 0.00 | 9.51 | 0.63 | 0.37 | 8.55 | 0.16 | 0.16 |
| 9.68 | 0.61 | 0.39 | 8.52 | 0.16 | 0.16 | 9.84 | 0.64 | 0.36 | 8.50 | 0.16 | 0.15 |
| 10.01 | 0.77 | 0.23 | 8.47 | 0.16 | 0.10 | 10.17 | 1.11 | 0.00 | 8.45 | 0.16 | 0.00 |
| 10.33 | 1.73 | 0.00 | 8.42 | 0.16 | 0.00 | 10.50 | 2.00 | 0.00 | 8.40 | 0.16 | 0.00 |
| 10.66 | 2.00 | 0.00 | 8.37 | 0.16 | 0.00 | 10.83 | 2.00 | 0.00 | 8.35 | 0.16 | 0.00 |
| 10.99 | 2.00 | 0.00 | 8.32 | 0.16 | 0.00 | 11.15 | 2.00 | 0.00 | 8.30 | 0.16 | 0.00 |
| 11.32 | 2.00 | 0.00 | 8.27 | 0.16 | 0.00 | 11.48 | 2.00 | 0.00 | 8.25 | 0.16 | 0.00 |
| 11.65 | 2.00 | 0.00 | 8.22 | 0.16 | 0.00 | 11.81 | 1.98 | 0.00 | 8.20 | 0.16 | 0.00 |
| 11.98 | 1.65 | 0.00 | 8.17 | 0.16 | 0.00 | 12.14 | 1.51 | 0.00 | 8.15 | 0.16 | 0.00 |
| 12.30 | 1.81 | 0.00 | 8.12 | 0.16 | 0.00 | 12.47 | 2.00 | 0.00 | 8.10 | 0.16 | 0.00 |
| 12.63 | 2.00 | 0.00 | 8.07 | 0.16 | 0.00 | 12.80 | 2.00 | 0.00 | 8.05 | 0.16 | 0.00 |
| 12.96 | 2.00 | 0.00 | 8.02 | 0.16 | 0.00 | 13.12 | 2.00 | 0.00 | 8.00 | 0.16 | 0.00 |
| 13.29 | 2.00 | 0.00 | 7.97 | 0.16 | 0.00 | 13.45 | 2.00 | 0.00 | 7.95 | 0.16 | 0.00 |
| 13.62 | 2.00 | 0.00 | 7.92 | 0.16 | 0.00 | 13.78 | 2.00 | 0.00 | 7.90 | 0.16 | 0.00 |
| 13.94 | 2.00 | 0.00 | 7.87 | 0.16 | 0.00 | 14.11 | 1.04 | 0.00 | 7.85 | 0.16 | 0.00 |
| 14.27 | 0.97 | 0.03 | 7.82 | 0.16 | 0.01 | 14.44 | 1.16 | 0.00 | 7.80 | 0.16 | 0.00 |
| 14.60 | 1.44 | 0.00 | 7.77 | 0.16 | 0.00 | 14.76 | 1.62 | 0.00 | 7.75 | 0.16 | 0.00 |
| 14.93 | 1.56 | 0.00 | 7.72 | 0.16 | 0.00 | 15.09 | 1.35 | 0.00 | 7.70 | 0.16 | 0.00 |
| 15.26 | 1.22 | 0.00 | 7.67 | 0.16 | 0.00 | 15.42 | 1.13 | 0.00 | 7.65 | 0.16 | 0.00 |
| 15.58 | 1.03 | 0.00 | 7.62 | 0.16 | 0.00 | 15.75 | 0.92 | 0.08 | 7.60 | 0.16 | 0.03 |


| :: Liquefaction Potential Index calculation data :: (continued) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth <br> (ft) | FS | FL | $\mathrm{W}_{2}$ | $\mathrm{d}_{2}$ | LPI | Depth <br> (ft) | FS | FL | $\mathrm{W}_{\mathrm{z}}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| 15.91 | 0.83 | 0.17 | 7.57 | 0.16 | 0.07 | 16.08 | 0.77 | 0.23 | 7.55 | 0.16 | 0.09 |
| 16.24 | 0.74 | 0.26 | 7.52 | 0.16 | 0.10 | 16.40 | 0.73 | 0.27 | 7.50 | 0.16 | 0.10 |
| 16.57 | 0.71 | 0.29 | 7.47 | 0.16 | 0.11 | 16.73 | 0.69 | 0.31 | 7.45 | 0.16 | 0.11 |
| 16.90 | 0.68 | 0.32 | 7.42 | 0.16 | 0.12 | 17.06 | 0.71 | 0.29 | 7.40 | 0.16 | 0.11 |
| 17.22 | 0.78 | 0.22 | 7.37 | 0.16 | 0.08 | 17.39 | 2.00 | 0.00 | 7.35 | 0.16 | 0.00 |
| 17.55 | 2.00 | 0.00 | 7.32 | 0.16 | 0.00 | 17.72 | 2.00 | 0.00 | 7.30 | 0.16 | 0.00 |
| 17.88 | 2.00 | 0.00 | 7.27 | 0.16 | 0.00 | 18.04 | 2.00 | 0.00 | 7.25 | 0.16 | 0.00 |
| 18.21 | 2.00 | 0.00 | 7.22 | 0.16 | 0.00 | 18.37 | 2.00 | 0.00 | 7.20 | 0.16 | 0.00 |
| 18.54 | 1.84 | 0.00 | 7.17 | 0.16 | 0.00 | 18.70 | 1.50 | 0.00 | 7.15 | 0.16 | 0.00 |
| 18.86 | 1.48 | 0.00 | 7.12 | 0.16 | 0.00 | 19.03 | 1.55 | 0.00 | 7.10 | 0.16 | 0.00 |
| 19.19 | 1.49 | 0.00 | 7.07 | 0.16 | 0.00 | 19.36 | 1.40 | 0.00 | 7.05 | 0.16 | 0.00 |
| 19.52 | 1.35 | 0.00 | 7.02 | 0.16 | 0.00 | 19.69 | 1.38 | 0.00 | 7.00 | 0.16 | 0.00 |
| 19.85 | 1.39 | 0.00 | 6.97 | 0.16 | 0.00 | 20.01 | 1.33 | 0.00 | 6.95 | 0.16 | 0.00 |
| 20.18 | 1.23 | 0.00 | 6.92 | 0.16 | 0.00 | 20.34 | 1.12 | 0.00 | 6.90 | 0.16 | 0.00 |
| 20.51 | 1.07 | 0.00 | 6.87 | 0.16 | 0.00 | 20.67 | 1.09 | 0.00 | 6.85 | 0.16 | 0.00 |
| 20.83 | 1.15 | 0.00 | 6.82 | 0.16 | 0.00 | 21.00 | 1.17 | 0.00 | 6.80 | 0.16 | 0.00 |
| 21.16 | 1.11 | 0.00 | 6.77 | 0.16 | 0.00 | 21.33 | 1.07 | 0.00 | 6.75 | 0.16 | 0.00 |
| 21.49 | 1.07 | 0.00 | 6.72 | 0.16 | 0.00 | 21.65 | 1.14 | 0.00 | 6.70 | 0.16 | 0.00 |
| 21.82 | 1.23 | 0.00 | 6.67 | 0.16 | 0.00 | 21.98 | 1.29 | 0.00 | 6.65 | 0.16 | 0.00 |
| 22.15 | 1.35 | 0.00 | 6.62 | 0.16 | 0.00 | 22.31 | 1.40 | 0.00 | 6.60 | 0.16 | 0.00 |
| 22.47 | 1.49 | 0.00 | 6.57 | 0.16 | 0.00 | 22.64 | 1.56 | 0.00 | 6.55 | 0.16 | 0.00 |
| 22.80 | 1.56 | 0.00 | 6.52 | 0.16 | 0.00 | 22.97 | 1.51 | 0.00 | 6.50 | 0.16 | 0.00 |
| 23.13 | 1.47 | 0.00 | 6.47 | 0.16 | 0.00 | 23.29 | 1.44 | 0.00 | 6.45 | 0.16 | 0.00 |
| 23.46 | 1.36 | 0.00 | 6.42 | 0.16 | 0.00 | 23.62 | 1.22 | 0.00 | 6.40 | 0.16 | 0.00 |
| 23.79 | 1.10 | 0.00 | 6.37 | 0.16 | 0.00 | 23.95 | 1.02 | 0.00 | 6.35 | 0.16 | 0.00 |
| 24.11 | 0.94 | 0.06 | 6.32 | 0.16 | 0.02 | 24.28 | 0.92 | 0.08 | 6.30 | 0.16 | 0.02 |
| 24.44 | 0.93 | 0.07 | 6.27 | 0.16 | 0.02 | 24.61 | 1.08 | 0.00 | 6.25 | 0.16 | 0.00 |
| 24.77 | 1.24 | 0.00 | 6.22 | 0.16 | 0.00 | 24.93 | 1.37 | 0.00 | 6.20 | 0.16 | 0.00 |
| 25.10 | 1.49 | 0.00 | 6.17 | 0.16 | 0.00 | 25.26 | 1.65 | 0.00 | 6.15 | 0.16 | 0.00 |
| 25.43 | 1.79 | 0.00 | 6.12 | 0.16 | 0.00 | 25.59 | 1.81 | 0.00 | 6.10 | 0.16 | 0.00 |
| 25.75 | 1.77 | 0.00 | 6.07 | 0.16 | 0.00 | 25.92 | 1.85 | 0.00 | 6.05 | 0.16 | 0.00 |
| 26.08 | 1.97 | 0.00 | 6.02 | 0.16 | 0.00 | 26.25 | 2.00 | 0.00 | 6.00 | 0.16 | 0.00 |
| 26.41 | 2.00 | 0.00 | 5.97 | 0.16 | 0.00 | 26.57 | 2.00 | 0.00 | 5.95 | 0.16 | 0.00 |
| 26.74 | 2.00 | 0.00 | 5.92 | 0.16 | 0.00 | 26.90 | 2.00 | 0.00 | 5.90 | 0.16 | 0.00 |
| 27.07 | 2.00 | 0.00 | 5.87 | 0.16 | 0.00 | 27.23 | 1.91 | 0.00 | 5.85 | 0.16 | 0.00 |
| 27.40 | 1.71 | 0.00 | 5.82 | 0.16 | 0.00 | 27.56 | 1.48 | 0.00 | 5.80 | 0.16 | 0.00 |
| 27.72 | 1.33 | 0.00 | 5.77 | 0.16 | 0.00 | 27.89 | 1.19 | 0.00 | 5.75 | 0.16 | 0.00 |
| 28.05 | 1.11 | 0.00 | 5.72 | 0.16 | 0.00 | 28.22 | 1.11 | 0.00 | 5.70 | 0.16 | 0.00 |
| 28.38 | 1.15 | 0.00 | 5.67 | 0.16 | 0.00 | 28.54 | 1.23 | 0.00 | 5.65 | 0.16 | 0.00 |
| 28.71 | 1.38 | 0.00 | 5.62 | 0.16 | 0.00 | 28.87 | 1.58 | 0.00 | 5.60 | 0.16 | 0.00 |
| 29.04 | 1.78 | 0.00 | 5.57 | 0.16 | 0.00 | 29.20 | 1.89 | 0.00 | 5.55 | 0.16 | 0.00 |
| 29.36 | 1.93 | 0.00 | 5.52 | 0.16 | 0.00 | 29.53 | 2.00 | 0.00 | 5.50 | 0.16 | 0.00 |
| 29.69 | 2.00 | 0.00 | 5.47 | 0.16 | 0.00 | 29.86 | 2.00 | 0.00 | 5.45 | 0.16 | 0.00 |
| 30.02 | 2.00 | 0.00 | 5.42 | 0.16 | 0.00 | 30.18 | 2.00 | 0.00 | 5.40 | 0.16 | 0.00 |
| 30.35 | 2.00 | 0.00 | 5.37 | 0.16 | 0.00 | 30.51 | 2.00 | 0.00 | 5.35 | 0.16 | 0.00 |
| 30.68 | 2.00 | 0.00 | 5.32 | 0.16 | 0.00 | 30.84 | 2.00 | 0.00 | 5.30 | 0.16 | 0.00 |
| 31.00 | 2.00 | 0.00 | 5.27 | 0.16 | 0.00 | 31.17 | 2.00 | 0.00 | 5.25 | 0.16 | 0.00 |
| 31.33 | 2.00 | 0.00 | 5.22 | 0.16 | 0.00 | 31.50 | 2.00 | 0.00 | 5.20 | 0.16 | 0.00 |

:: Liquefaction Potential Index calculation data :: (continued)

| Depth <br> (ft) | FS | FL | $\mathrm{W}_{\mathrm{z}}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI | Depth (ft) | FS | FL | $\mathrm{w}_{\text {z }}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 31.66 | 2.00 | 0.00 | 5.17 | 0.16 | 0.00 | 31.82 | 1.48 | 0.00 | 5.15 | 0.16 | 0.00 |
| 31.99 | 2.00 | 0.00 | 5.12 | 0.16 | 0.00 | 32.15 | 2.00 | 0.00 | 5.10 | 0.16 | 0.00 |
| 32.32 | 2.00 | 0.00 | 5.07 | 0.16 | 0.00 | 32.48 | 2.00 | 0.00 | 5.05 | 0.16 | 0.00 |
| 32.64 | 2.00 | 0.00 | 5.02 | 0.16 | 0.00 | 32.81 | 2.00 | 0.00 | 5.00 | 0.16 | 0.00 |
| 32.97 | 2.00 | 0.00 | 4.97 | 0.16 | 0.00 | 33.14 | 2.00 | 0.00 | 4.95 | 0.16 | 0.00 |
| 33.30 | 2.00 | 0.00 | 4.92 | 0.16 | 0.00 | 33.46 | 2.00 | 0.00 | 4.90 | 0.16 | 0.00 |
| 33.63 | 2.00 | 0.00 | 4.87 | 0.16 | 0.00 | 33.79 | 2.00 | 0.00 | 4.85 | 0.16 | 0.00 |
| 33.96 | 0.65 | 0.35 | 4.82 | 0.16 | 0.08 | 34.12 | 0.81 | 0.19 | 4.80 | 0.16 | 0.05 |
| 34.28 | 2.00 | 0.00 | 4.77 | 0.16 | 0.00 | 34.45 | 2.00 | 0.00 | 4.75 | 0.16 | 0.00 |
| 34.61 | 2.00 | 0.00 | 4.72 | 0.16 | 0.00 | 34.78 | 2.00 | 0.00 | 4.70 | 0.16 | 0.00 |
| 34.94 | 2.00 | 0.00 | 4.67 | 0.16 | 0.00 | 35.10 | 2.00 | 0.00 | 4.65 | 0.16 | 0.00 |
| 35.27 | 2.00 | 0.00 | 4.62 | 0.16 | 0.00 | 35.43 | 1.22 | 0.00 | 4.60 | 0.16 | 0.00 |
| 35.60 | 0.90 | 0.10 | 4.57 | 0.16 | 0.02 | 35.76 | 2.00 | 0.00 | 4.55 | 0.16 | 0.00 |
| 35.93 | 2.00 | 0.00 | 4.52 | 0.16 | 0.00 | 36.09 | 2.00 | 0.00 | 4.50 | 0.16 | 0.00 |
| 36.25 | 2.00 | 0.00 | 4.47 | 0.16 | 0.00 | 36.42 | 2.00 | 0.00 | 4.45 | 0.16 | 0.00 |
| 36.58 | 2.00 | 0.00 | 4.42 | 0.16 | 0.00 | 36.75 | 2.00 | 0.00 | 4.40 | 0.16 | 0.00 |
| 36.91 | 2.00 | 0.00 | 4.37 | 0.16 | 0.00 | 37.07 | 2.00 | 0.00 | 4.35 | 0.16 | 0.00 |
| 37.24 | 2.00 | 0.00 | 4.32 | 0.16 | 0.00 | 37.40 | 2.00 | 0.00 | 4.30 | 0.16 | 0.00 |
| 37.57 | 2.00 | 0.00 | 4.27 | 0.16 | 0.00 | 37.73 | 2.00 | 0.00 | 4.25 | 0.16 | 0.00 |
| 37.89 | 2.00 | 0.00 | 4.22 | 0.16 | 0.00 | 38.06 | 2.00 | 0.00 | 4.20 | 0.16 | 0.00 |
| 38.22 | 2.00 | 0.00 | 4.17 | 0.16 | 0.00 | 38.39 | 2.00 | 0.00 | 4.15 | 0.16 | 0.00 |
| 38.55 | 2.00 | 0.00 | 4.12 | 0.16 | 0.00 | 38.71 | 2.00 | 0.00 | 4.10 | 0.16 | 0.00 |
| 38.88 | 0.68 | 0.32 | 4.07 | 0.16 | 0.07 | 39.04 | 0.65 | 0.35 | 4.05 | 0.16 | 0.07 |
| 39.21 | 2.00 | 0.00 | 4.02 | 0.16 | 0.00 | 39.37 | 2.00 | 0.00 | 4.00 | 0.16 | 0.00 |
| 39.53 | 2.00 | 0.00 | 3.97 | 0.16 | 0.00 | 39.70 | 2.00 | 0.00 | 3.95 | 0.16 | 0.00 |
| 39.86 | 2.00 | 0.00 | 3.92 | 0.16 | 0.00 | 40.03 | 2.00 | 0.00 | 3.90 | 0.16 | 0.00 |
| 40.19 | 2.00 | 0.00 | 3.87 | 0.16 | 0.00 | 40.35 | 2.00 | 0.00 | 3.85 | 0.16 | 0.00 |
| 40.52 | 2.00 | 0.00 | 3.82 | 0.16 | 0.00 | 40.68 | 2.00 | 0.00 | 3.80 | 0.16 | 0.00 |
| 40.85 | 1.98 | 0.00 | 3.77 | 0.16 | 0.00 | 41.01 | 1.69 | 0.00 | 3.75 | 0.16 | 0.00 |
| 41.17 | 1.58 | 0.00 | 3.72 | 0.16 | 0.00 | 41.34 | 1.52 | 0.00 | 3.70 | 0.16 | 0.00 |
| 41.50 | 1.51 | 0.00 | 3.67 | 0.16 | 0.00 | 41.67 | 1.51 | 0.00 | 3.65 | 0.16 | 0.00 |
| 41.83 | 1.53 | 0.00 | 3.62 | 0.16 | 0.00 | 41.99 | 1.53 | 0.00 | 3.60 | 0.16 | 0.00 |
| 42.16 | 1.47 | 0.00 | 3.57 | 0.16 | 0.00 | 42.32 | 1.47 | 0.00 | 3.55 | 0.16 | 0.00 |
| 42.49 | 1.49 | 0.00 | 3.52 | 0.16 | 0.00 | 42.65 | 1.55 | 0.00 | 3.50 | 0.16 | 0.00 |
| 42.81 | 1.53 | 0.00 | 3.47 | 0.16 | 0.00 | 42.98 | 1.53 | 0.00 | 3.45 | 0.16 | 0.00 |
| 43.14 | 1.53 | 0.00 | 3.42 | 0.16 | 0.00 | 43.31 | 1.70 | 0.00 | 3.40 | 0.16 | 0.00 |
| 43.47 | 1.97 | 0.00 | 3.37 | 0.16 | 0.00 | 43.64 | 2.00 | 0.00 | 3.35 | 0.16 | 0.00 |
| 43.80 | 2.00 | 0.00 | 3.32 | 0.16 | 0.00 | 43.96 | 2.00 | 0.00 | 3.30 | 0.16 | 0.00 |
| 44.13 | 2.00 | 0.00 | 3.27 | 0.16 | 0.00 | 44.29 | 2.00 | 0.00 | 3.25 | 0.16 | 0.00 |
| 44.46 | 2.00 | 0.00 | 3.22 | 0.16 | 0.00 | 44.62 | 2.00 | 0.00 | 3.20 | 0.16 | 0.00 |
| 44.78 | 2.00 | 0.00 | 3.17 | 0.16 | 0.00 | 44.95 | 2.00 | 0.00 | 3.15 | 0.16 | 0.00 |
| 45.11 | 2.00 | 0.00 | 3.12 | 0.16 | 0.00 | 45.28 | 2.00 | 0.00 | 3.10 | 0.16 | 0.00 |
| 45.44 | 2.00 | 0.00 | 3.07 | 0.16 | 0.00 | 45.60 | 2.00 | 0.00 | 3.05 | 0.16 | 0.00 |
| 45.77 | 2.00 | 0.00 | 3.02 | 0.16 | 0.00 | 45.93 | 2.00 | 0.00 | 3.00 | 0.16 | 0.00 |
| 46.10 | 2.00 | 0.00 | 2.97 | 0.16 | 0.00 | 46.26 | 2.00 | 0.00 | 2.95 | 0.16 | 0.00 |
| 46.42 | 2.00 | 0.00 | 2.92 | 0.16 | 0.00 | 46.59 | 2.00 | 0.00 | 2.90 | 0.16 | 0.00 |
| 46.75 | 2.00 | 0.00 | 2.87 | 0.16 | 0.00 | 46.92 | 2.00 | 0.00 | 2.85 | 0.16 | 0.00 |
| 47.08 | 2.00 | 0.00 | 2.82 | 0.16 | 0.00 | 47.24 | 2.00 | 0.00 | 2.80 | 0.16 | 0.00 |


| :: Liquefaction Potential Index calculation data :: (continued) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth (ft) | FS | FL | $\mathrm{W}_{2}$ | $\mathrm{d}_{2}$ | LPI | Depth <br> (ft) | FS | FL | $\mathrm{w}_{z}$ | $\mathrm{d}_{\mathrm{z}}$ | LPI |
| 47.41 | 2.00 | 0.00 | 2.77 | 0.16 | 0.00 | 47.57 | 2.00 | 0.00 | 2.75 | 0.16 | 0.00 |
| 47.74 | 2.00 | 0.00 | 2.72 | 0.16 | 0.00 | 47.90 | 2.00 | 0.00 | 2.70 | 0.16 | 0.00 |
| 48.06 | 2.00 | 0.00 | 2.67 | 0.16 | 0.00 | 48.23 | 2.00 | 0.00 | 2.65 | 0.16 | 0.00 |
| 48.39 | 2.00 | 0.00 | 2.62 | 0.16 | 0.00 | 48.56 | 2.00 | 0.00 | 2.60 | 0.16 | 0.00 |
| 48.72 | 2.00 | 0.00 | 2.57 | 0.16 | 0.00 | 48.88 | 2.00 | 0.00 | 2.55 | 0.16 | 0.00 |
| 49.05 | 2.00 | 0.00 | 2.52 | 0.16 | 0.00 | 49.21 | 2.00 | 0.00 | 2.50 | 0.16 | 0.00 |
| 49.38 | 2.00 | 0.00 | 2.47 | 0.16 | 0.00 | 49.54 | 2.00 | 0.00 | 2.45 | 0.16 | 0.00 |
| 49.70 | 2.00 | 0.00 | 2.42 | 0.16 | 0.00 | 49.87 | 2.00 | 0.00 | 2.40 | 0.16 | 0.00 |
| 50.03 | 0.29 | 0.71 | 2.37 | 0.16 | 0.08 |  |  |  |  |  |  |

LPI $=0.00$ - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low LPI between 5.00 and 15.00 - Liquefaction risk high LPI > 15.00 - Liquefaction risk very high

## Abbreviations

FS: Calculated factor of safety for test point
FL: 1 - FS
$\mathrm{w}_{z}$ : Function value of the extend of soil liquefaction according to depth
$\mathrm{d}_{\mathrm{z}}$ : $\quad$ Layer thickness (ft)
LPI: Liquefaction potential index value for test point

## :: Post-earthquake settlement of dry sands ::

| Depth <br> (ft) | Ic | Kc | Qc1n | Qc1n,cs | $\begin{aligned} & \mathrm{N} 1,60 \\ & \text { (blows) } \end{aligned}$ | Vs (ft/s) | Gmax (tsf) | CSR | Shear, Y (\%) | Svol,15 <br> (\%) | Nc | ev <br> (\%) | Settle. <br> (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.16 | 1.80 | 1.00 | 69.02 | 69.02 | 13 | 151.8 | 31 | 0.14 | 0.026 | 0.04 | 11.65 | 0.04 | 0.001 |
| 0.33 | 1.92 | 1.21 | 74.60 | 89.90 | 18 | 193.0 | 54 | 0.14 | 0.014 | 0.02 | 11.65 | 0.01 | 0.001 |
| 0.49 | 1.82 | 1.00 | 78.01 | 78.01 | 15 | 224.0 | 74 | 0.14 | 0.012 | 0.02 | 11.65 | 0.01 | 0.001 |
| 0.66 | 1.68 | 1.00 | 95.57 | 95.57 | 18 | 267.2 | 108 | 0.14 | 0.007 | 0.01 | 11.65 | 0.01 | 0.000 |
| 0.82 | 1.59 | 1.00 | 112.07 | 112.07 | 20 | 311.2 | 151 | 0.14 | 0.005 | 0.01 | 11.65 | 0.00 | 0.000 |
| 0.98 | 1.55 | 1.00 | 118.78 | 118.78 | 21 | 333.3 | 175 | 0.14 | 0.005 | 0.01 | 11.65 | 0.00 | 0.000 |
| 1.15 | 1.54 | 1.00 | 114.03 | 114.03 | 20 | 337.7 | 179 | 0.14 | 0.006 | 0.01 | 11.65 | 0.01 | 0.000 |
| 1.31 | 1.55 | 1.00 | 107.07 | 107.07 | 19 | 337.0 | 177 | 0.14 | 0.008 | 0.01 | 11.65 | 0.01 | 0.000 |
| 1.48 | 1.54 | 1.00 | 106.77 | 106.77 | 19 | 342.5 | 183 | 0.14 | 0.009 | 0.01 | 11.65 | 0.01 | 0.000 |
| 1.64 | 1.61 | 1.00 | 110.74 | 110.74 | 20 | 361.5 | 211 | 0.14 | 0.008 | 0.01 | 11.65 | 0.01 | 0.000 |
| 1.80 | 1.78 | 1.09 | 115.96 | 126.31 | 24 | 391.5 | 260 | 0.14 | 0.006 | 0.01 | 11.65 | 0.00 | 0.000 |
| 1.97 | 1.98 | 1.27 | 118.57 | 150.83 | 31 | 418.9 | 309 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.13 | 2.12 | 1.49 | 117.14 | 174.84 | 38 | 440.9 | 349 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.30 | 2.17 | 1.60 | 118.49 | 189.92 | 42 | 461.3 | 387 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.46 | 2.18 | 1.61 | 124.52 | 200.92 | 45 | 486.3 | 435 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.62 | 2.20 | 1.66 | 127.53 | 212.31 | 48 | 507.4 | 478 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.79 | 2.25 | 1.79 | 124.02 | 221.73 | 51 | 518.6 | 503 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 2.95 | 2.30 | 1.95 | 113.78 | 221.50 | 52 | 515.5 | 496 | 0.14 | 0.005 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.12 | 2.33 | 2.03 | 105.61 | 214.60 | 51 | 511.4 | 487 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.28 | 2.33 | 2.04 | 100.18 | 204.32 | 49 | 508.9 | 481 | 0.14 | 0.006 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.44 | 2.31 | 1.99 | 96.73 | 192.66 | 46 | 507.8 | 477 | 0.14 | 0.007 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.61 | 2.31 | 1.98 | 94.63 | 187.59 | 44 | 512.1 | 485 | 0.14 | 0.007 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.77 | 2.33 | 2.05 | 89.04 | 182.50 | 44 | 508.7 | 477 | 0.14 | 0.007 | 0.00 | 11.65 | 0.00 | 0.000 |
| 3.94 | 2.38 | 2.25 | 81.17 | 182.67 | 45 | 502.8 | 465 | 0.14 | 0.008 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.10 | 2.44 | 2.47 | 70.47 | 174.30 | 44 | 484.8 | 429 | 0.14 | 0.009 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.27 | 2.48 | 2.67 | 63.48 | 169.61 | 43 | 474.5 | 408 | 0.14 | 0.010 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.43 | 2.50 | 2.79 | 59.70 | 166.68 | 43 | 471.4 | 402 | 0.14 | 0.011 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.59 | 2.53 | 2.92 | 56.42 | 165.02 | 43 | 469.6 | 398 | 0.14 | 0.012 | 0.00 | 11.65 | 0.00 | 0.000 |
| 4.76 | 2.56 | 3.07 | 51.98 | 159.53 | 42 | 461.9 | 383 | 0.14 | 0.013 | 0.01 | 11.65 | 0.00 | 0.000 |
| 4.92 | 2.55 | 3.01 | 49.15 | 148.08 | 39 | 453.9 | 368 | 0.14 | 0.015 | 0.01 | 11.65 | 0.01 | 0.000 |
| 5.09 | 2.46 | 2.56 | 53.72 | 137.43 | 35 | 465.0 | 386 | 0.14 | 0.014 | 0.01 | 11.65 | 0.01 | 0.000 |
| 5.25 | 2.38 | 2.24 | 59.76 | 133.70 | 33 | 482.6 | 418 | 0.14 | 0.013 | 0.01 | 11.65 | 0.01 | 0.000 |
| 5.41 | 2.36 | 2.15 | 61.15 | 131.78 | 32 | 489.9 | 432 | 0.14 | 0.013 | 0.01 | 11.65 | 0.01 | 0.000 |
| 5.58 | 2.40 | 2.30 | 55.63 | 127.68 | 31 | 479.5 | 411 | 0.14 | 0.014 | 0.01 | 11.65 | 0.01 | 0.000 |
| 5.74 | 2.43 | 2.43 | 49.67 | 120.66 | 30 | 464.2 | 382 | 0.14 | 0.017 | 0.01 | 11.65 | 0.01 | 0.000 |
| 5.91 | 2.43 | 2.44 | 46.90 | 114.67 | 29 | 456.7 | 367 | 0.14 | 0.019 | 0.01 | 11.65 | 0.01 | 0.000 |

Total estimated settlement: 0.01
:: Post-earthquake settlement due to soil liquefaction ::

| Depth <br> $(\mathrm{ft})$ | $\mathrm{Q}_{\mathrm{tn}, \mathrm{cs}}$ | FS | $\mathrm{e}_{\mathrm{v}}(\%)$ | Settlement <br> $(\mathrm{in})$ |  | Depth <br> $(\mathrm{ft})$ | $\mathrm{Q}_{\mathrm{tn}, \mathrm{cs}}$ | FS | $\mathrm{e}_{\mathrm{v}}(\%)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## :: Post-earthquake settlement due to soil liquefaction :: (continued)

| Depth (ft) | $Q_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement <br> (in) | Depth <br> (ft) | $Q_{\text {tn,cs }}$ | FS | $e_{\mathrm{V}}(\%)$ | Settlement <br> (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8.04 | 134.69 | 2.00 | 0.00 | 0.00 | 8.20 | 129.67 | 2.00 | 0.00 | 0.00 |
| 8.37 | 124.89 | 2.00 | 0.00 | 0.00 | 8.53 | 119.08 | 2.00 | 0.00 | 0.00 |
| 8.69 | 243.21 | 2.00 | 0.00 | 0.00 | 8.86 | 108.68 | 2.00 | 0.00 | 0.00 |
| 9.02 | 93.90 | 2.00 | 0.00 | 0.00 | 9.19 | 84.28 | 2.00 | 0.00 | 0.00 |
| 9.35 | 74.02 | 2.00 | 0.00 | 0.00 | 9.51 | 67.87 | 0.63 | 3.21 | 0.06 |
| 9.68 | 66.93 | 0.61 | 3.25 | 0.06 | 9.84 | 70.94 | 0.64 | 3.10 | 0.06 |
| 10.01 | 84.72 | 0.77 | 2.59 | 0.05 | 10.17 | 108.45 | 1.11 | 0.52 | 0.01 |
| 10.33 | 135.79 | 1.73 | 0.00 | 0.00 | 10.50 | 158.33 | 2.00 | 0.00 | 0.00 |
| 10.66 | 174.43 | 2.00 | 0.00 | 0.00 | 10.83 | 178.22 | 2.00 | 0.00 | 0.00 |
| 10.99 | 171.25 | 2.00 | 0.00 | 0.00 | 11.15 | 169.77 | 2.00 | 0.00 | 0.00 |
| 11.32 | 161.52 | 2.00 | 0.00 | 0.00 | 11.48 | 156.23 | 2.00 | 0.00 | 0.00 |
| 11.65 | 151.53 | 2.00 | 0.00 | 0.00 | 11.81 | 146.91 | 1.98 | 0.00 | 0.00 |
| 11.98 | 135.76 | 1.65 | 0.00 | 0.00 | 12.14 | 130.78 | 1.51 | 0.00 | 0.00 |
| 12.30 | 141.97 | 1.81 | 0.00 | 0.00 | 12.47 | 152.07 | 2.00 | 0.00 | 0.00 |
| 12.63 | 159.26 | 2.00 | 0.00 | 0.00 | 12.80 | 155.61 | 2.00 | 0.00 | 0.00 |
| 12.96 | 149.27 | 2.00 | 0.00 | 0.00 | 13.12 | 148.19 | 2.00 | 0.00 | 0.00 |
| 13.29 | 156.27 | 2.00 | 0.00 | 0.00 | 13.45 | 228.77 | 2.00 | 0.00 | 0.00 |
| 13.62 | 152.59 | 2.00 | 0.00 | 0.00 | 13.78 | 143.46 | 2.00 | 0.00 | 0.00 |
| 13.94 | 315.24 | 2.00 | 0.00 | 0.00 | 14.11 | 111.14 | 1.04 | 0.80 | 0.02 |
| 14.27 | 107.00 | 0.97 | 0.83 | 0.02 | 14.44 | 117.98 | 1.16 | 0.36 | 0.01 |
| 14.60 | 131.36 | 1.44 | 0.00 | 0.00 | 14.76 | 138.55 | 1.62 | 0.00 | 0.00 |
| 14.93 | 136.61 | 1.56 | 0.00 | 0.00 | 15.09 | 127.94 | 1.35 | 0.00 | 0.00 |
| 15.26 | 122.10 | 1.22 | 0.35 | 0.01 | 15.42 | 117.30 | 1.13 | 0.50 | 0.01 |
| 15.58 | 112.35 | 1.03 | 0.79 | 0.02 | 15.75 | 105.52 | 0.92 | 1.45 | 0.03 |
| 15.91 | 99.07 | 0.83 | 2.06 | 0.04 | 16.08 | 94.40 | 0.77 | 2.21 | 0.04 |
| 16.24 | 92.31 | 0.74 | 2.50 | 0.05 | 16.40 | 91.69 | 0.73 | 2.51 | 0.05 |
| 16.57 | 90.53 | 0.71 | 2.54 | 0.05 | 16.73 | 88.56 | 0.69 | 2.58 | 0.05 |
| 16.90 | 87.81 | 0.68 | 2.60 | 0.05 | 17.06 | 90.22 | 0.71 | 2.54 | 0.05 |
| 17.22 | 97.05 | 0.78 | 2.12 | 0.04 | 17.39 | 114.50 | 2.00 | 0.00 | 0.00 |
| 17.55 | 138.26 | 2.00 | 0.00 | 0.00 | 17.72 | 164.91 | 2.00 | 0.00 | 0.00 |
| 17.88 | 186.44 | 2.00 | 0.00 | 0.00 | 18.04 | 189.06 | 2.00 | 0.00 | 0.00 |
| 18.21 | 183.32 | 2.00 | 0.00 | 0.00 | 18.37 | 168.16 | 2.00 | 0.00 | 0.00 |
| 18.54 | 149.99 | 1.84 | 0.00 | 0.00 | 18.70 | 137.52 | 1.50 | 0.00 | 0.00 |
| 18.86 | 136.71 | 1.48 | 0.00 | 0.00 | 19.03 | 139.46 | 1.55 | 0.00 | 0.00 |
| 19.19 | 137.10 | 1.49 | 0.00 | 0.00 | 19.36 | 133.65 | 1.40 | 0.00 | 0.00 |
| 19.52 | 131.46 | 1.35 | 0.00 | 0.00 | 19.69 | 132.81 | 1.38 | 0.00 | 0.00 |
| 19.85 | 133.21 | 1.39 | 0.00 | 0.00 | 20.01 | 130.66 | 1.33 | 0.24 | 0.00 |
| 20.18 | 126.05 | 1.23 | 0.34 | 0.01 | 20.34 | 120.60 | 1.12 | 0.49 | 0.01 |
| 20.51 | 118.01 | 1.07 | 0.50 | 0.01 | 20.67 | 119.37 | 1.09 | 0.49 | 0.01 |
| 20.83 | 122.26 | 1.15 | 0.48 | 0.01 | 21.00 | 123.35 | 1.17 | 0.35 | 0.01 |
| 21.16 | 120.65 | 1.11 | 0.49 | 0.01 | 21.33 | 118.65 | 1.07 | 0.49 | 0.01 |
| 21.49 | 118.63 | 1.07 | 0.49 | 0.01 | 21.65 | 122.16 | 1.14 | 0.48 | 0.01 |
| 21.82 | 126.73 | 1.23 | 0.34 | 0.01 | 21.98 | 129.82 | 1.29 | 0.24 | 0.00 |
| 22.15 | 132.61 | 1.35 | 0.24 | 0.00 | 22.31 | 134.87 | 1.40 | 0.00 | 0.00 |
| 22.47 | 138.76 | 1.49 | 0.00 | 0.00 | 22.64 | 141.66 | 1.56 | 0.00 | 0.00 |
| 22.80 | 141.64 | 1.56 | 0.00 | 0.00 | 22.97 | 139.89 | 1.51 | 0.00 | 0.00 |
| 23.13 | 138.10 | 1.47 | 0.00 | 0.00 | 23.29 | 137.03 | 1.44 | 0.00 | 0.00 |
| 23.46 | 133.55 | 1.36 | 0.00 | 0.00 | 23.62 | 127.28 | 1.22 | 0.34 | 0.01 |

## :: Post-earthquake settlement due to soil liquefaction :: (continued)

| Depth (ft) | $Q_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}(\%)$ | Settlement <br> (in) | Depth <br> (ft) | $Q_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{v}}(\%)$ | Settlement <br> (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 23.79 | 120.77 | 1.10 | 0.49 | 0.01 | 23.95 | 116.67 | 1.02 | 0.77 | 0.02 |
| 24.11 | 111.79 | 0.94 | 1.33 | 0.03 | 24.28 | 110.38 | 0.92 | 1.35 | 0.03 |
| 24.44 | 111.21 | 0.93 | 1.34 | 0.03 | 24.61 | 119.77 | 1.08 | 0.49 | 0.01 |
| 24.77 | 128.23 | 1.24 | 0.34 | 0.01 | 24.93 | 134.60 | 1.37 | 0.00 | 0.00 |
| 25.10 | 139.57 | 1.49 | 0.00 | 0.00 | 25.26 | 145.83 | 1.65 | 0.00 | 0.00 |
| 25.43 | 151.11 | 1.79 | 0.00 | 0.00 | 25.59 | 151.88 | 1.81 | 0.00 | 0.00 |
| 25.75 | 150.48 | 1.77 | 0.00 | 0.00 | 25.92 | 153.13 | 1.85 | 0.00 | 0.00 |
| 26.08 | 157.08 | 1.97 | 0.00 | 0.00 | 26.25 | 160.19 | 2.00 | 0.00 | 0.00 |
| 26.41 | 160.87 | 2.00 | 0.00 | 0.00 | 26.57 | 161.72 | 2.00 | 0.00 | 0.00 |
| 26.74 | 162.92 | 2.00 | 0.00 | 0.00 | 26.90 | 162.71 | 2.00 | 0.00 | 0.00 |
| 27.07 | 161.67 | 2.00 | 0.00 | 0.00 | 27.23 | 155.41 | 1.91 | 0.00 | 0.00 |
| 27.40 | 148.31 | 1.71 | 0.00 | 0.00 | 27.56 | 139.59 | 1.48 | 0.00 | 0.00 |
| 27.72 | 132.89 | 1.33 | 0.24 | 0.00 | 27.89 | 126.23 | 1.19 | 0.34 | 0.01 |
| 28.05 | 122.33 | 1.11 | 0.48 | 0.01 | 28.22 | 121.87 | 1.11 | 0.48 | 0.01 |
| 28.38 | 124.50 | 1.15 | 0.35 | 0.01 | 28.54 | 128.54 | 1.23 | 0.34 | 0.01 |
| 28.71 | 135.30 | 1.38 | 0.00 | 0.00 | 28.87 | 143.47 | 1.58 | 0.00 | 0.00 |
| 29.04 | 151.04 | 1.78 | 0.00 | 0.00 | 29.20 | 154.72 | 1.89 | 0.00 | 0.00 |
| 29.36 | 156.05 | 1.93 | 0.00 | 0.00 | 29.53 | 158.50 | 2.00 | 0.00 | 0.00 |
| 29.69 | 163.07 | 2.00 | 0.00 | 0.00 | 29.86 | 168.56 | 2.00 | 0.00 | 0.00 |
| 30.02 | 175.07 | 2.00 | 0.00 | 0.00 | 30.18 | 180.46 | 2.00 | 0.00 | 0.00 |
| 30.35 | 184.55 | 2.00 | 0.00 | 0.00 | 30.51 | 191.61 | 2.00 | 0.00 | 0.00 |
| 30.68 | 207.82 | 2.00 | 0.00 | 0.00 | 30.84 | 225.39 | 2.00 | 0.00 | 0.00 |
| 31.00 | 234.96 | 2.00 | 0.00 | 0.00 | 31.17 | 231.61 | 2.00 | 0.00 | 0.00 |
| 31.33 | 216.75 | 2.00 | 0.00 | 0.00 | 31.50 | 190.45 | 2.00 | 0.00 | 0.00 |
| 31.66 | 159.52 | 2.00 | 0.00 | 0.00 | 31.82 | 139.44 | 1.48 | 0.00 | 0.00 |
| 31.99 | 253.08 | 2.00 | 0.00 | 0.00 | 32.15 | 101.45 | 2.00 | 0.00 | 0.00 |
| 32.32 | 83.73 | 2.00 | 0.00 | 0.00 | 32.48 | 74.30 | 2.00 | 0.00 | 0.00 |
| 32.64 | 71.61 | 2.00 | 0.00 | 0.00 | 32.81 | 67.19 | 2.00 | 0.00 | 0.00 |
| 32.97 | 67.44 | 2.00 | 0.00 | 0.00 | 33.14 | 67.01 | 2.00 | 0.00 | 0.00 |
| 33.30 | 65.57 | 2.00 | 0.00 | 0.00 | 33.46 | 64.92 | 2.00 | 0.00 | 0.00 |
| 33.63 | 68.08 | 2.00 | 0.00 | 0.00 | 33.79 | 78.85 | 2.00 | 0.00 | 0.00 |
| 33.96 | 88.98 | 0.65 | 2.57 | 0.05 | 34.12 | 102.61 | 0.81 | 1.96 | 0.04 |
| 34.28 | 111.78 | 2.00 | 0.00 | 0.00 | 34.45 | 114.55 | 2.00 | 0.00 | 0.00 |
| 34.61 | 203.05 | 2.00 | 0.00 | 0.00 | 34.78 | 106.36 | 2.00 | 0.00 | 0.00 |
| 34.94 | 101.38 | 2.00 | 0.00 | 0.00 | 35.10 | 95.53 | 2.00 | 0.00 | 0.00 |
| 35.27 | 88.58 | 2.00 | 0.00 | 0.00 | 35.43 | 127.24 | 1.22 | 0.34 | 0.01 |
| 35.60 | 109.12 | 0.90 | 1.38 | 0.03 | 35.76 | 200.28 | 2.00 | 0.00 | 0.00 |
| 35.93 | 93.76 | 2.00 | 0.00 | 0.00 | 36.09 | 89.18 | 2.00 | 0.00 | 0.00 |
| 36.25 | 81.67 | 2.00 | 0.00 | 0.00 | 36.42 | 76.67 | 2.00 | 0.00 | 0.00 |
| 36.58 | 74.40 | 2.00 | 0.00 | 0.00 | 36.75 | 74.08 | 2.00 | 0.00 | 0.00 |
| 36.91 | 74.67 | 2.00 | 0.00 | 0.00 | 37.07 | 75.49 | 2.00 | 0.00 | 0.00 |
| 37.24 | 77.51 | 2.00 | 0.00 | 0.00 | 37.40 | 79.68 | 2.00 | 0.00 | 0.00 |
| 37.57 | 81.91 | 2.00 | 0.00 | 0.00 | 37.73 | 85.30 | 2.00 | 0.00 | 0.00 |
| 37.89 | 93.60 | 2.00 | 0.00 | 0.00 | 38.06 | 105.32 | 2.00 | 0.00 | 0.00 |
| 38.22 | 109.03 | 2.00 | 0.00 | 0.00 | 38.39 | 102.40 | 2.00 | 0.00 | 0.00 |
| 38.55 | 92.58 | 2.00 | 0.00 | 0.00 | 38.71 | 90.19 | 2.00 | 0.00 | 0.00 |
| 38.88 | 90.26 | 0.68 | 2.54 | 0.05 | 39.04 | 87.76 | 0.65 | 2.60 | 0.05 |
| 39.21 | 81.86 | 2.00 | 0.00 | 0.00 | 39.37 | 78.40 | 2.00 | 0.00 | 0.00 |

:: Post-earthquake settlement due to soil liquefaction :: (continued)

| Depth <br> (ft) | Qtn,cs | FS | $\mathrm{e}_{\mathrm{V}}(\%)$ | Settlement <br> (in) | Depth <br> (ft) | $\mathrm{Q}_{\text {tn,cs }}$ | FS | $\mathrm{e}_{\mathrm{V}}$ (\%) | Settlement <br> (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39.53 | 81.43 | 2.00 | 0.00 | 0.00 | 39.70 | 173.81 | 2.00 | 0.00 | 0.00 |
| 39.86 | 82.01 | 2.00 | 0.00 | 0.00 | 40.03 | 76.81 | 2.00 | 0.00 | 0.00 |
| 40.19 | 75.63 | 2.00 | 0.00 | 0.00 | 40.35 | 77.44 | 2.00 | 0.00 | 0.00 |
| 40.52 | 76.57 | 2.00 | 0.00 | 0.00 | 40.68 | 73.07 | 2.00 | 0.00 | 0.00 |
| 40.85 | 67.25 | 1.98 | 0.00 | 0.00 | 41.01 | 61.73 | 1.69 | 0.02 | 0.00 |
| 41.17 | 59.01 | 1.58 | 0.03 | 0.00 | 41.34 | 57.07 | 1.52 | 0.04 | 0.00 |
| 41.50 | 56.48 | 1.51 | 0.04 | 0.00 | 41.67 | 56.66 | 1.51 | 0.05 | 0.00 |
| 41.83 | 58.16 | 1.53 | 0.04 | 0.00 | 41.99 | 60.00 | 1.53 | 0.04 | 0.00 |
| 42.16 | 60.66 | 1.47 | 0.05 | 0.00 | 42.32 | 59.67 | 1.47 | 0.05 | 0.00 |
| 42.49 | 56.31 | 1.49 | 0.05 | 0.00 | 42.65 | 53.47 | 1.55 | 0.04 | 0.00 |
| 42.81 | 52.84 | 1.53 | 0.04 | 0.00 | 42.98 | 55.20 | 1.53 | 0.04 | 0.00 |
| 43.14 | 57.42 | 1.53 | 0.04 | 0.00 | 43.31 | 60.12 | 1.70 | 0.02 | 0.00 |
| 43.47 | 63.84 | 1.97 | 0.00 | 0.00 | 43.64 | 68.26 | 2.00 | 0.00 | 0.00 |
| 43.80 | 71.44 | 2.00 | 0.00 | 0.00 | 43.96 | 73.14 | 2.00 | 0.00 | 0.00 |
| 44.13 | 76.88 | 2.00 | 0.00 | 0.00 | 44.29 | 80.46 | 2.00 | 0.00 | 0.00 |
| 44.46 | 84.17 | 2.00 | 0.00 | 0.00 | 44.62 | 83.87 | 2.00 | 0.00 | 0.00 |
| 44.78 | 84.61 | 2.00 | 0.00 | 0.00 | 44.95 | 86.16 | 2.00 | 0.00 | 0.00 |
| 45.11 | 94.22 | 2.00 | 0.00 | 0.00 | 45.28 | 101.58 | 2.00 | 0.00 | 0.00 |
| 45.44 | 103.70 | 2.00 | 0.00 | 0.00 | 45.60 | 96.70 | 2.00 | 0.00 | 0.00 |
| 45.77 | 87.64 | 2.00 | 0.00 | 0.00 | 45.93 | 81.15 | 2.00 | 0.00 | 0.00 |
| 46.10 | 76.62 | 2.00 | 0.00 | 0.00 | 46.26 | 73.22 | 2.00 | 0.00 | 0.00 |
| 46.42 | 74.06 | 2.00 | 0.00 | 0.00 | 46.59 | 79.66 | 2.00 | 0.00 | 0.00 |
| 46.75 | 86.27 | 2.00 | 0.00 | 0.00 | 46.92 | 89.08 | 2.00 | 0.00 | 0.00 |
| 47.08 | 87.92 | 2.00 | 0.00 | 0.00 | 47.24 | 85.29 | 2.00 | 0.00 | 0.00 |
| 47.41 | 84.64 | 2.00 | 0.00 | 0.00 | 47.57 | 85.36 | 2.00 | 0.00 | 0.00 |
| 47.74 | 85.62 | 2.00 | 0.00 | 0.00 | 47.90 | 83.98 | 2.00 | 0.00 | 0.00 |
| 48.06 | 81.36 | 2.00 | 0.00 | 0.00 | 48.23 | 78.69 | 2.00 | 0.00 | 0.00 |
| 48.39 | 76.56 | 2.00 | 0.00 | 0.00 | 48.56 | 76.04 | 2.00 | 0.00 | 0.00 |
| 48.72 | 76.39 | 2.00 | 0.00 | 0.00 | 48.88 | 77.20 | 2.00 | 0.00 | 0.00 |
| 49.05 | 76.96 | 2.00 | 0.00 | 0.00 | 49.21 | 77.09 | 2.00 | 0.00 | 0.00 |
| 49.38 | 78.22 | 2.00 | 0.00 | 0.00 | 49.54 | 80.90 | 2.00 | 0.00 | 0.00 |
| 49.70 | 69.56 | 2.00 | 0.00 | 0.00 | 49.87 | 53.55 | 2.00 | 0.00 | 0.00 |

## Abbreviations

| Qttn,cs: $^{\text {FS: }}$ | Equivalent clean sand normalized cone resistance |
| :--- | :--- |
| $\mathrm{e}_{\mathrm{v}}(\%):$ | Factor of safety against liquefaction |
| Settlement: | Post-liquefaction volumentric strain |
| Calculated settlement |  |

Appendix D
Traffic Study

# TRAFFIC STUDY 

# PROPOSED EXPANSION <br> LEMOORE COMMUNITY COLLEGE CAMPUS <br> LEMOORE, CALIFORNIA 

## Prepared for: <br> QK, Inc.

December 2020

Prepared by:


1800 30th Street, Suite 260
Bakersfield, California 93301


## TABLE OF CONTENTS

Page
INTRODUCTION ..... 1
FIGURE 1: VICINITY MAP ..... 2
FIGURE 2: LOCATION MAP .....  3
FIGURE 3: SITE PLAN ..... 4
PROJECT TRIP GENERATION AND DESIGN HOUR VOLUMES ..... 6
TABLE 1: PROJECT TRIP GENERATION ..... 6
PROJECT TRIP DISTRIBUTION AND ASSIGNMENT ..... 6
TABLE 2: PROJECT TRIP DISTRIBUTION ..... 6
EXISTING AND FUTURE TRAFFIC ..... 7
FIGURE 4: PROJECT PEAK HOUR TRAFFIC ..... 8
FIGURE 5: 2020 PEAK HOUR TRAFFIC ..... 9
FIGURE 6: 2020+PROJECT PEAK HOUR TRAFFIC ..... 10
FIGURE 7: 2024 PEAK HOUR TRAFFIC ..... 11
FIGURE 8: 2024+PROJECT PEAK HOUR TRAFFIC ..... 12
FIGURE 9: 2040 PEAK HOUR TRAFFIC ..... 13
FIGURE 10: 2040+PROJECT PEAK HOUR TRAFFIC ..... 14
INTERSECTION ANALYSIS ..... 15
TABLE 3a: INTERSECTION LOS, WEEKDAY PM PEAK HOUR ..... 16
TABLE 3b: INTERSECTION LOS, WEEKDAY AM PEAK HOUR ..... 17
QUEUE LENGTH ANALYSIS ..... 18
TABLE 4a: QUEUE LENGTH ANALYSIS, WEEKDAY PM PEAK HOUR ..... 18
TABLE 4b: QUEUE LENGTH ANALYSIS, WEEKDAY AM PEAK HOUR ..... 18
TRAFFIC SIGNAL WARRANT ANALYSIS ..... 19
TABLE 5a: TRAFFIC SIGNAL WARRANTS, WEEKDAY PM PEAK HOUR ..... 19
TABLE 5b: TRAFFIC SIGNAL WARRANTS, WEEKDAY AM PEAK HOUR ..... 19
ROADWAY ANALYSIS ..... 20
TABLE 6: ROADWAY LEVEL OF SERVICE ..... 20
VEHICLE MILES TRAVELED (VMT) ANALYSIS ..... 21
TABLE 7: VEHICLE MILES TRAVELED. ..... 21
MITIGATION ..... 22
TABLE 8: FUTURE INTERSECTION IMPROVEMENTS ..... 22
SUMMARY AND CONCLUSIONS ..... 23
REFERENCES ..... 25
APPENDIX ..... 26

## INTRODUCTION

The purpose of this study is to evaluate the potential traffic impacts of a proposed expansion of the Lemoore Community College campus located south of Bush Street and west of College Avenue in Lemoore, California. A vicinity map is presented in Figure 1 and a location map is presented in Figure 2.

## A. Project Description

The project is an expansion to the West Hills Community College in Lemoore, CA. The District is proposing to construct a 42,000 square foot, two-story Instructional Center (IC) on an undeveloped portion of the existing campus. The college has a current enrollment of 4,641 students and the proposed expansion is anticipated to increase the overall student population by approximately five percent, or 232 students. The IC will be used to expand education opportunities in the areas of allied health services, computer science, and graphic arts. A site plan is presented in Figure 3.



## SITE PLAN <br> FIGURE 3



## B. Roadway Descriptions

$191 / 2$ Avenue is a north-south collector that extends from Cinnamon Drive to Silverado Drive. In the vicinity of the project, it exists as a two-lane roadway and provides access to residential land uses.

Belle Haven Drive is an east-west collector that runs parallel to State Route 41 and extends south from W Hanford Armona Road. In the vicinity of the project, it exists as a two-lane roadway with curb and gutter.

Bush Street is an east-west arterial that extends from Marsh Drive to E D Street. It operates as a twolane roadway and provides access to State Route 41 as well as many commercial, educational, religious, and residential land uses.

College Avenue is a north-south arterial that extends south from Bush Street. It operates as a two-lane roadway with partial curb and gutter and provides access to West Hills College Lemoore.

State Route 41 is a north-south state highway that extends from north from State Route 46. In the vicinity of the project, it operates as a four-lane highway.

## PROJECT TRIP GENERATION AND DESIGN HOUR VOLUMES

The project trip generation and design hour volumes shown in Table 1 were estimated using the Institute of Transportation Engineers (ITE) Trip Generation Manual, 10th Edition. Rates and directional splits for ITE Land Use Code 540 (Junior/Community College: Students, Weekday, Peak Hour of Adjacent Street Traffic) were used to estimate project trip generation based on a total of 232 students. The AM and PM peak hours of adjacent street traffic were determined to be between 7:00 AM and 8:00 AM, and between 4:30 PM and 5:30 PM, based on a review of historical count data.

Table 1
Project Trip Generation

| General Information |  |  | Daily Trips |  | AM Peak Hour Trips |  |  | PM Peak Hour Trips |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ITE <br> Code | Development Type | Variable | $\begin{gathered} \text { ADT } \\ \text { RATE } \end{gathered}$ | ADT | Rate | In <br> \% Split/ <br> Trips | Out \% Split/ Trips | Rate | In <br> \% Split/ <br> Trips | Out \% Split/ Trips |
| 540 | Junior/Community College | $232$ <br> Students | eq | 1012 | eq | $\begin{gathered} \hline 81 \% \\ 92 \end{gathered}$ | $\begin{gathered} 19 \% \\ 22 \\ \hline \end{gathered}$ | eq | $\begin{gathered} \hline 56 \% \\ 51 \\ \hline \end{gathered}$ | $\begin{gathered} 44 \% \\ 40 \\ \hline \end{gathered}$ |

## PROJECT TRIP DISTRIBUTION AND ASSIGNMENT

The distribution of project peak hour trips is shown in Table 2 and represents the movement of traffic accessing the project site by direction. The project trip distribution was developed based on site location and travel patterns anticipated for the proposed land use.

Table 2
Project Trip Distribution

| Direction | Percent |
| :---: | :---: |
| North | 5 |
| East | 5 |
| South | 5 |
| West | 85 |

Project peak hour trips were assigned to the study intersections as shown in Figure 4. Project trip assignment was developed based on trip generation, trip distribution and likely travel routes for traffic accessing the project site.

## EXISTING AND FUTURE TRAFFIC

Due to the reduction in traffic due to the COVID-19 pandemic, the peak hour turning movement counts used were obtained from the Lennar Lemoore Traffic Impact Study prepared by ND Engineering, PC, in August 2019 and are attached in the appendix. Growth rates were applied to grow out the 2018 peak hour turning movement counts to reflect traffic volumes in 2020.

Average annual growth rates ranging between $1 \%$ and $6.9 \%$ were applied to counts at the study intersections in order to estimate projected 2040 peak hour volumes. For intersections showing negative or zero growth, $1 \%$ per year growth was applied to estimate future peak hour turning movements. These growth rates were developed based on a review of the regional travel demand model data from the Kings County Association of Governments (KCAG)

Existing peak hour volumes are shown in Figure 5, and existing plus project peak hour volumes are shown in Figure 6. Peak hour volumes for the year 2024 (assumed build out year), both without and with project traffic, are shown in Figures 7 and 8, respectively. The same for the year 2040 is shown in Figures 9 and 10, respectively.








## INTERSECTION ANALYSIS

A capacity analysis of the study intersections was conducted using Synchro 9 software from Trafficware. This software utilizes the capacity analysis methodology in the Transportation Research Board’s Highway Capacity Manual 2010 (HCM 2010). The analysis was performed for each of the following traffic scenarios.

- Existing (2020)
- Existing (2020) + Project
- Opening (2024)
- Opening (2024) + Project
- Future (2040)
- Future (2040) + Project

Level of service (LOS) criteria for unsignalized and signalized intersections, as defined in HCM 2010, are presented in the tables below.

## LEVEL OF SERVICE CRITERIA UNSIGNALIZED INTERSECTION

| Level of Service | Average Control Delay <br> (sec/veh) | Expected Delay to Minor <br> Street Traffic |
| :---: | :---: | :---: |
| A | $\leq 10$ | Little or no delay |
| B | $>10$ and $\leq 15$ | Short delays |
| C | $>15$ and $\leq 25$ | Average delays |
| D | $>25$ and $\leq 35$ | Long delays |
| E | $>35$ and $\leq 50$ | Very long delays |
| F | $>50$ | Extreme delays |

LEVEL OF SERVICE CRITERIA
SIGNALIZED INTERSECTIONS

| Level of Service | Average Control Delay <br> (sec/veh) | Volume-to-Capacity <br> Ratio |
| :---: | :---: | :---: |
| A | $\leq 10$ | $<0.60$ |
| B | $>10$ and $\leq 20$ | $0.61-0.70$ |
| C | $>20$ and $\leq 35$ | $0.71-0.80$ |
| D | $>35$ and $\leq 55$ | $0.81-0.90$ |
| E | $>55$ and $\leq 80$ | $0.91-1.00$ |
| F | $>80$ | $>1.00$ |

Peak hour level of service for the study intersections is presented in Tables 3a and 3b.
Table 3a
Intersection Level of Service
Weekday PM Peak Hour

| \# | Intersection | Control | 2020 | 2020+ <br> Project | 2024 | 2024+ <br> Project | 2040 | 2040+ <br> Project | $\begin{array}{\|c\|} \hline \text { 2040+ } \\ \text { Project } \\ \text { w/Mitigation }{ }^{1} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Bush St \& College Ave | $\begin{aligned} & \hline \text { NB } \\ & \text { SB } \end{aligned}$ | B | B | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \hline \mathrm{C} \\ & \mathrm{~A} \\ & \hline \end{aligned}$ |  |
| 2 |  <br> Semas Dr | $\begin{aligned} & \text { NB } \\ & \text { SB } \end{aligned}$ |  | - | $\begin{gathered} \text { C } \\ \text { F } \\ (273.5) \end{gathered}$ | $\begin{gathered} \text { C } \\ \text { F } \\ (>300) \end{gathered}$ | $\begin{gathered} \hline F \\ (96.7) \\ F \\ (>300) \\ \hline \end{gathered}$ | $\begin{gathered} \hline F \\ (144.7) \\ F \\ (>300) \\ \hline \end{gathered}$ | - |
|  |  | Signal | - | - | - | - | - | - | C |
| 3 | Bush St \& Belle Haven Dr | AWSC | B | B | B | B | C | $\begin{gathered} \mathrm{D} \\ (28.5) \\ \hline \end{gathered}$ | C |
| 4 | Bush St \& SR 41 SB Ramps | SB | B | B | B | B | C | C | C |
| 5 | Bush St \& SR 41 NB Ramps | NB | B | B | B | C | $\begin{gathered} \hline \text { D } \\ (32.5) \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ (38.8) \end{gathered}$ | C |
| 6 |  <br> S. $191 / 2$ Ave | AWSC | B | B | B | B | $\begin{gathered} \hline \mathrm{D} \\ (26.7) \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ (30.5) \end{gathered}$ | B |

[^4]Table 3b
Intersection Level of Service Weekday AM Peak Hour

| \# | Intersection | Control | 2020 | 2020+ <br> Project | 2024 | 2024+ <br> Project | 2040 | 2040+ <br> Project | 2040+ Project w/Mitigation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Bush St \& College Ave | $\begin{aligned} & \hline \text { NB } \\ & \text { SB } \end{aligned}$ | A | A | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \hline \mathrm{A} \\ & \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \end{aligned}$ |  |
| 2 |  <br> Semas Dr | $\begin{aligned} & \text { NB } \\ & \text { SB } \end{aligned}$ | - | - | $\begin{aligned} & \text { B } \\ & \text { C } \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{C} \end{aligned}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | $\begin{gathered} \hline \mathrm{C} \\ \mathrm{D} \\ (28.5) \\ \hline \end{gathered}$ | - |
|  |  | Signal | - | - | - | - | - | - | C |
| 3 | Bush St \& Belle Haven Dr | AWSC | B | B | B | C | $\begin{gathered} \hline \mathrm{E} \\ (46.5) \\ \hline \end{gathered}$ | $\begin{gathered} F \\ (51.6) \end{gathered}$ | C |
| 4 | Bush St \& SR 41 SB Ramps | SB | $\begin{gathered} \hline \mathrm{D} \\ (33.8) \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ (41.1) \end{gathered}$ | $\begin{gathered} \mathrm{F} \\ (50.2) \end{gathered}$ | $\begin{gathered} F \\ (63.9) \end{gathered}$ | $\begin{gathered} F \\ (>300) \end{gathered}$ | $\begin{gathered} F \\ (>300) \end{gathered}$ | C |
| 5 |  <br> SR 41 NB Ramps | NB | C | C | C | C | $\begin{gathered} \mathrm{F} \\ (92.2) \end{gathered}$ | $\begin{gathered} \mathrm{F} \\ (127.8) \\ \hline \end{gathered}$ | C |
| 6 |  <br> S. $191 / 2$ Ave | AWSC | C | C | C | $\begin{gathered} \mathrm{D} \\ (25.1) \end{gathered}$ | $\begin{gathered} \mathrm{F} \\ (57.9) \end{gathered}$ | $\begin{gathered} F \\ (58.6) \\ \hline \end{gathered}$ | C |

${ }^{1}$ Mitigation shown in Table 8

## QUEUE LENGTH ANALYSIS

Existing and future peak hour volumes, both with and without project traffic, were used to analyze whether traffic queues exceed storage capacities at four of the five study intersections. The queue length analysis was conducted using Synchro 9 and SimTraffic software. The analysis results shown in Tables 4a and 4b are provided for informational purposes only. All lengths are reported in feet.

Table 4a
Queue Length Analysis
Weekday PM Peak Hour

| Intersection |  <br> SR 41 SB Ramps |  |  |  <br> SR 41 NB Ramps |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | WBL | SBL | SBR | EBL | NBL | NBR |
| Storage Capacity | 250 | 1300 | 500 | 100 | 1200 | 500 |
| 2020 | 47 | 32 | 33 | 36 | 64 | 78 |
| $2020+$ Project | 46 | 30 | 39 | 36 | 61 | 70 |
| 2024 | 41 | 36 | 36 | 30 | 74 | 98 |
| $2024+$ Project | 46 | 27 | 37 | 44 | 84 | 90 |
| 2040 | 61 | 39 | 38 | 48 | 182 | 218 |
| $2040+$ Project | 60 | 28 | 44 | 43 | 198 | 246 |

Table 4b
Queue Length Analysis
Weekday AM Peak Hour

| Intersection |  <br> SR 41 SB Ramps |  |  |  <br> SR 41 NB Ramps |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | WBL | SBL | SBR | EBL | NBL | NBR |
| Storage Capacity | 250 | 1300 | 500 | 100 | 1200 | 500 |
| 2020 | 57 | 66 | 49 | 31 | 89 | 44 |
| $2020+$ Project | 92 | 58 | 41 | 41 | 88 | 44 |
| 2024 | 77 | 55 | 45 | 33 | 94 | 41 |
| $2024+$ Project | 70 | 71 | 43 | 35 | 175 | 47 |
| 2040 | 167 | 116 | 54 | 42 | 429 | 325 |
| $2040+$ Project | 118 | 105 | 53 | 55 | 411 | 456 |

## TRAFFIC SIGNAL WARRANT ANALYSIS

Peak hour signal warrants were evaluated for each of the unsignalized intersections within the study based on the 2014 California Manual on Uniform Traffic Control Devices (2014 CA MUTCD). Peak hour signal warrants assess delay to traffic on minor street approaches when entering or crossing a major street. Signal warrant analysis results are shown in Tables 5a and 5b.

Table 5a
Traffic Signal Warrants
Weekday PM Peak Hour

|  |  | 2020 |  |  | 2020+Project |  |  | 2024 |  |  | 2024+Project |  |  | 2040 |  |  | 2040+Project |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Intersection | Major <br> Street <br> Total <br> Approach <br> Vol | Minor <br> Street High Approach Vol | Warrant Met | Major Street Total Approach Vol | Minor Street High Approach Vol | Warrant Met | Major <br> Street <br> Total <br> Approach <br> Vol | Minor Street High Approach Vol | Warrant Met | Major <br> Street <br> Total <br> Approach <br> Vol | Minor Street High Approach Vol | Warrant Met | Major <br> Street <br> Total <br> Approach <br> Vol | Minor <br> Street <br> High <br> Approach <br> Vol | Warrant Met | Major <br> Street <br> Total <br> Approach <br> Vol | Minor Street High Approach Vol | Warrant <br> Met |
| 1 | College Ave at Bush St | 670 | 112 | NO | 737 | 131 | NO | 755 | 116 | NO | 822 | 135 | NO | 1171 | 139 | YES | 1238 | 158 | YES |
| 2 | Semas Dr at Bush St | - | - | - | - | - | - | 744 | 289 | YES | 830 | 289 | YES | 1297 | 289 | YES | 1383 | 289 | YES |
| 3 | Belle Haven Dr at Bush St | 556 | 71 | NO | 637 | 73 | NO | 598 | 86 | NO | 679 | 88 | NO | 810 | 189 | NO | 891 | 191 | YES |
| 4 | SR 41 SB Ramps at Bush St | 699 | 57 | NO | 772 | 61 | NO | 764 | 60 | NO | 837 | 64 | NO | 1088 | 76 | NO | 1161 | 80 | NO |
| 5 | SR 41 NB Ramps at Bush St | 679 | 352 | YES | 742 | 356 | YES | 738 | 389 | YES | 801 | 393 | YES | 1036 | 585 | YES | 1099 | 589 | YES |
| 6 | S 19 1/2 Ave at Bush St | 708 | 176 | NO | 753 | 184 | NO | 770 | 196 | NO | 815 | 204 | NO | 1075 | 298 | YES | 1120 | 306 | YES |

Table 5b
Traffic Signal Warrants
Weekday AM Peak Hour

|  |  | 2020 |  |  | 2020+Project |  |  | 2024 |  |  | 2024+Project |  |  | 2040 |  |  | 2040+Project |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Intersection | Major Street Total Approach Vol Vol | Minor <br> Street High Approach Vol | Warrant Met | Major Street Total Approach Vol | Minor <br> Street <br> High <br> Approach <br> Vol | Warrant Met | Major <br> Street <br> Total <br> Approach <br> Vol <br>  | Minor <br> Street <br> High <br> Approach <br> Vol <br>  | Warrant Met | Major <br> Street <br> Total <br> Approach <br> Vol | Minor <br> Street <br> High <br> Approach <br> Vol | Warrant Met | Major <br> Street <br> Total <br> Approach <br> Vol | Minor Street High Approach Vol | Warrant Met | Major <br> Street <br> Total <br> Approach <br> Vol | Minor <br> Street <br> High <br> Approach <br> Vol | Warrant Met |
| 1 | College Ave at Bush St | 266 | 112 | NO | 365 | 123 | NO | 291 | 116 | NO | 390 | 127 | NO | 433 | 120 | NO | 532 | 131 | NO |
| 2 | Semas Dr at Bush St | - | - | - | - | - | - | 849 | 122 | YES | 956 | 122 | YES | 1138 | 122 | YES | 1245 | 122 | YES |
| 3 | Belle Haven Dr at Bush St | 739 | 93 | NO | 837 | 97 | NO | 802 | 113 | NO | 900 | 117 | NO | 1109 | 247 | YES | 1207 | 251 | YES |
| 4 | SR 41 SB Ramps at Bush St | 1010 | 148 | YES | 1099 | 155 | YES | 1102 | 156 | YES | 1191 | 163 | YES | 1568 | 198 | YES | 1657 | 205 | YES |
| 5 | SR 41 NB Ramps at Bush St | 952 | 246 | YES | 1027 | 253 | YES | 1034 | 273 | YES | 1109 | 280 | YES | 1443 | 409 | YES | 1518 | 416 | YES |
| 6 | $\begin{array}{\|l} \hline \begin{array}{l} \text { S } 19 ~ 1 / 2 ~ A v e ~ a t ~ \\ \text { Bush St } \end{array} \\ \hline \end{array}$ | 651 | 280 | NO | 674 | 312 | YES | 731 | 304 | YES | 754 | 338 | YES | 1156 | 434 | YES | 1179 | 468 | YES |

It is important to note that a signal warrant defines the minimum condition under which signalization of an intersection might be warranted. Meeting this threshold does not suggest traffic signals are required, but rather, that other traffic factors and conditions be considered in order to determine whether signals are truly justified.

It is also noted that signal warrants do not necessarily correlate with level of service. An intersection may satisfy a signal warrant condition and operate at or above an acceptable level of service, or operate below an acceptable level of service and not meet signal warrant criteria.

## ROADWAY ANALYSIS

A capacity analysis of the study roadways was conducted using HCS software from McTrans. This software utilizes the capacity analysis methodology in the Transportation Research Board's Highway Capacity Manual. The analysis was performed for the following AM and PM traffic scenarios:

- Existing (2020)
- Existing+Project (2020)
- Opening (2024)
- Opening+Project (2024)
- Future (2040)
- Future+Project (2040)

Table 6
Roadway Level of Service

| Street | $2020$ <br> Directional LOS |  | 2024Directional LOS |  | $2040$ <br> Directional LOS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { East } \\ \text { AM/PM } \end{gathered}$ | $\begin{gathered} \text { West } \\ \text { AM/PM } \end{gathered}$ | $\begin{gathered} \text { East } \\ \text { AM/PM } \end{gathered}$ | $\begin{gathered} \text { West } \\ \text { AM/PM } \end{gathered}$ | $\begin{gathered} \text { East } \\ \text { AM/PM } \end{gathered}$ | $\begin{gathered} \text { West } \\ \text { AM/PM } \end{gathered}$ |
| Bush St: <br> College Ave to Semas Dr | A/B | C/B | B/B | B/B | C/C | C/C |
| Bush St: <br> Semas Dr to Belle Haven Dr | B/B | B/B | B/B | B/B | C/B | C/B |
| Bush St: <br> Belle Haven Dr to SR 41 SB | B/B | B/B | B/B | B/B | C/B | C/B |
| Bush St: SR 41 SB to SR 41 NB | A/A | A/A | A/A | A/A | A/A | B/A |
| Bush St: <br> SR 41 NB to N 19 1/2 Ave | A/A | A/A | A/A | A/A | A/A | B/A |


| Street | 2020+Project <br> Directional LOS |  | 2024+Project <br> Directional LOS |  | 2040+Project <br> Directional LOS |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | East <br> AM/PM | West <br> AM/PM | East <br> AM/PM | West <br> AM/PM | East <br> AM/PM | West <br> AM/PM |
|  | $\mathrm{B} / \mathrm{C}$ | $\mathrm{B} / \mathrm{B}$ | $\mathrm{B} / \mathrm{B}$ | $\mathrm{B} / \mathrm{B}$ | $\mathrm{C} / \mathrm{C}$ | C/C |
| Bush St: <br> Semas Dr to Belle Haven Dr | $\mathrm{B} / \mathrm{B}$ | $\mathrm{B} / \mathrm{B}$ | $\mathrm{B} / \mathrm{B}$ | $\mathrm{B} / \mathrm{B}$ | $\mathrm{C} / \mathrm{B}$ | $\mathrm{C} / \mathrm{B}$ |
| Bush St: <br> Belle Haven Dr to SR 41 SB | $\mathrm{B} / \mathrm{B}$ | $\mathrm{B} / \mathrm{B}$ | $\mathrm{B} / \mathrm{B}$ | $\mathrm{C} / \mathrm{B}$ | $\mathrm{C} / \mathrm{C}$ | $\mathrm{C} / \mathrm{C}$ |
| Bush St: <br> SR 41 SB to SR 41 NB <br> Bush St: <br> SR 41 NB to N 19 1/2 Ave | $\mathrm{A} / \mathrm{A}$ | $\mathrm{A} / \mathrm{A}$ | $\mathrm{A} / \mathrm{A}$ | $\mathrm{A} / \mathrm{A}$ | $\mathrm{A} / \mathrm{A}$ | $\mathrm{B} / \mathrm{A}$ |

## VEHICLE MILES TRAVELED (VMT) ANALYSIS

An evaluation of vehicle miles traveled (VMT) for project traffic was conducted based on applicable California Environmental Quality Act (CEQA) Guidelines. The analysis involved comparing an estimate of VMT attributable to the project to a baseline VMT and assessing whether project VMT would result in a significant transportation impact. Following CEQA Guidelines, only passenger vehicles were included in the analysis.

Several factors were taken into consideration when estimating project VMT, including proposed land use, project trip type and distribution, and location of other land developments. $82.8 \%$ of project traffic is anticipated to be students, $15.7 \%$ of project traffic is anticipated to be faculty and staff, and $1.5 \%$ is anticipated to be heavy truck trips. Of the staff and faculty trips, $40 \%$ were anticipated to be local trips and $60 \%$ were anticipated to be traveling from other towns such as Hanford, Visalia, and Fresno. No pass-by trips are anticipated since there are no other land developments in the vicinity of the project.

As shown in Table 7, it is anticipated that the project would result in an average VMT of 5.49 miles per person. An average regional VMT of 8.37 miles per capita for the year 2020 was obtained from the Kings County 2018 Regional Transportation Plan. This baseline average was estimated based on population and travel characteristic projections for the KCAG transportation modeling area.

Table 7
Vehicle Miles Traveled

| Trip Type | Project <br> ADT | Weighted <br> Average | Miles <br> Traveled | VMT per <br> Trip | Vehicle <br> Occupancy | VMT per <br> Person |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Staff/Faculty | 159 | 9.30 | 1,477 | 9.30 | 1 | 9.30 |
| Student | 838 | 4.0 | 3,352 | 4.0 | 1 | 4.0 |
| Heavy Trucks | 15 | 47.6 | 723 | 47.6 | 1 | 47.6 |
| Total | 1,012 | Weighted Average |  |  |  |  |

The average project VMT of 5.49 miles per person is more than $15 \%$ less than the baseline average VMT of 8.37 miles per capita. Therefore, the project does not to result in a significant transportation impact.

## MITIGATION

Intersection and roadway improvements needed by the year 2040 to maintain or improve the operational level of service of the street system in the vicinity of the project are shown in Table 8.

Table 8
Future Intersection Improvements

| $\#$ | Intersection | Total Improvements <br> Required by 2040 |
| :---: | :--- | :---: |
| 2 | Bush St \& Semas Dr | Signal |
| 3 | Bush St \& Belle Haven Dr | Signal |
| 4 | Bush St \& SR 41 SB Ramps | Signal |
| 5 | Bush St \& SR 41 NB Ramps | Signal |
| 6 | Bush St \& S. 19 1⁄2 Ave | Signal |

## SUMMARY AND CONCLUSIONS

This study evaluated the potential traffic impacts of a proposed Lemoore Community College campus expansion located south of Bush Street and west of College Avenue in Lemoore, California.

## Level of Service Analysis

Bush Street and State Route 41 Southbound Ramps operates below an acceptable level of service in the existing year prior to the addition of project traffic. All other intersections within the scope of the study are anticipated to operate at an acceptable level of service prior to and with the addition of project traffic.

In 2024, Bush Street and Semas Drive is anticipated to operate below an acceptable level of service prior to the addition of project traffic. With the addition of project traffic, Bush Street and S. $191 / 2$ Avenue is anticipated to operate below an acceptable level of service. All other intersections within the scope of the study are anticipated to operate at an acceptable level of service prior to and with the addition of project traffic.

In 2040, Bush Street and Belle Haven Drive and Bush Street and State Route 41 Northbound Ramps are anticipated to operate below an acceptable level of service prior to the addition of project traffic. The remaining intersections within the scope of study are anticipated to operate at acceptable levels of service during the peak hour.

## Roadway Capacity

All roadways within the project scope currently operate at acceptable levels of service and are expected to continue to do so with the addition of project traffic through the future year.

## Vehicle Miles Traveled Evaluation

The average vehicle miles traveled (VMT) is lower than the regional VMT, therefore there are no impacts.

## Conclusion

Based on the City of Lemoore standards for determining whether project traffic has a significant impact on intersections and roadways, the mitigation measures identified in Table 8 are anticipated to be needed in order to reduce the impacts for the listed facilities to less-than-significant levels in the year 2040.

## REFERENCES

1. Annual Traffic Census, Kings County Associatioin of Governments (KCAG)
2. Highway Capacity Manual 2010, Transportation Research Board
3. California Manual on Uniform Traffic Control Devices for Streets and Highways, 2014 Edition, California Department of Transportation (Caltrans)
4. Trip Generation Manual, 10th Edition, Institute of Transportation Engineers (ITE)

## APPENDIX

## INTERSECTION LEVEL OF SERVICE




## Intersection

Intersection Delay, s/veh 11.1
Intersection LOS
B

| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Traffic Vol, veh/h | 0 | 7 | 256 | 1 | 0 | 40 | 206 | 46 | 0 | 4 | 1 | 31 |
| Future Vol, veh/h | 0 | 7 | 256 | 1 | 0 | 40 | 206 | 46 | 0 | 4 | 1 | 31 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 8 | 278 | 1 | 0 | 43 | 224 | 50 | 0 | 4 | 1 | 34 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Opposing Approach | WB | EB | SB |
| Opposing Lanes | 2 | 1 | 3 |
| Conflicting Approach Left | SB | NB | EB |
| Conflicting Lanes Left | 3 | 2 | 1 |
| Conflicting Approach Right | NB | SB | WB |
| Conflicting Lanes Right | 2 | 3 | 2 |
| HCM Control Delay | 12.8 | 10.1 | 9.1 |

HCM LOS B B A

| Lane | NBLn1 | NBLn2 | EBLn1WBLn1WBLn2 | SBLn1 | SBLn2 SBLn3 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, $\%$ | $100 \%$ | $0 \%$ | $3 \%$ | $28 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $3 \%$ | $97 \%$ | $72 \%$ | $69 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, $\%$ | $0 \%$ | $97 \%$ | $0 \%$ | $0 \%$ | $31 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 4 | 32 | 264 | 143 | 149 | 57 | 2 | 12 |
| LT Vol | 4 | 0 | 7 | 40 | 0 | 57 | 0 | 0 |
| Through Vol | 0 | 1 | 256 | 103 | 103 | 0 | 2 | 0 |
| RT Vol | 0 | 31 | 1 | 0 | 46 | 0 | 0 | 12 |
| Lane Flow Rate | 4 | 35 | 287 | 155 | 162 | 62 | 2 | 13 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.009 | 0.057 | 0.444 | 0.246 | 0.24 | 0.12 | 0.004 | 0.021 |
| Departure Headway (Hd) | 7.11 | 5.908 | 5.672 | 5.792 | 5.434 | 6.961 | 6.453 | 5.742 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 506 | 609 | 640 | 623 | 666 | 518 | 558 | 627 |
| Service Time | 4.817 | 3.615 | 3.372 | 3.492 | 3.134 | 4.664 | 4.156 | 3.446 |
| HCM Lane V/C Ratio | 0.008 | 0.057 | 0.448 | 0.249 | 0.243 | 0.12 | 0.004 | 0.021 |
| HCM Control Delay | 9.9 | 9 | 12.8 | 10.4 | 9.8 | 10.6 | 9.2 | 8.6 |
| HCM Lane LOS | A | A | B | B | A | B | A | A |
| HCM 95th-tile Q | 0 | 0.2 | 2.3 | 1 | 0.9 | 0.4 | 0 | 0.1 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 57 | 2 | 12 |
| Future Vol, veh/h | 0 | 57 | 2 | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 62 | 2 | 13 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 10.2 |
| HCM LOS | B |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 0 | 226 | 118 | 105 | 250 | 0 | 0 | 0 | 0 | 15 | 0 | 42 |
| Future Vol, veh/h | 0 | 226 | 118 | 105 | 250 | 0 | 0 | 0 | 0 | 15 | 0 | 42 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free |  | Free | Free | ree | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  |  | - |  | None |  |  | None |
| Storage Length | - | - |  | 250 | - | - | - | - | - | 0 | - | 500 |
| Veh in Median Storage, \# | \# - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 246 | 128 | 114 | 272 | 0 | 0 | 0 | 0 | 16 | 0 | 46 |


| Major/Minor | Major1 | Major2 |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 272 | 0 | 0 | 374 | 0 | 0 | 810 | 874 | 136 |
| Stage 1 | - | - | - | - | - | - | 500 | 500 |  |
| Stage 2 | - | - | - | - | - | - | 310 | 374 |  |
| Critical Hdwy | 4.14 | - | - | 4.12 | - | - | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - | 2.218 | - | - | 3.519 | . 019 | . 319 |
| Pot Cap-1 Maneuver | 1288 | - | - | 1184 | - | - | 333 | 287 | 888 |
| Stage 1 | - | - | - | - | - | - | 575 | 542 |  |
| Stage 2 | - | - | - | - | - | - | 743 | 617 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1288 | - | - | 1184 | - | - | 301 | 0 | 888 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 301 | 0 |  |
| Stage 1 | - | - | - | - | - | - | 520 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 743 | 0 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 44 | 297 | 0 | 0 | 240 | 98 | 115 | 0 | 237 | 0 | 0 | 0 |
| Future Vol, veh/h | 44 | 297 | 0 | 0 | 240 | 98 | 115 | 0 | 237 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - | - | - | 0 | - | 300 | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 48 | 323 | 0 | 0 | 261 | 107 | 125 | 0 | 258 | 0 | 0 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 12.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS B |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 214 | 206 | 114 | 0 | 18 | 140 | 16 | 0 | 80 | 57 | 19 |
| Future Vol, veh/h | 0 | 214 | 206 | 114 | 0 | 18 | 140 | 16 | 0 | 80 | 57 | 19 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 233 | 224 | 124 | 0 | 20 | 152 | 17 | 0 | 87 | 62 | 21 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Righ |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 13 |  |  |  | 12.2 |  |  |  | 11.4 |  |  |
| HCM LOS |  | B |  |  |  | B |  |  |  | B |  |  |


| Lane | NBLn1 NBLn2 | NBLn3 | EBLn1 | EBLn2 | EBLn3WBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 16 | 42 | 118 |
| Future Vol, veh/h | 0 | 16 | 42 | 118 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 17 | 46 | 128 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |
| :--- | ---: |
| Approach | NB |
| Opposing Approach | 3 |
| Opposing Lanes | WB |
| Conflicting Approach Left | 3 |
| Conflictin Lanes Left | EB |
| Conflictin Approach Right | 3 |
| Conflicting Lanes Right | 11 |
| HCM Control Delay | B |
| HCM LOS |  |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.4 |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Traffic Vol, veh/h | 174 | 3 | 295 | 265 | 3 | 128 |
| Future Vol, veh/h | 174 | 3 | 295 | 265 | 3 | 128 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - None | - | None | - | None |  |
| Storage Length | - | 150 | 400 | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 189 | 3 | 321 | 288 | 3 | 139 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 12.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS B |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 9 | 290 | 3 | 0 | 40 | 249 | 46 | 0 | 7 | 1 | 31 |
| Future Vol, veh/h | 0 | 9 | 290 | 3 | 0 | 40 | 249 | 46 | 0 | 7 | 1 | 31 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 10 | 315 | 3 | 0 | 43 | 271 | 50 | 0 | 8 | 1 | 34 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 2 |  |  |  | 1 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 2 |  |  |  | 1 |  |  |
| Conflicting Approach Righ |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 2 |  |  |  | 3 |  |  |  | 2 |  |  |
| HCM Control Delay |  | 14.9 |  |  |  | 10.8 |  |  |  | 9.5 |  |  |

HCM LOS B B A

| Lane | NBLn1 | NBLn2 | EBLn1WBLn1WBLn2 | SBLn1 | SBLn2 SBLn3 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $3 \%$ | $24 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $3 \%$ | $96 \%$ | $76 \%$ | $73 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $97 \%$ | $1 \%$ | $0 \%$ | $27 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 7 | 32 | 302 | 165 | 171 | 57 | 2 | 14 |
| LT Vol | 7 | 0 | 9 | 40 | 0 | 57 | 0 | 0 |
| Through Vol | 0 | 1 | 290 | 125 | 125 | 0 | 2 | 0 |
| RT Vol | 0 | 31 | 3 | 0 | 46 | 0 | 0 | 14 |
| Lane Flow Rate | 8 | 35 | 328 | 179 | 185 | 62 | 2 | 15 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.016 | 0.06 | 0.53 | 0.294 | 0.288 | 0.125 | 0.004 | 0.026 |
| Departure Headway (Hd) | 7.411 | 6.205 | 5.809 | 5.916 | 5.604 | 7.255 | 6.746 | 6.033 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 483 | 577 | 620 | 608 | 641 | 494 | 530 | 593 |
| Service Time | 5.157 | 3.95 | 3.537 | 3.648 | 3.335 | 4.998 | 4.488 | 3.775 |
| HCM Lane V/C Ratio | 0.017 | 0.061 | 0.529 | 0.294 | 0.289 | 0.126 | 0.004 | 0.025 |
| HCM Control Delay | 10.3 | 9.3 | 14.9 | 11.1 | 10.6 | 11 | 9.5 | 8.9 |
| HCM Lane LOS | B | A | B | B | B | B | A | A |
| HCM 95th-tile Q | 0 | 0.2 | 3.1 | 1.2 | 1.2 | 0.4 | 0 | 0.1 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 57 | 2 | 14 |
| Future Vol, veh/h | 0 | 57 | 2 | 14 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 62 | 2 | 15 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 10.6 |
| HCM LOS | B |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 0 | 257 | 121 | 105 | 289 | 0 | 0 | 0 | 0 | 15 | 0 | 46 |
| Future Vol, veh/h | 0 | 257 | 121 | 105 | 289 | 0 | 0 | 0 | 0 | 15 | 0 | 46 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free |  | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  |  | - |  | one | - |  | None |
| Storage Length | - | - | - | 250 | - | - | - | - |  | 0 |  | 500 |
| Veh in Median Storage, \# | - | 0 | - | - | 0 |  | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 279 | 132 | 114 | 314 | 0 | 0 | 0 | 0 | 16 | 0 | 50 |


| Major/Minor | Major1 | Major2 |  |  |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 314 | 0 | 0 |  | 411 | 0 | 0 |  | 887 | 953 | 157 |
| Stage 1 | - | - | - |  | - | - | - |  | 542 | 542 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 345 | 411 |  |
| Critical Hdwy | 4.14 | - | - |  | 4.12 | - | - |  | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - |  | - | - | - |  | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - |  |  | - | - |  | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - |  | 2.218 | - | - |  | 3.519 | . 019 | 3.319 |
| Pot Cap-1 Maneuver | 1243 | - | - |  | 1148 | - | - |  | 299 | 258 | 861 |
| Stage 1 | - | - | - |  |  | - | - |  | 548 | 519 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 716 | 594 |  |
| Platoon blocked, \% |  | - | - |  |  | - | - |  |  |  |  |
| Mov Cap-1 Maneuver | 1243 | - | - |  | 1148 | - | - |  | 269 | 0 | 861 |
| Mov Cap-2 Maneuver | - | - | - |  | - | - | - |  | 269 | 0 |  |
| Stage 1 | - | - | - |  |  | - | - |  | 494 | 0 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 716 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  |  | SB |  |  |
| HCM Control Delay, s | 0 |  |  |  | 2.3 |  |  |  | 11.8 |  |  |
| HCM LOS |  |  |  |  |  |  |  |  | B |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt EBL EBT EBR WBL WBT WBPBBLnISBLn2 |  |  |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 1243 | - |  | 1148 | - | - | 269 | 861 |  |  |  |
| HCM Lane V/C Ratio | - | - |  | 0.099 | - |  | 0.061 | . 058 |  |  |  |
| HCM Control Delay (s) | 0 | - |  | 8.5 |  |  | 19.2 | 9.4 |  |  |  |
| HCM Lane LOS | A | - | - | A | - | - | C | A |  |  |  |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0.3 | - | - | 0.2 | 0.2 |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 5.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 49 | 323 | 0 | 0 | 272 | 98 | 119 | 0 | 237 | 0 | 0 | 0 |
| Future Vol, veh/h | 49 | 323 | 0 | 0 | 272 | 98 | 119 | 0 | 237 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - | - | - | 0 | - | 300 | - | - |  |
| Veh in Median Storage, \# | \# - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 53 | 351 | 0 | 0 | 296 | 107 | 129 | 0 | 258 | 0 | 0 | 0 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 12.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | B |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 220 | 222 | 118 | 0 | 18 | 159 | 16 | 0 | 85 | 57 | 19 |
| Future Vol, veh/h | 0 | 220 | 222 | 118 | 0 | 18 | 159 | 16 | 0 | 85 | 57 | 19 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 239 | 241 | 128 | 0 | 20 | 173 | 17 | 0 | 92 | 62 | 21 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Righ |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 13.6 |  |  |  | 13 |  |  |  | 11.8 |  |  |
| HCM LOS |  | B |  |  |  | B |  |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | NBLn3 | EBLn1 | EBLn2 | EBLn3WBLn1WBLn2WBLn3 | SBLn1 | SBLn2 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, $\%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Vol Right, $\%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 85 | 57 | 19 | 220 | 222 | 118 | 18 | 159 | 16 | 16 | 42 |
| LT Vol | 85 | 0 | 0 | 220 | 0 | 0 | 18 | 0 | 0 | 16 | 0 |
| Through Vol | 0 | 57 | 0 | 0 | 222 | 0 | 0 | 159 | 0 | 0 | 42 |
| RT Vol | 0 | 0 | 19 | 0 | 0 | 118 | 0 | 0 | 16 | 0 | 0 |
| Lane Flow Rate | 92 | 62 | 21 | 239 | 241 | 128 | 20 | 173 | 17 | 17 | 46 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.201 | 0.126 | 0.038 | 0.457 | 0.428 | 0.203 | 0.041 | 0.342 | 0.031 | 0.038 | 0.093 |
| Departure Headway (Hd) | 7.84 | 7.34 | 6.64 | 6.884 | 6.384 | 5.684 | 7.617 | 7.117 | 6.417 | 7.818 | 7.318 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 455 | 485 | 535 | 521 | 562 | 627 | 467 | 501 | 553 | 455 | 487 |
| Service Time | 5.634 | 5.134 | 4.434 | 4.655 | 4.155 | 3.455 | 5.408 | 4.908 | 4.208 | 5.607 | 5.107 |
| HCM Lane V/C Ratio | 0.202 | 0.128 | 0.039 | 0.459 | 0.429 | 0.204 | 0.043 | 0.345 | 0.031 | 0.037 | 0.094 |
| HCM Control Delay | 12.6 | 11.2 | 9.7 | 15.4 | 13.9 | 9.9 | 10.7 | 13.6 | 9.4 | 10.9 | 10.9 |
| HCM Lane LOS | $B$ | $B$ | A | C | B | A | B | B | A | B | B |
| HCM 95th-tile Q | 0.7 | 0.4 | 0.1 | 2.4 | 2.1 | 0.8 | 0.1 | 1.5 | 0.1 | 0.1 | 0.3 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
|  |  |  |  |  |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 16 | 42 | 126 |
| Future Vol, veh/h | 0 | 16 | 42 | 126 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 17 | 46 | 137 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |
| :--- | ---: |
| Approach | NB |
| Opposing Approach | 3 |
| Opposing Lanes | WB |
| Conflicting Approach Left | 3 |
| Conflicting Lanes Left | EB |
| Conflicting Approach Right | 3 |
| Conflicting Lanes Right | 11.4 |
| HCM Control Delay | B |
| HCM LOS |  |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 6 | 194 | 4 | 286 | 252 | 13 | 3 | 0 | 113 | 7 | 0 | 1 |
| Future Vol, veh/h | 6 | 194 | 4 | 286 | 252 | 13 | 3 | 0 | 113 | 7 | 0 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 200 | - | 150 | 400 | - | 150 | 200 | - | - | 200 | - |  |
| Veh in Median Storage, \# | - | 0 |  |  | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |  | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 7 | 211 | 4 | 311 | 274 | 14 | 3 | 0 | 123 | 8 | 0 | 1 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 51.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 18 | 297 | 15 | 43 | 276 | 95 | 37 | 8 |  | 169 | 11 | 33 |
| Future Vol, veh/h | 18 | 297 | 15 | 43 | 276 | 95 | 37 | 8 | 244 | 169 | 11 | 33 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free |  | Free | Free | Free | Free | Stop | Stop |  | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length |  | - | - | - |  |  |  | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - |  | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 20 | 323 | 16 | 47 | 300 | 103 | 40 | 9 | 265 | 184 | 12 | 36 |


| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 403 | 0 | 0 | 339 | 0 | 0 | 839 | 867 | 331 | 952 | 823 | 352 |
| Stage 1 | - | - | - | - | - | - | 370 | 370 |  | 445 | 445 |  |
| Stage 2 | - | - | - | - | - | - | 469 | 497 | - | 507 | 378 |  |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - | 3.518 | . 018 | 3.318 | 3.518 | .0183 | . 318 |
| Pot Cap-1 Maneuver | 1156 | - | - | 1220 | - | - | 285 | 291 | 711 | 239 | 309 | 692 |
| Stage 1 | - | - | - | - | - | - | 650 | 620 | - | 592 | 575 |  |
| Stage 2 | - | - | - | - | - | - | 575 | 545 | - | 548 | 615 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1156 | - | - | 1220 | - | - | 248 | 271 | 711 | ~ 138 | 287 | 692 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 248 | 271 | - | ~ 138 | 287 |  |
| Stage 1 | - | - | - | - | - | - | 636 | 607 | - | 580 | 546 |  |
| Stage 2 | - | - | - | - | - | - | 507 | 518 | - | 332 | 602 |  |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0.4 | 0.8 | 19.7 | 273.5 |
| HCM LOS |  | $C$ | $F$ |  |

Minor Lane/Major MvmNBLn1 EBL EBT EBR WBL WBT WBRSBLn1

| Capacity (veh/h) | 5541156 |  |  | - 1220 |  |  | 163 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HCM Lane V/C Ratio | 0.5670 .017 |  |  | -0.038 | - |  | 1.42 |
| HCM Control Delay (s) | 19.7 | 8.2 | 0 | 8.1 | 0 |  | 273.5 |
| HCM Lane LOS | C | A | A | A | A | - | F |
| HCM 95th \%tile Q(veh) | 3.5 | 0.1 | - | 0.1 | - |  | 14.5 |

Notes
~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | B |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 7 | 271 | 1 | 0 | 44 | 225 | 50 | 0 | 5 | 1 | 40 |
| Future Vol, veh/h | 0 | 7 | 271 | 1 | 0 | 44 | 225 | 50 | 0 | 5 | 1 | 40 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 8 | 295 | 1 | 0 | 48 | 245 | 54 | 0 | 5 | 1 | 43 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Opposing Approach | WB | EB | SB |
| Opposing Lanes | 2 | 1 | 3 |
| Conflicting Approach Left | SB | NB | EB |
| Conflicting Lanes Left | 3 | 2 | 1 |
| Conflicting Approach Right | NB | SB | WB |
| Conflicting Lanes Right | 2 | 3 | 2 |
| HCM Control Delay | 14.2 | 10.7 | 9.5 |

HCM LOS B B A

| Lane | NBLn1 | NBLn2 | EBLn1WBLn1WBLn2 | SBLn1 | SBLn2 SBLn3 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, $\%$ | $100 \%$ | $0 \%$ | $3 \%$ | $28 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $2 \%$ | $97 \%$ | $72 \%$ | $69 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, $\%$ | $0 \%$ | $98 \%$ | $0 \%$ | $0 \%$ | $31 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 5 | 41 | 279 | 157 | 163 | 69 | 2 | 15 |
| LT Vol | 5 | 0 | 7 | 44 | 0 | 69 | 0 | 0 |
| Through Vol | 0 | 1 | 271 | 113 | 113 | 0 | 2 | 0 |
| RT Vol | 0 | 40 | 1 | 0 | 50 | 0 | 0 | 15 |
| Lane Flow Rate | 5 | 45 | 303 | 170 | 177 | 75 | 2 | 16 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.011 | 0.076 | 0.493 | 0.281 | 0.275 | 0.149 | 0.004 | 0.027 |
| Departure Headway (Hd) | 7.341 | 6.131 | 5.851 | 5.955 | 5.596 | 7.166 | 6.657 | 5.945 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 488 | 584 | 616 | 604 | 643 | 501 | 538 | 602 |
| Service Time | 5.085 | 3.875 | 3.578 | 3.682 | 3.324 | 4.905 | 4.397 | 3.684 |
| HCM Lane V/C Ratio | 0.01 | 0.077 | 0.492 | 0.281 | 0.275 | 0.15 | 0.004 | 0.027 |
| HCM Control Delay | 10.2 | 9.4 | 14.2 | 11 | 10.4 | 11.2 | 9.4 | 8.8 |
| HCM Lane LOS | B | A | B | $B$ | $B$ | $B$ | A | A |
| HCM 95th-tile Q | 0 | 0.2 | 2.7 | 1.1 | 1.1 | 0.5 | 0 | 0.1 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 69 | 2 | 15 |
| Future Vol, veh/h | 0 | 69 | 2 | 15 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 75 | 2 | 16 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 10.7 |
| HCM LOS | B |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 0 | 247 | 129 | 115 | 273 | 0 | 0 | 0 | 0 | 16 | 0 | 44 |
| Future Vol, veh/h | 0 | 247 | 129 | 115 | 273 | 0 | 0 | 0 | 0 | 16 | 0 | 44 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  |  | - |  | None | - |  | None |
| Storage Length | - | - | - | 250 | - | - | - | - | - | 0 | - | 500 |
| Veh in Median Storage, \# | \# - | 0 |  | - | 0 | - | - | 0 |  | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 268 | 140 | 125 | 297 | 0 | 0 | 0 | 0 | 17 | 0 | 48 |


| Major/Minor | Major1 | Major2 |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 297 | 0 | 0 | 409 | 0 | 0 | 886 | 956 | 148 |
| Stage 1 | - | - | - | - | - | - | 547 | 547 |  |
| Stage 2 | - | - | - | - | - | - | 339 | 409 |  |
| Critical Hdwy | 4.14 | - | - | 4.12 | - | - | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - |  | - | - | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - | 2.218 | - | - | 3.519 | . 019 | 3.319 |
| Pot Cap-1 Maneuver | 1261 | - | - | 1150 | - | - | 299 | 257 | 873 |
| Stage 1 | - | - | - | - | - | - | 545 | 517 |  |
| Stage 2 | - | - | - | - | - | - | 721 | 595 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1261 | - | - | 1150 | - | - | 267 | 0 | 873 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 267 | 0 |  |
| Stage 1 | - | - | - | - | - | - | 486 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 721 | 0 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 5.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT | NBR | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 48 | 324 | 0 | 0 | 260 | 106 | 127 | 0 | 262 | 0 | 0 | 0 |
| Future Vol, veh/h | 48 | 324 | 0 | 0 | 260 | 106 | 127 | 0 | 262 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - | - | - | 0 | - | 300 | - | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 52 | 352 | 0 | 0 | 283 | 115 | 138 | 0 | 285 | 0 | 0 | 0 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 13.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | B |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 232 | 224 | 124 | 0 | 20 | 153 | 17 | 0 | 91 | 65 | 22 |
| Future Vol, veh/h | 0 | 232 | 224 | 124 | 0 | 20 | 153 | 17 | 0 | 91 | 65 | 22 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 252 | 243 | 135 | 0 | 22 | 166 | 18 | 0 | 99 | 71 | 24 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Right |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 14.3 |  |  |  | 13.2 |  |  |  | 12.1 |  |  |
| HCM LOS |  | B |  |  |  | B |  |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | NBLn3 | EBLn1 | EBLn2 | EBLn3WBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 18 | 47 | 131 |
| Future Vol, veh/h | 0 | 18 | 47 | 131 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 20 | 51 | 142 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |
| :--- | ---: |
| Approach | NB |
| Opposing Approach | 3 |
| Opposing Lanes | WB |
| Conflicting Approach Left | 3 |
| Conflictin Lanes Left | EB |
| Conflictin Approach Right | 3 |
| Conflicting Lanes Right | 11.7 |
| HCM Control Delay | B |
| HCM LOS |  |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 6 | 213 | 4 | 309 | 277 | 13 | 3 | 0 | 132 | 7 | 0 | 1 |
| Future Vol, veh/h | 6 | 213 | 4 | 309 | 277 | 13 | 3 | 0 | 132 | 7 | 0 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 200 | - | 150 | 400 | - | 150 | 200 | - | - | 200 | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - |  | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |  | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mumt Flow | 7 | 232 | 4 | 336 | 301 | 14 | 3 | 0 | 143 | 8 | 0 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 69.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT | SBR |
| Traffic Vol, veh/h | 18 | 335 | 15 | 43 | 324 | 95 | 37 | 8 | 244 | 169 | 11 | 33 |
| Future Vol, veh/h | 18 | 335 | 15 | 43 | 324 | 95 | 37 | 8 |  | 169 | 11 | 33 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | None | - |  | None |  |  | None |
| Storage Length | - | - |  | - |  | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 20 | 364 | 16 | 47 | 352 | 103 | 40 | 9 | 265 | 184 | 12 | 36 |


| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 455 | 0 | 0 | 380 | 0 | 0 | 932 | 960 | 372 | 1045 | 917 | 404 |
| Stage 1 | - | - | - | - | - | - | 411 | 411 |  | 497 | 497 |  |
| Stage 2 | - | - | - | - | - | - | 521 | 549 | - | 548 | 420 |  |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - | 3.518 | . 018 | 3.318 | 3.518 | .0183 | . 318 |
| Pot Cap-1 Maneuver | 1106 | - | - | 1178 | - | - | 247 | 257 | 674 | 207 | 272 | 647 |
| Stage 1 | - | - | - | - | - | - | 618 | 595 | - | 555 | 545 |  |
| Stage 2 | - | - | - | - | - | - | 539 | 516 | - | 521 | 589 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1106 | - | - | 1178 | - | - | 212 | 238 | 674 | ~ 115 | 251 | 647 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 212 | 238 | - | ~ 115 | 251 |  |
| Stage 1 | - | - | - | - | - | - | 604 | 581 | - | 542 | 516 |  |
| Stage 2 | - | - | - | - | - | - | 470 | 488 | - | 304 | 575 |  |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | ---: |
| HCM Control Delay, s | 0.4 | 0.8 | 23 | $\$ 402.2$ |
| HCM LOS |  | $C$ | F |  |

Minor Lane/Major MvmNBLn1 EBL EBT EBR WBL WBT WBRSBLn1

| Capacity (veh/h) | 507 | 1106 | - | -1178 |  | - | -136 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| HCM Lane V/C Ratio | 0.620 .018 | - | -0.04 | - | -1.702 |  |  |
| HCM Control Delay (s) | 23 | 8.3 | 0 | - | 8.2 | 0 | $\$ 402.2$ |
| HCM Lane LOS | C | A | A | - | A | A | - |
| HCM 95th \%tile Q(veh) | 4.2 | 0.1 | - | - | 0.1 | - | - |

Notes
~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

## Intersection

Intersection Delay, s/veh 13.3
Intersection LOS
B

| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Traffic Vol, veh/h | 0 | 9 | 305 | 3 | 0 | 44 | 268 | 50 | 0 | 8 | 1 | 40 |
| Future Vol, veh/h | 0 | 9 | 305 | 3 | 0 | 44 | 268 | 50 | 0 | 8 | 1 | 40 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 10 | 332 | 3 | 0 | 48 | 291 | 54 | 0 | 9 | 1 | 43 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Opposing Approach | WB | EB | SB |
| Opposing Lanes | 2 | 1 | 3 |
| Conflicting Approach Left | SB | NB | EB |
| Conflicting Lanes Left | 3 | 2 | 1 |
| Conflicting Approach Right | NB | SB | WB |
| Conflicting Lanes Right | 2 | 3 | 2 |
| HCM Control Delay | 16.6 | 11.5 | 9.9 |

HCM LOS C B A

| Lane | NBLn1 | NBLn2 | EBLn1WBLn1WBLn2 | SBLn1 | SBLn2 SBLn3 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $3 \%$ | $25 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $2 \%$ | $96 \%$ | $75 \%$ | $73 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $98 \%$ | $1 \%$ | $0 \%$ | $27 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 8 | 41 | 317 | 178 | 184 | 69 | 2 | 17 |
| LT Vol | 8 | 0 | 9 | 44 | 0 | 69 | 0 | 0 |
| Through Vol | 0 | 1 | 305 | 134 | 134 | 0 | 2 | 0 |
| RT Vol | 0 | 40 | 3 | 0 | 50 | 0 | 0 | 17 |
| Lane Flow Rate | 9 | 45 | 345 | 193 | 200 | 75 | 2 | 18 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.018 | 0.08 | 0.575 | 0.328 | 0.321 | 0.156 | 0.004 | 0.032 |
| Departure Headway (Hd) | 7.648 | 6.434 | 6.003 | 6.1 | 5.783 | 7.466 | 6.956 | 6.242 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 467 | 555 | 600 | 590 | 622 | 480 | 514 | 572 |
| Service Time | 5.409 | 4.195 | 3.742 | 3.84 | 3.523 | 5.221 | 4.711 | 3.997 |
| HCM Lane V/C Ratio | 0.019 | 0.081 | 0.575 | 0.327 | 0.322 | 0.156 | 0.004 | 0.031 |
| HCM Control Delay | 10.6 | 9.8 | 16.6 | 11.8 | 11.3 | 11.6 | 9.7 | 9.2 |
| HCM Lane LOS | B | A | C | B | B | B | A | A |
| HCM 95th-tile Q | 0.1 | 0.3 | 3.6 | 1.4 | 1.4 | 0.5 | 0 | 0.1 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 69 | 2 | 17 |
| Future Vol, veh/h | 0 | 69 | 2 | 17 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 75 | 2 | 18 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 11.1 |
| HCM LOS | B |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 0 | 278 | 132 | 115 | 312 | 0 | 0 | 0 | 0 | 16 | 0 | 48 |
| Future Vol, veh/h | 0 | 278 | 132 | 115 | 312 | 0 | 0 | 0 | 0 | 16 | 0 | 48 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free |  | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  |  | - |  | one | - |  | None |
| Storage Length | - | - | - | 250 | - | - | - | - |  | 0 |  | 500 |
| Veh in Median Storage, \# | - | 0 | - |  | 0 |  | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 302 | 143 | 125 | 339 | 0 | 0 | 0 | 0 | 17 | 0 | 52 |


| Major/Minor | Major1 | Major2 |  |  |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 339 | 0 | 0 |  | 446 | 0 | 0 |  | 963 | 1035 | 170 |
| Stage 1 | - | - | - |  | - | - | - |  | 589 | 589 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 374 | 446 |  |
| Critical Hdwy | 4.14 | - | - |  | 4.12 | - | - |  | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - |  | - | - | - |  | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - |  |  | - | - |  | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - |  | 2.218 | - | - |  | 3.519 | . 019 | 3.319 |
| Pot Cap-1 Maneuver | 1217 | - | - |  | 1114 | - | - |  | 268 | 231 | 845 |
| Stage 1 | - | - | - |  |  | - | - |  | 518 | 495 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 695 | 573 |  |
| Platoon blocked, \% |  | - | - |  |  | - | - |  |  |  |  |
| Mov Cap-1 Maneuver | 1217 | - | - |  | 1114 | - | - |  | 238 | 0 | 845 |
| Mov Cap-2 Maneuver | - | - | - |  | - | - | - |  | 238 | 0 |  |
| Stage 1 | - | - | - |  |  | - | - |  | 460 | 0 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 695 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  |  | SB |  |  |
| HCM Control Delay, s | 0 |  |  |  | 2.3 |  |  |  | 12.5 |  |  |
| HCM LOS |  |  |  |  |  |  |  |  | B |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt EBL EBT EBR WBL WBT WBPSBLnISBLn2 |  |  |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 1217 | - |  | 1114 | - | - | 238 | 845 |  |  |  |
| HCM Lane V/C Ratio | - | - |  | 0.112 | - |  | 0.073 | . 062 |  |  |  |
| HCM Control Delay (s) | 0 | - |  | 8.6 |  |  | 21.3 | 9.5 |  |  |  |
| HCM Lane LOS | A | - | - | A | - | - | C | A |  |  |  |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0.4 | - |  | 0.2 | 0.2 |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 5.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 53 | 350 | 0 | 0 | 292 | 106 | 131 | 0 | 262 | 0 | 0 | 0 |
| Future Vol, veh/h | 53 | 350 | 0 | 0 | 292 | 106 | 131 | 0 | 262 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - | - | - | 0 | - | 300 | - | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 58 | 380 | 0 | 0 | 317 | 115 | 142 | 0 | 285 | 0 | 0 | 0 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 14.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS B |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 238 | 240 | 128 | 0 | 20 | 172 | 17 | 0 | 96 | 65 | 22 |
| Future Vol, veh/h | 0 | 238 | 240 | 128 | 0 | 20 | 172 | 17 | 0 | 96 | 65 | 22 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 259 | 261 | 139 | 0 | 22 | 187 | 18 | 0 | 104 | 71 | 24 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Right |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 15.2 |  |  |  | 14.3 |  |  |  | 12.5 |  |  |
| HCM LOS |  | C |  |  |  | B |  |  |  | B |  |  |


| Lane | NBLn1 | NBLn2 | NBLn3 | EBLn1 | EBLn2 | EBLn3WBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 18 | 47 | 139 |
| Future Vol, veh/h | 0 | 18 | 47 | 139 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 20 | 51 | 151 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |
| :--- | ---: |
| Approach | NB |
| Opposing Approach | 3 |
| Opposing Lanes | WB |
| Conflicting Approach Left | 3 |
| Conflicting Lanes Left | EB |
| Conflicting Approach Right | 3 |
| Conflicting Lanes Right | 12.3 |
| HCM Control Delay | B |
| HCM LOS |  |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 7.2 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 15 | 480 | 9 | 349 | 308 | 10 | 4 | 2 | 133 | 18 | 2 | 4 |
| Future Vol, veh/h | 15 | 480 | 9 | 349 | 308 | 10 | 4 | 2 | 133 | 18 | 2 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free |  | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | one | - |  | None | - |  | None |
| Storage Length | 200 | - | 150 | 400 | - | 150 | 200 | - | - | 200 | - |  |
| Veh in Median Storage, \# | \# - | 0 | - | - | 0 | - | - | 0 |  | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |  | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 16 | 522 | 10 | 379 | 335 | 11 | 4 | 2 | 145 | 20 | 2 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 228.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 18 | 472 | 15 | 43 | 654 | 95 | 37 | 8 | 244 | 169 | 11 | 33 |
| Future Vol, veh/h | 18 | 472 | 15 | 43 | 654 | 95 | 37 | 8 | 244 | 169 | 11 | 33 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | one | - |  | None | - |  | None |
| Storage Length | - | - |  | - | - | - |  |  |  | - | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 |  |  | 0 |  | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 20 | 513 | 16 | 47 | 711 | 103 | 40 | 9 | 265 | 184 | 12 | 36 |


| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 814 | 0 | 0 | 529 | 0 | 0 | 1440 | 1468 | 521 | 1553 | 1424 | 763 |
| Stage 1 | - | - | - | - | - | - | 560 | 560 |  | 856 | 856 |  |
| Stage 2 | - | - | - | - | - | - | 880 | 908 | - | 697 | 568 |  |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | . 318 |
| Pot Cap-1 Maneuver | 813 | - | - | 1038 | - | - | 111 | 128 | 555 | -92 | 136 | 404 |
| Stage 1 | - | - | - | - | - | - | 513 | 511 | - | 352 | 374 |  |
| Stage 2 | - | - | - | - | - | - | 342 | 354 | - | 431 | 506 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 813 | - | - | 1038 | - | - | 85 | 113 | 555 | - 41 | 120 | 404 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 85 | 113 | - | -41 | 120 |  |
| Stage 1 | - | - | - | - | - | - | 495 | 493 | - | 340 | 343 |  |
| Stage 2 | - | - | - | - | - | - | 276 | 324 | - | 213 | 488 |  |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | ---: | ---: |
| HCM Control Delay, s | 0.3 | 0.5 | 96.7 | F 1797.9 |
| HCM LOS |  | $F$ | F |  |

Minor Lane/Major MvmNBLn1 EBL EBT EBR WBL WBT WBRSBLn1

| Capacity (veh/h) | 306 | 813 | - | -1038 |  | - | - |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| HCM Lane V/C Ratio | 1.027 | 0.024 | - | -0.045 | - | -4.63 |  |
| HCM Control Delay (s) | 96.7 | 9.5 | 0 | - | 8.6 | 0 | $\$ 1797.9$ |
| HCM Lane LOS | F | A | A | - | A | A | - |
| HCM 95th \%tile Q(veh) | 11.4 | 0.1 | - | - | 0.1 | - | - |

Notes
$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 21.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS C |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 9 | 343 | 1 | 0 | 63 | 322 | 72 | 0 | 15 | 4 | 118 |
| Future Vol, veh/h | 0 | 9 | 343 | 1 | 0 | 63 | 322 | 72 | 0 | 15 | 4 | 118 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 10 | 373 | 1 | 0 | 68 | 350 | 78 | 0 | 16 | 4 | 128 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 2 |  |  |  | 1 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 2 |  |  |  | 1 |  |  |
| Conflicting Approach Righ |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 2 |  |  |  | 3 |  |  |  | 2 |  |  |
| HCM Control Delay |  | 33.4 |  |  |  | 17.3 |  |  |  | 13.6 |  |  |

HCM LOS D C B

| Lane | NBLn1 NBLn2 EBLn1WBLn1WBLn2 SBLn1 SBLn2 SBLn3 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vol Left, \% | 100\% | 0\% | 3\% | 28\% | 0\% | 100\% | 0\% | 0\% |
| Vol Thru, \% | 0\% | 3\% | 97\% | 72\% | 69\% | 0\% | 100\% | 0\% |
| Vol Right, \% | 0\% | 97\% | 0\% | 0\% | 31\% | 0\% | 0\% | 100\% |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 15 | 122 | 353 | 224 | 233 | 152 | 5 | 32 |
| LT Vol | 15 | 0 | 9 | 63 | 0 | 152 | 0 | 0 |
| Through Vol | 0 | 4 | 343 | 161 | 161 | 0 | 5 | 0 |
| RT Vol | 0 | 118 | 1 | 0 | 72 | 0 | 0 | 32 |
| Lane Flow Rate | 16 | 133 | 384 | 243 | 253 | 165 | 5 | 35 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.041 | 0.289 | 0.794 | 0.506 | 0.501 | 0.402 | 0.012 | 0.073 |
| Departure Headway (Hd) | 9.076 | 7.849 | 7.45 | 7.485 | 7.121 | 8.76 | 8.244 | 7.521 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 393 | 456 | 483 | 480 | 504 | 410 | 433 | 474 |
| Service Time | 6.864 | 5.636 | 5.217 | 5.254 | 4.89 | 6.541 | 6.025 | 5.302 |
| HCM Lane V/C Ratio | 0.041 | 0.292 | 0.795 | 0.506 | 0.502 | 0.402 | 0.012 | 0.074 |
| HCM Control Delay | 12.3 | 13.8 | 33.4 | 17.7 | 16.9 | 17.4 | 11.1 | 10.9 |
| HCM Lane LOS | B | B | D | C | C | C | B | B |
| HCM 95th-tile Q | 0.1 | 1.2 | 7.3 | 2.8 | 2.8 | 1.9 | 0 | 0.2 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 152 | 5 | 32 |
| Future Vol, veh/h | 0 | 152 | 5 | 32 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 165 | 5 | 35 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 16.1 |
| HCM LOS | C |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 0 | 353 | 185 | 163 | 387 | 0 | 0 | 0 | 0 | 20 | 0 | 56 |
| Future Vol, veh/h | 0 | 353 | 185 | 163 | 387 | 0 | 0 | 0 | 0 | 20 | 0 | 56 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | ne | - |  | None | - |  | None |
| Storage Length | - | - | - | 250 | - | - | - | - | - | 0 | - | 500 |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 384 | 201 | 177 | 421 | 0 | 0 | 0 | 0 | 22 | 0 | 61 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 12.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 68 | 460 | 0 | 0 | 361 | 147 | 191 | 0 | 394 | 0 | 0 | 0 |
| Future Vol, veh/h | 68 | 460 | 0 | 0 | 361 | 147 | 191 | 0 | 394 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - |  | - | 0 | - | 300 | - |  |  |
| Veh in Median Storage, \# | \# - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 74 | 500 | 0 | 0 | 392 | 160 | 208 | 0 | 428 | 0 | 0 | 0 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 26.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | D |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 322 | 310 | 171 | 0 | 28 | 219 | 25 | 0 | 152 | 108 | 36 |
| Future Vol, veh/h | 0 | 322 | 310 | 171 | 0 | 28 | 219 | 25 | 0 | 152 | 108 | 36 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 350 | 337 | 186 | 0 | 30 | 238 | 27 | 0 | 165 | 117 | 39 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Righ |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 33.7 |  |  |  | 23.9 |  |  |  | 18.1 |  |  |
| HCM LOS |  | D |  |  |  | C |  |  |  | C |  |  |


| Lane | NBLn1 NBLn2 NBLn3 EBLn1 EBLn2 EBLn3WBLn1WBLn2WBLn3 SBLn1 SBLn2 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vol Left, \% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% |
| Vol Thru, \% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% |
| Vol Right, \% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 152 | 108 | 36 | 322 | 310 | 171 | 28 | 219 | 25 | 27 | 71 |
| LT Vol | 152 | 0 | 0 | 322 | 0 | 0 | 28 | 0 | 0 | 27 | 0 |
| Through Vol | 0 | 108 | 0 | 0 | 310 | 0 | 0 | 219 | 0 | 0 | 71 |
| RT Vol | 0 | 0 | 36 | 0 | 0 | 171 | 0 | 0 | 25 | 0 | 0 |
| Lane Flow Rate | 165 | 117 | 39 | 350 | 337 | 186 | 30 | 238 | 27 | 29 | 77 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.454 | 0.307 | 0.095 | 0.846 | 0.767 | 0.387 | 0.084 | 0.623 | 0.066 | 0.081 | 0.203 |
| Departure Headway (Hd) | 9.903 | 9.403 | 8.703 | 8.697 | 8.197 | 7.497 | 9.925 | 9.425 | 8.725 | 9.949 | 9.449 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 363 | 383 | 412 | 417 | 441 | 480 | 361 | 383 | 410 | 360 | 380 |
| Service Time | 7.659 | 7.159 | 6.459 | 6.445 | 5.945 | 5.245 | 7.686 | 7.186 | 6.486 | 7.707 | 7.207 |
| HCM Lane V/C Ratio | 0.455 | 0.305 | 0.095 | 0.839 | 0.764 | 0.388 | 0.083 | 0.621 | 0.066 | 0.081 | 0.203 |
| HCM Control Delay | 20.7 | 16.3 | 12.4 | 44.1 | 33.3 | 14.9 | 13.6 | 26.6 | 12.1 | 13.6 | 14.6 |
| HCM Lane LOS | C | C | B | E | D | B | B | D | B | B | B |
| HCM 95th-tile Q | 2.3 | 1.3 | 0.3 | 8.1 | 6.5 | 1.8 | 0.3 | 4 | 0.2 | 0.3 | 0.7 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 27 | 71 | 200 |
| Future Vol, veh/h | 0 | 27 | 71 | 200 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 29 | 77 | 217 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |
| :--- | ---: |
| Approach | NB |
| Opposing Approach | 3 |
| Opposing Lanes | WB |
| Conflicting Approach Left | 3 |
| Conflicting Lanes Left | EB |
| Conflicting Approach Right | 3 |
| Conflicting Lanes Right | 18.7 |
| HCM Control Delay | C |
| HCM LOS |  |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 8.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 15 | 499 | 9 | 372 | 333 | 10 | 4 | 2 | 152 | 18 | 2 | 4 |
| Future Vol, veh/h | 15 | 499 | 9 | 372 | 333 | 10 | 4 | 2 | 152 | 18 | 2 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free |  | Free | Free | Free | Stop | Stop |  | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | one | - |  | None | - |  | None |
| Storage Length | 200 | - | 150 | 400 | - | 150 | 200 | - |  | 200 | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 16 | 542 | 10 | 404 | 362 | 11 | 4 | 2 | 165 | 20 | 2 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 288.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT | SBR |
| Traffic Vol, veh/h | 18 | 510 | 15 | 43 | 702 | 95 | 37 | 8 | 244 | 169 | 11 | 33 |
| Future Vol, veh/h | 18 | 510 | 15 | 43 | 702 | 95 | 37 | 8 |  | 169 | 11 | 33 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | None | - |  | None |  |  | None |
| Storage Length | - | - |  | - |  | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 20 | 554 | 16 | 47 | 763 | 103 | 40 | 9 | 265 | 184 | 12 | 36 |


| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 866 | 0 | 0 | 571 | 0 | 0 | 1534 | 1562 | 563 | 1647 | 1518 | 815 |
| Stage 1 | - | - | - | - | - | - | 602 | 602 |  | 908 | 908 |  |
| Stage 2 | - | - | - | - | - | - | 932 | 960 | - | 739 | 610 |  |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - | 3.518 | 4.018 | . 318 | 3.518 | 4.018 | . 318 |
| Pot Cap-1 Maneuver | 777 | - | - | 1002 | - | - | 95 | 112 | 526 | - 79 | 119 | 377 |
| Stage 1 | - | - | - | - | - | - | 486 | 489 | - | 330 | 354 |  |
| Stage 2 | - | - | - | - | - | - | 320 | 335 | - | 409 | 485 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 777 | - | - | 1002 | - | - | 71 | 98 | 526 | - 33 | 104 | 377 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 71 | 98 | - | - 33 | 104 |  |
| Stage 1 | - | - | - | - | - | - | 468 | 470 | - | 317 | 321 |  |
| Stage 2 | - | - | - | - | - | - | 253 | 304 | - | 191 | 467 |  |


| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 0.3 | 0.4 | 144.7 | F |
| HCM LOS |  |  | F |  |

Minor Lane/Major MvmNBLn1 EBL EBT EBR WBL WBT WBRSBLn1

| Capacity (veh/h) | 271 | 777 | - | -1002 | - | - |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| HCM Lane V/C Ratio | 1.159 | 0.025 | - | -0.047 | - | -5.788 |
| HCM Control Delay (s) | 144.7 | 9.8 | 0 | -8.8 | 0 | $\$ 2353.4$ |
| HCM Lane LOS | F | A | A | - | A | A |
| HCM 95th \%tile Q(veh) | 13.9 | 0.1 | - | - | F |  |
| H |  | 0.1 | - | -27.1 |  |  |

Notes
~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 28.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | D |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 11 | 377 | 3 | 0 | 63 | 365 | 72 | 0 | 18 | 4 | 118 |
| Future Vol, veh/h | 0 | 11 | 377 | 3 | 0 | 63 | 365 | 72 | 0 | 18 | 4 | 118 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 12 | 410 | 3 | 0 | 68 | 397 | 78 | 0 | 20 | 4 | 128 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 2 |  |  |  | 1 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 2 |  |  |  | 1 |  |  |
| Conflicting Approach Righ |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 2 |  |  |  | 3 |  |  |  | 2 |  |  |
| HCM Control Delay |  | 49.7 |  |  |  | 20.1 |  |  |  | 14.6 |  |  |

HCM LOS E C B

|  | NBLn1 | NBLn2 | EBLn1WBLn1 | Lancn | SBLn1 | SBLn2 | SBLn3 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $3 \%$ | $26 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $3 \%$ | $96 \%$ | $74 \%$ | $72 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, $\%$ | $0 \%$ | $97 \%$ | $1 \%$ | $0 \%$ | $28 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 18 | 122 | 391 | 246 | 255 | 152 | 5 | 34 |
| LT Vol | 18 | 0 | 11 | 63 | 0 | 152 | 0 | 0 |
| Through Vol | 0 | 4 | 377 | 183 | 183 | 0 | 5 | 0 |
| RT Vol | 0 | 118 | 3 | 0 | 72 | 0 | 0 | 34 |
| Lane Flow Rate | 20 | 133 | 425 | 267 | 277 | 165 | 5 | 37 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.052 | 0.309 | 0.907 | 0.574 | 0.569 | 0.425 | 0.013 | 0.082 |
| Departure Headway (Hd) | 9.614 | 8.38 | 7.791 | 7.851 | 7.517 | 9.271 | 8.753 | 8.027 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 374 | 431 | 467 | 462 | 484 | 390 | 411 | 449 |
| Service Time | 7.324 | 6.09 | 5.491 | 5.551 | 5.217 | 6.979 | 6.461 | 5.735 |
| HCM Lane V/C Ratio | 0.053 | 0.309 | 0.91 | 0.578 | 0.572 | 0.423 | 0.012 | 0.082 |
| HCM Control Delay | 12.9 | 14.8 | 49.7 | 20.6 | 19.7 | 18.7 | 11.6 | 11.5 |
| HCM Lane LOS | B | B | E | C | C | C | B | B |
| HCM 95th-tile Q | 0.2 | 1.3 | 10.1 | 3.5 | 3.5 | 2.1 | 0 | 0.3 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 152 | 5 | 34 |
| Future Vol, veh/h | 0 | 152 | 5 | 34 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 165 | 5 | 37 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 17.2 |
| HCM LOS | C |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 0 | 384 | 188 | 163 | 426 | 0 | 0 | 0 | 0 | 20 | 0 | 60 |
| Future Vol, veh/h | 0 | 384 | 188 | 163 | 426 | 0 | 0 | 0 | 0 | 20 | 0 | 60 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | ne | - |  | None | - |  | None |
| Storage Length | - | - | - | 250 | - | - | - | - | - | 0 | - | 500 |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 417 | 204 | 177 | 463 | 0 | 0 | 0 | 0 | 22 | 0 | 65 |


| Major/Minor | Major1 | Major2 |  |  |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 463 | 0 | 0 |  | 622 | 0 | 0 |  | 1337 | 1439 | 232 |
| Stage 1 | - | - | - |  | - | - | - |  | 817 | 817 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 520 | 622 |  |
| Critical Hdwy | 4.14 | - | - |  | 4.12 | - | - |  | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - |  | - | - | - |  | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - |  |  | - | - |  | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - |  | 2.218 | - | - |  | 3.519 | 4.019 | 3.319 |
| Pot Cap-1 Maneuver | 1095 | - | - |  | 959 | - | - |  | 156 | 132 | 771 |
| Stage 1 | - | - | - |  |  | - | - |  | 396 | 389 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 596 | 478 |  |
| Platoon blocked, \% |  | - | - |  |  | - | - |  |  |  |  |
| Mov Cap-1 Maneuver | 1095 | - | - |  | 959 | - | - |  | 127 | 0 | 771 |
| Mov Cap-2 Maneuver | - | - | - |  | - | - | - |  | 127 | 0 |  |
| Stage 1 | - | - | - |  |  | - |  |  | 323 | 0 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 596 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  |  | SB |  |  |
| HCM Control Delay, s | 0 |  |  |  | 2.7 |  |  |  | 17.3 |  |  |
| HCM LOS |  |  |  |  |  |  |  |  | C |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt EBL EBT EBR WBL WBT WBPBBLnISBLn2 |  |  |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 1095 | - | - | 959 | - | - | 127 | 771 |  |  |  |
| HCM Lane V/C Ratio | - | - |  | 0.185 | - |  | 0.171 | . 085 |  |  |  |
| HCM Control Delay (s) | 0 | - | - | 9.6 |  |  | 39.1 | 10.1 |  |  |  |
| HCM Lane LOS | A | - | - | A | - | - | E | B |  |  |  |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0.7 | - |  | 0.6 | 0.3 |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 13.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 73 | 486 | 0 | 0 | 393 | 147 | 195 | 0 | 394 | 0 | 0 | 0 |
| Future Vol, veh/h | 73 | 486 | 0 | 0 | 393 | 147 | 195 | 0 | 394 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - | - | - | 0 | - | 300 | - |  |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 79 | 528 | 0 | 0 | 427 | 160 | 212 | 0 | 428 | 0 | 0 | 0 |



HCM LOS E D C

| Lane | NBLn1 NBLn2 NBLn3 EBLn1 EBLn2 EBLn3WBLn1WBLn2WBLn3 SBLn1 SBLn2 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vol Left, \% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% |
| Vol Thru, \% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% |
| Vol Right, \% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 157 | 108 | 36 | 328 | 326 | 175 | 28 | 238 | 25 | 27 | 71 |
| LT Vol | 157 | 0 | 0 | 328 | 0 | 0 | 28 | 0 | 0 | 27 | 0 |
| Through Vol | 0 | 108 | 0 | 0 | 326 | 0 | 0 | 238 | 0 | 0 | 71 |
| RT Vol | 0 | 0 | 36 | 0 | 0 | 175 | 0 | 0 | 25 | 0 | 0 |
| Lane Flow Rate | 171 | 117 | 39 | 357 | 354 | 190 | 30 | 259 | 27 | 29 | 77 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.482 | 0.315 | 0.098 | 0.882 | 0.827 | 0.407 | 0.086 | 0.693 | 0.068 | 0.083 | 0.208 |
| Departure Headway (Hd) | 10.171 | 9.671 | 8.971 | 8.905 | 8.405 | 7.705 | 10.15 | 9.65 | 8.95 | 10.209 | 9.709 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 355 | 371 | 399 | 406 | 432 | 466 | 353 | 375 | 399 | 351 | 370 |
| Service Time | 7.939 | 7.439 | 6.739 | 6.661 | 6.161 | 5.461 | 7.919 | 7.419 | 6.719 | 7.977 | 7.477 |
| HCM Lane V/C Ratio | 0.482 | 0.315 | 0.098 | 0.879 | 0.819 | 0.408 | 0.085 | 0.691 | 0.068 | 0.083 | 0.208 |
| HCM Control Delay | 22.1 | 16.9 | 12.7 | 50.4 | 40.5 | 15.7 | 13.9 | 31.7 | 12.4 | 13.9 | 15 |
| HCM Lane LOS | C | C | B | F | E | C | B | D | B | B | B |
| HCM 95th-tile Q | 2.5 | 1.3 | 0.3 | 8.9 | 7.8 | 1.9 | 0.3 | 5 | 0.2 | 0.3 | 0.8 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 27 | 71 | 208 |
| Future Vol, veh/h | 0 | 27 | 71 | 208 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 29 | 77 | 226 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |
| :--- | ---: |
| Approach | NB |
| Opposing Approach | 3 |
| Opposing Lanes | WB |
| Conflicting Approach Left | 3 |
| Conflictin Lanes Left | EB |
| Conflictin Approach Right | 3 |
| Conflicting Lanes Right | 20.3 |
| HCM Control Delay | C |
| HCM LOS |  |
|  |  |
| Lane |  |


|  | $\gamma$ |  |  |  |  | 4 | 4 | 4 |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |  | $\uparrow$ |  |  | ${ }_{\text {¢ }}$ |  |
| Traffic Volume (veh/h) | 18 | 510 | 15 | 43 | 702 | 95 | 37 | 8 | 244 | 169 | 11 | 33 |
| Future Volume (veh/h) | 18 | 510 | 15 | 43 | 702 | 95 | 37 | 8 | 244 | 169 | 11 | 33 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1750 | 1863 | 1750 | 1750 | 1863 | 1750 | 1750 | 1863 | 1750 | 1750 | 1863 | 1750 |
| Adj Flow Rate, veh/h | 20 | 554 | 16 | 47 | 763 | 103 | 40 | 9 | 265 | 184 | 12 | 36 |
| Adj No. of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 56 | 931 | 26 | 74 | 824 | 109 | 94 | 44 | 505 | 353 | 27 | 57 |
| Arrive On Green | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.36 | 0.36 | 0.36 | 0.36 | 0.36 | 0.36 |
| Sat Flow, veh/h | 27 | 1702 | 48 | 58 | 1505 | 199 | 135 | 122 | 1387 | 774 | 75 | 156 |
| Grp Volume(v), veh/h | 590 | 0 | 0 | 913 | 0 | 0 | 314 | 0 | 0 | 232 | 0 | 0 |
| Grp Sat Flow(s), veh/h/ln | 1777 | 0 | 0 | 1763 | 0 | 0 | 1644 | 0 | 0 | 1005 | 0 | 0 |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.6 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 19.0 | 0.0 | 0.0 | 43.5 | 0.0 | 0.0 | 13.5 | 0.0 | 0.0 | 20.1 | 0.0 | 0.0 |
| Prop In Lane | 0.03 |  | 0.03 | 0.05 |  | 0.11 | 0.13 |  | 0.84 | 0.79 |  | 0.16 |
| Lane Grp Cap(c), veh/h | 1014 | 0 | 0 | 1006 | 0 | 0 | 643 | 0 | 0 | 437 | 0 | 0 |
| V/C Ratio(X) | 0.58 | 0.00 | 0.00 | 0.91 | 0.00 | 0.00 | 0.49 | 0.00 | 0.00 | 0.53 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 1067 | 0 | 0 | 1059 | 0 | 0 | 643 | 0 | 0 | 437 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 13.5 | 0.0 | 0.0 | 18.8 | 0.0 | 0.0 | 22.6 | 0.0 | 0.0 | 25.3 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.7 | 0.0 | 0.0 | 10.9 | 0.0 | 0.0 | 2.6 | 0.0 | 0.0 | 4.6 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ | /ln 9.9 | 0.0 | 0.0 | 24.1 | 0.0 | 0.0 | 6.6 | 0.0 | 0.0 | 5.5 | 0.0 | 0.0 |
| LnGrp Delay (d),s/veh | 14.3 | 0.0 | 0.0 | 29.7 | 0.0 | 0.0 | 25.2 | 0.0 | 0.0 | 29.9 | 0.0 | 0.0 |
| LnGrp LOS | B |  |  | C |  |  | C |  |  | C |  |  |
| Approach Vol, veh/h |  | 590 |  |  | 913 |  |  | 314 |  |  | 232 |  |
| Approach Delay, s/veh |  | 14.3 |  |  | 29.7 |  |  | 25.2 |  |  | 29.9 |  |
| Approach LOS |  | B |  |  | C |  |  | C |  |  | C |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs |  | 2 |  | 4 |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), |  | 36.8 |  | 53.2 |  | 36.8 |  | 53.2 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | 4.0 |  | 4.0 |  | 4.0 |  | 4.0 |  |  |  |  |
| Max Green Setting (Gmax) | ), s | 30.0 |  | 52.0 |  | 30.0 |  | 52.0 |  |  |  |  |
| Max Q Clear Time (g_c+1 | 11), s | 15.5 |  | 21.0 |  | 22.1 |  | 45.5 |  |  |  |  |
| Green Ext Time (p_c), s |  | 2.0 |  | 8.3 |  | 1.5 |  | 3.7 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl DelayHCM 2010 LOS |  |  | 24.6 |  |  |  |  |  |  |  |  |  |
|  |  |  | C |  |  |  |  |  |  |  |  |  |







## Intersection

Intersection Delay, s/veh 12.7
Intersection LOS
B

| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Traffic Vol, veh/h | 0 | 14 | 191 | 3 | 0 | 20 | 466 | 45 | 0 | 5 | 0 | 39 |
| Future Vol, veh/h | 0 | 14 | 191 | 3 | 0 | 20 | 466 | 45 | 0 | 5 | 0 | 39 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 15 | 208 | 3 | 0 | 22 | 507 | 49 | 0 | 5 | 0 | 42 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Opposing Approach | WB | EB | SB |
| Opposing Lanes | 2 | 1 | 3 |
| Conflicting Approach Left | SB | NB | EB |
| Conflicting Lanes Left | 3 | 2 | 1 |
| Conflicting Approach Right | NB | SB | WB |
| Conflicting Lanes Right | 2 | 3 | 2 |
| HCM Control Delay | 13.2 | 13.1 | 9.8 |

HCM LOS B B A

|  | NBLn1 | NBLn2 | EBLn1WBLn1 | Lancn | SBLn1 | SBLn2 | SBLn3 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, $\%$ | $100 \%$ | $0 \%$ | $7 \%$ | $8 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $0 \%$ | $92 \%$ | $92 \%$ | $84 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, $\%$ | $0 \%$ | $100 \%$ | $1 \%$ | $0 \%$ | $16 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 5 | 39 | 208 | 253 | 278 | 52 | 0 | 41 |
| LT Vol | 5 | 0 | 14 | 20 | 0 | 52 | 0 | 0 |
| Through Vol | 0 | 0 | 191 | 233 | 233 | 0 | 0 | 0 |
| RT Vol | 0 | 39 | 3 | 0 | 45 | 0 | 0 | 41 |
| Lane Flow Rate | 5 | 42 | 226 | 275 | 302 | 57 | 0 | 45 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.012 | 0.076 | 0.398 | 0.438 | 0.469 | 0.118 | 0 | 0.078 |
| Departure Headway (Hd) | 7.672 | 6.447 | 6.335 | 5.738 | 5.584 | 7.496 | 6.986 | 6.273 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 466 | 554 | 567 | 627 | 644 | 478 | 0 | 570 |
| Service Time | 5.428 | 4.202 | 4.079 | 3.474 | 3.32 | 5.249 | 4.739 | 4.025 |
| HCM Lane V/C Ratio | 0.011 | 0.076 | 0.399 | 0.439 | 0.469 | 0.119 | 0 | 0.079 |
| HCM Control Delay | 10.5 | 9.7 | 13.2 | 12.9 | 13.2 | 11.3 | 9.7 | 9.6 |
| HCM Lane LOS | B | A | B | B | B | B | N | A |
| HCM 95th-tile Q | 0 | 0.2 | 1.9 | 2.2 | 2.5 | 0.4 | 0 | 0.3 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 52 | 0 | 41 |
| Future Vol, veh/h | 0 | 52 | 0 | 41 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 57 | 0 | 45 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 10.6 |
| HCM LOS | B |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 6.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 0 | 171 | 111 | 286 | 442 | 0 | 0 | 0 | 0 | 59 | 0 | 89 |
| Future Vol, veh/h | 0 | 171 | 111 | 286 | 442 | 0 | 0 | 0 | 0 | 59 | 0 | 89 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  |  | - |  | None | - |  | None |
| Storage Length | - | - | - | 250 | - | - | - | - | - | 0 | - | 500 |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 |  | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 186 | 121 | 311 | 480 | 0 | 0 | 0 | 0 | 64 | 0 | 97 |


| Major/Minor | Major1 | Major2 |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 480 | 0 | 0 | 307 | 0 | 0 | 1348 | 1409 | 240 |
| Stage 1 | - | - | - |  | - | - | 1102 | 1102 |  |
| Stage 2 | - | - | - | - | - | - | 246 | 307 |  |
| Critical Hdwy | 4.14 | - | - | 4.12 | - | - | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - | 2.218 | - | - | 3.519 | 4.019 | . 319 |
| Pot Cap-1 Maneuver | 1079 | - | - | 1254 | - | - | 154 | 138 | 762 |
| Stage 1 | - | - | - | - | - | - | 281 | 286 |  |
| Stage 2 | - | - | - | - | - | - | 794 | 660 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1079 | - | - | 1254 | - | - | 116 | 0 | 762 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 116 | 0 |  |
| Stage 1 | - | - | - | - | - | - | 211 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 794 | 0 |  |


| Approach | EB | WB | SB |
| :--- | :---: | ---: | ---: |
| HCM Control Delay, s | 0 | 3.5 | 33.8 |

HCM LOS D

Minor Lane/Major Mvmt EBL EBT EBR WBL WBT WBFBBLnisBLn2

| Capacity (veh/h) | 1079 | - | -1254 | - | -116 | 762 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| HCM Lane V/C Ratio | - | - | -0.248 | - | -0.5530 .127 |  |
| HCM Control Delay (s) | 0 | - | -8.8 | - | - | 69 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 32 | 198 | 0 | 0 | 564 | 158 | 164 | 0 | 82 | 0 | 0 | 0 |
| Future Vol, veh/h | 32 | 198 | 0 | 0 | 564 | 158 | 164 | 0 | 82 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop |  | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - | - | - | 0 | - | 300 | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 35 | 215 | 0 | 0 | 613 | 172 | 178 | 0 | 89 | 0 | 0 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 16.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS C |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 95 | 118 | 67 | 0 | 22 | 234 | 22 | 0 | 190 | 53 | 19 |
| Future Vol, veh/h | 0 | 95 | 118 | 67 | 0 | 22 | 234 | 22 | 0 | 190 | 53 | 19 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 103 | 128 | 73 | 0 | 24 | 254 | 24 | 0 | 207 | 58 | 21 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Righ |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 13 |  |  |  | 18.3 |  |  |  | 16.5 |  |  |
| HCM LOS |  | B |  |  |  | C |  |  |  | C |  |  |


| Lane | NBLn1 | NBLn2 | NBLn3 | EBLn1 | BLn2 | Ln | Ln | BLn | BLn | BLn | SBLn2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vol Left, \% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% |
| Vol Thru, \% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% |
| Vol Right, \% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 190 | 53 | 19 | 95 | 118 | 67 | 22 | 234 | 22 | 32 | 59 |
| LT Vol | 190 | 0 | 0 | 95 | 0 | 0 | 22 | 0 | 0 | 32 | 0 |
| Through Vol | 0 | 53 | 0 | 0 | 118 | 0 | 0 | 234 | 0 | 0 | 59 |
| RT Vol | 0 | 0 | 19 | 0 | 0 | 67 | 0 | 0 | 22 | 0 | 0 |
| Lane Flow Rate | 207 | 58 | 21 | 103 | 128 | 73 | 24 | 254 | 24 | 35 | 64 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.476 | 0.125 | 0.041 | 0.239 | 0.279 | 0.144 | 0.055 | 0.55 | 0.047 | 0.078 | 0.135 |
| Departure Headway (Hd) | 8.29 | 7.79 | 7.09 | 8.324 | 7.824 | 7.124 | 8.288 | 7.788 | 7.088 | 8.058 | 7.558 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 434 | 459 | 504 | 431 | 458 | 502 | 431 | 463 | 504 | 444 | 474 |
| Service Time | 6.053 | 5.553 | 4.853 | 6.088 | 5.588 | 4.888 | 6.052 | 5.552 | 4.852 | 5.815 | 5.315 |
| HCM Lane V/C Ratio | 0.477 | 0.126 | 0.042 | 0.239 | 0.279 | 0.145 | 0.056 | 0.549 | 0.048 | 0.079 | 0.135 |
| HCM Control Delay | 18.4 | 11.7 | 10.2 | 13.7 | 13.6 | 11.1 | 11.5 | 19.7 | 10.2 | 11.5 | 11.5 |
| HCM Lane LOS | C | B | B | B | B | B | B | C | B | B | B |
| HCM 95th-tile Q | 2.5 | 0.4 | 0.1 | 0.9 | 1.1 | 0.5 | 0.2 | 3.3 | 0.1 | 0.3 | 0.5 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 32 | 59 | 298 |
| Future Vol, veh/h | 0 | 32 | 59 | 298 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 35 | 64 | 324 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |
| :--- | ---: |
| Approach | NB |
| Opposing Approach | 3 |
| Opposing Lanes | WB |
| Conflicting Approach Left | 3 |
| Conflicting Lanes Left | EB |
| Conflicting Approach Right | 3 |
| Conflicting Lanes Right | 18.1 |
| HCM Control Delay | C |
| HCM LOS |  |
|  |  |
| Lane |  |




| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 14.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS B |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 15 | 210 | 4 | 0 | 20 | 543 | 45 | 0 | 10 | 0 | 39 |
| Future Vol, veh/h | 0 | 15 | 210 | 4 | 0 | 20 | 543 | 45 | 0 | 10 | 0 | 39 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 16 | 228 | 4 | 0 | 22 | 590 | 49 | 0 | 11 | 0 | 42 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 2 |  |  |  | 1 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 2 |  |  |  | 1 |  |  |
| Conflicting Approach Right |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 2 |  |  |  | 3 |  |  |  | 2 |  |  |
| HCM Control Delay |  | 14.7 |  |  |  | 15.1 |  |  |  | 10.3 |  |  |

HCM LOS B C B B

| Lane | NBLn1 NBLn2 EBLn1WBLn1WBLn2 SBLn1 SBLn2 SBLn3 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vol Left, \% | 100\% | 0\% | 7\% | 7\% | 0\% | 100\% | 0\% | 0\% |
| Vol Thru, \% | 0\% | 0\% | 92\% | 93\% | 86\% | 0\% | 100\% | 0\% |
| Vol Right, \% | 0\% | 100\% | 2\% | 0\% | 14\% | 0\% | 0\% | 100\% |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 10 | 39 | 229 | 292 | 317 | 52 | 0 | 45 |
| LT Vol | 10 | 0 | 15 | 20 | 0 | 52 | 0 | 0 |
| Through Vol | 0 | 0 | 210 | 272 | 272 | 0 | 0 | 0 |
| RT Vol | 0 | 39 | 4 | 0 | 45 | 0 | 0 | 45 |
| Lane Flow Rate | 11 | 42 | 249 | 317 | 344 | 57 | 0 | 49 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.024 | 0.08 | 0.454 | 0.517 | 0.549 | 0.123 | 0 | 0.09 |
| Departure Headway (Hd) | 7.997 | 6.768 | 6.569 | 5.877 | 5.742 | 7.818 | 7.307 | 6.592 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 446 | 527 | 548 | 612 | 626 | 457 | 0 | 541 |
| Service Time | 5.772 | 4.542 | 4.326 | 3.621 | 3.486 | 5.585 | 5.074 | 4.358 |
| HCM Lane V/C Ratio | 0.025 | 0.08 | 0.454 | 0.518 | 0.55 | 0.125 | 0 | 0.091 |
| HCM Control Delay | 11 | 10.1 | 14.7 | 14.8 | 15.3 | 11.7 | 10.1 | 10 |
| HCM Lane LOS | B | B | B | B | C | B | N | A |
| HCM 95th-tile Q | 0.1 | 0.3 | 2.3 | 3 | 3.3 | 0.4 | 0 | 0.3 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 52 | 0 | 45 |
| Future Vol, veh/h | 0 | 52 | 0 | 45 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 57 | 0 | 49 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 10.9 |
| HCM LOS | B |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 7.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 0 | 188 | 113 | 286 | 512 | 0 | 0 | 0 | 0 | 59 | 0 | 96 |
| Future Vol, veh/h | 0 | 188 | 113 | 286 | 512 | 0 | 0 | 0 | 0 | 59 | 0 | 96 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free |  | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | ne | - |  | None | - |  | None |
| Storage Length | - |  |  | 250 | - | - | - |  |  | 0 | - | 500 |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 |  | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 204 | 123 | 311 | 557 | 0 | 0 | 0 | 0 | 64 | 0 |  |


| Major/Minor | Major1 | Major2 |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 557 | 0 | 0 | 327 | 0 | 0 | 1444 | 1505 | 278 |
| Stage 1 | - | - | - |  | - | - | 1178 | 1178 |  |
| Stage 2 | - | - | - | - | - | - | 266 | 327 |  |
| Critical Hdwy | 4.14 | - | - | 4.12 | - | - | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - |  | - | - | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - | 2.218 | - | - | 3.519 | 4.019 | . 319 |
| Pot Cap-1 Maneuver | 1010 | - | - | 1233 | - | - | 134 | 121 | 720 |
| Stage 1 | - | - | - | - | - | - | 256 | 264 |  |
| Stage 2 | - | - | - | - | - | - | 778 | 647 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1010 | - | - | 1233 | - | - | 100 | 0 | 720 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 100 | 0 |  |
| Stage 1 | - | - | - | - | - | - | 191 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 778 | 0 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 35 | 212 | 0 | 0 | 622 | 158 | 171 | 0 | 82 | 0 | 0 | 0 |
| Future Vol, veh/h | 35 | 212 | 0 | 0 | 622 | 158 | 171 | 0 | 82 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - |  | - | 0 | - | 300 | - | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 38 | 230 | 0 | 0 | 676 | 172 | 186 | 0 | 89 | 0 | 0 | 0 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 19 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS C |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 98 | 127 | 69 | 0 | 22 | 268 | 22 | 0 | 199 | 53 | 19 |
| Future Vol, veh/h | 0 | 98 | 127 | 69 | 0 | 22 | 268 | 22 | 0 | 199 | 53 | 19 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 107 | 138 | 75 | 0 | 24 | 291 | 24 | 0 | 216 | 58 | 21 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Right |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 13.7 |  |  |  | 22.6 |  |  |  | 18 |  |  |
| HCM LOS |  | B |  |  |  | C |  |  |  | C |  |  |


| Lane | NBLn1 NBLn2 NBLn3 EBLn1 EBLn2 EBLn3WBLn1WBLn2WBLn3 SBLn1 SBLn2 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vol Left, \% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% |
| Vol Thru, \% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% |
| Vol Right, \% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 199 | 53 | 19 | 98 | 127 | 69 | 22 | 268 | 22 | 32 | 59 |
| LT Vol | 199 | 0 | 0 | 98 | 0 | 0 | 22 | 0 | 0 | 32 | 0 |
| Through Vol | 0 | 53 | 0 | 0 | 127 | 0 | 0 | 268 | 0 | 0 | 59 |
| RT Vol | 0 | 0 | 19 | 0 | 0 | 69 | 0 | 0 | 22 | 0 | 0 |
| Lane Flow Rate | 216 | 58 | 21 | 107 | 138 | 75 | 24 | 291 | 24 | 35 | 64 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.516 | 0.13 | 0.042 | 0.255 | 0.311 | 0.154 | 0.056 | 0.648 | 0.049 | 0.081 | 0.14 |
| Departure Headway (Hd) | 8.594 | 8.094 | 7.394 | 8.607 | 8.107 | 7.407 | 8.503 | 8.003 | 7.303 | 8.34 | 7.84 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 417 | 441 | 482 | 415 | 442 | 482 | 420 | 449 | 488 | 428 | 456 |
| Service Time | 6.377 | 5.877 | 5.177 | 6.39 | 5.89 | 5.19 | 6.282 | 5.782 | 5.082 | 6.115 | 5.615 |
| HCM Lane V/C Ratio | 0.518 | 0.132 | 0.044 | 0.258 | 0.312 | 0.156 | 0.057 | 0.648 | 0.049 | 0.082 | 0.14 |
| HCM Control Delay | 20.3 | 12.1 | 10.5 | 14.3 | 14.5 | 11.5 | 11.8 | 24.5 | 10.5 | 11.9 | 11.9 |
| HCM Lane LOS | C | B | B | B | B | B | B | C | B | B | B |
| HCM 95th-tile Q | 2.9 | 0.4 | 0.1 | 1 | 1.3 | 0.5 | 0.2 | 4.5 | 0.2 | 0.3 | 0.5 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 32 | 59 | 312 |
| Future Vol, veh/h | 0 | 32 | 59 | 312 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 35 | 64 | 339 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |
| :--- | ---: |
| Approach | NB |
| Opposing Approach | 3 |
| Opposing Lanes | WB |
| Conflicting Approach Left | 3 |
| Conflicting Lanes Left | EB |
| Conflicting Approach Right | 3 |
| Conflicting Lanes Right | 20.9 |
| HCM Control Delay | C |
| HCM LOS |  |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 0 | 50 | 5 | 88 | 145 | 3 | 3 | 0 |  | 7 | 0 | 1 |
| Future Vol, veh/h | 0 | 50 | 5 | 88 | 145 | 3 | 3 | 0 | 113 | 7 | 0 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop |  | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 200 | - | 150 | 400 | - | 150 | 200 | - | - | 200 | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 54 | 5 | 96 | 158 | 3 | 3 | 0 | 123 | 8 | 0 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 3 | 238 | 17 | 43 | 541 | 7 | 19 | 0 | 103 | 4 | 0 | 7 |
| Future Vol, veh/h | 3 | 238 | 17 | 43 | 541 | 7 | 19 | 0 | 103 | 4 | 0 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  |  | - |  | None | - |  | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# - | 0 |  | - | 0 | - | - | 0 | - |  | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |  | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 259 | 18 | 47 | 588 | 8 | 21 | 0 | 112 | 4 | 0 | 8 |


| Major/Minor | Major1 |  |  | Major2 |  | Minor1 |  |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 596 | 0 | 0 | 277 | 0 | 0 |  | 963 | 963 | 268 | 1015 | 969 | 592 |
| Stage 1 | - | - | - | - | - |  |  | 274 | 274 |  | 685 | 685 |  |
| Stage 2 | - | - | - | - | - |  |  | 689 | 689 | - | 330 | 284 |  |
| Critical Hdwy | 4.12 | - | - | 4.12 | - |  |  | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | - |  |  | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Critical Hdwy Stg 2 | - | - | - |  | - |  |  | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - |  |  | 3.518 | . 018 | 3.318 | 3.518 | . 018 | 3.318 |
| Pot Cap-1 Maneuver | 980 | - | - | 1286 | - |  |  | 235 | 256 | 771 | 217 | 254 | 506 |
| Stage 1 | - | - | - |  | - |  |  | 732 | 683 |  | 438 | 448 |  |
| Stage 2 | - | - | - | - | - |  |  | 436 | 446 | - | 683 | 676 |  |
| Platoon blocked, \% |  | - | - |  | - |  |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 980 | - | - | 1286 | - |  |  | 221 | 241 | 771 | 177 | 239 | 506 |
| Mov Cap-2 Maneuver | - | - | - | - | - |  |  | 221 | 241 |  | 177 | 239 |  |
| Stage 1 | - |  | - |  |  |  |  | 729 | 680 |  | 436 | 423 |  |
| Stage 2 | - | - | - | - | - |  |  | 406 | 421 |  | 581 | 673 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 0.1 |  |  | 0.6 |  |  |  | 13.5 |  |  | 17.4 |  |  |
| HCM LOS |  |  |  |  |  |  |  | B |  |  | C |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major MvmNBLn1 EBL EBT EBR WBL WBT WBFSBLn1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 556 | 980 | - | - 1286 | - |  | 302 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.239 | . 003 | - | -0.036 | - |  | - 0.04 |  |  |  |  |  |  |
| HCM Control Delay (s) | 13.5 | 8.7 | 0 | - 7.9 | 0 |  | - 17.4 |  |  |  |  |  |  |
| HCM Lane LOS | B | A | A | - A | A |  | C |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 0.9 | 0 | - | - 0.1 | - |  | - 0.1 |  |  |  |  |  |  |

## Intersection

Intersection Delay, s/veh 14.1
Intersection LOS
B

| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Traffic Vol, veh/h | 0 | 15 | 203 | 3 | 0 | 22 | 510 | 49 | 0 | 7 | 0 | 51 |
| Future Vol, veh/h | 0 | 15 | 203 | 3 | 0 | 22 | 510 | 49 | 0 | 7 | 0 | 51 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 16 | 221 | 3 | 0 | 24 | 554 | 53 | 0 | 8 | 0 | 55 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Opposing Approach | WB | EB | SB |
| Opposing Lanes | 2 | 1 | 3 |
| Conflicting Approach Left | SB | NB | EB |
| Conflicting Lanes Left | 3 | 2 | 1 |
| Conflicting Approach Right | NB | SB | WB |
| Conflicting Lanes Right | 2 | 3 | 2 |
| HCM Control Delay | 14.6 | 14.8 | 10.4 |


| HCM LOS B | B | B |
| :---: | :---: | :---: | :---: |


| Lane | NBLn1 NBLn2 EBLn1WBLn1WBLn2 SBLn1 SBLn2 SBLn3 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vol Left, \% | 100\% | 0\% | 7\% | 8\% | 0\% | 100\% | 0\% | 0\% |
| Vol Thru, \% | 0\% | 0\% | 92\% | 92\% | 84\% | 0\% | 100\% | 0\% |
| Vol Right, \% | 0\% | 100\% | 1\% | 0\% | 16\% | 0\% | 0\% | 100\% |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 7 | 51 | 221 | 277 | 304 | 63 | 0 | 50 |
| LT Vol | 7 | 0 | 15 | 22 | 0 | 63 | 0 | 0 |
| Through Vol | 0 | 0 | 203 | 255 | 255 | 0 | 0 | 0 |
| RT Vol | 0 | 51 | 3 | 0 | 49 | 0 | 0 | 50 |
| Lane Flow Rate | 8 | 55 | 240 | 301 | 330 | 68 | 0 | 54 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.017 | 0.104 | 0.443 | 0.499 | 0.533 | 0.148 | 0 | 0.099 |
| Departure Headway (Hd) | 7.984 | 6.756 | 6.633 | 5.962 | 5.808 | 7.78 | 7.269 | 6.554 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 446 | 528 | 540 | 602 | 621 | 459 | 0 | 544 |
| Service Time | 5.765 | 4.535 | 4.395 | 3.711 | 3.557 | 5.553 | 5.042 | 4.326 |
| HCM Lane V/C Ratio | 0.018 | 0.104 | 0.444 | 0.5 | 0.531 | 0.148 | 0 | 0.099 |
| HCM Control Delay | 10.9 | 10.3 | 14.6 | 14.5 | 15 | 11.9 | 10 | 10.1 |
| HCM Lane LOS | B | B | B | B | B | B | N | B |
| HCM 95th-tile Q | 0.1 | 0.3 | 2.3 | 2.8 | 3.1 | 0.5 | 0 | 0.3 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 63 | 0 | 50 |
| Future Vol, veh/h | 0 | 63 | 0 | 50 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 68 | 0 | 54 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 11.1 |
| HCM LOS | B |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 8.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 0 | 187 | 121 | 312 | 482 | 0 | 0 | 0 | 0 | 62 | 0 | 94 |
| Future Vol, veh/h | 0 | 187 | 121 | 312 | 482 | 0 | 0 | 0 | 0 | 62 | 0 | 94 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free |  | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  |  | - |  | one | - |  | None |
| Storage Length | - | - | - | 250 | - | - | - | - | - | 0 |  | 500 |
| Veh in Median Storage, \# | - | 0 |  |  | 0 |  | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 203 | 132 | 339 | 524 | 0 | 0 | 0 | 0 | 67 | 0 | 102 |


| Major/Minor | Major1 | Major2 |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 524 | 0 | 0 | 335 | 0 | 0 | 1471 | 1537 | 262 |
| Stage 1 | - | - | - |  | - | - | 1202 | 1202 |  |
| Stage 2 | - | - | - | - | - | - | 269 | 335 |  |
| Critical Hdwy | 4.14 | - | - | 4.12 | - | - | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - | 2.218 | - | - | 3.519 | . 019 | 3.319 |
| Pot Cap-1 Maneuver | 1039 | - | - | 1224 | - | - | 128 | 115 | 737 |
| Stage 1 | - | - | - | - | - | - | 248 | 257 |  |
| Stage 2 | - | - | - | - | - | - | 775 | 642 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1039 | - | - | 1224 | - | - | 93 | 0 | 737 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 93 | 0 |  |
| Stage 1 | - | - | - |  | - | - | 179 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 775 | 0 |  |


| Approach | EB | WB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 3.6 | 50.2 |
| HCM LOS |  | $F$ |  |

Minor Lane/Major Mvmt EBL EBT EBR WBL WBT WBFBBLnisBLn2

| Capacity (veh/h) | 1039 | - | -1224 | - | - | 93 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| 737 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | - | - | -0.277 | - | -0.725 | 0.139 |
| HCM Control Delay (s) | 0 | - | - | 9.1 | - | -110.1 |
| 10.7 |  |  |  |  |  |  |
| HCM Lane LOS | A | - | - | A | - | - |
| HCM 95 th \%tile Q(veh) | 0 | - | - | 1.1 | - | - |
| H | 3.7 | 0.5 |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL WBT WBR |  |  | NBL | NBT | NBR | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 35 | 216 | 0 | 0 | 612 | 171 | 182 | 0 | 91 | 0 | 0 | 0 |
| Future Vol, veh/h | 35 | 216 | 0 | 0 | 612 | 171 | 182 | 0 | 91 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | one | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - | - | - | 0 | - | 300 | - | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 |  | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 38 | 235 | 0 | 0 | 665 | 186 | 198 | 0 | 99 | 0 | 0 | 0 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 20.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS C |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 103 | 128 | 73 | 0 | 24 | 256 | 24 | 0 | 216 | 60 | 22 |
| Future Vol, veh/h | 0 | 103 | 128 | 73 | 0 | 24 | 256 | 24 | 0 | 216 | 60 | 22 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 112 | 139 | 79 | 0 | 26 | 278 | 26 | 0 | 235 | 65 | 24 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Right |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 14.3 |  |  |  | 22.6 |  |  |  | 19.7 |  |  |
| HCM LOS |  | B |  |  |  | C |  |  |  | C |  |  |


| Lane | NBLn1 | NBLn2 | NBLn3 | EBLn1 | EBLn2 | EBLn3WBLn1WBLn2WBLn3 | SBLn1 | SBLn2 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, $\%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Vol Right, $\%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 216 | 60 | 22 | 103 | 128 | 73 | 24 | 256 | 24 | 36 | 66 |
| LT Vol | 216 | 0 | 0 | 103 | 0 | 0 | 24 | 0 | 0 | 36 | 0 |
| Through Vol | 0 | 60 | 0 | 0 | 128 | 0 | 0 | 256 | 0 | 0 | 66 |
| RT Vol | 0 | 0 | 22 | 0 | 0 | 73 | 0 | 0 | 24 | 0 | 0 |
| Lane Flow Rate | 235 | 65 | 24 | 112 | 139 | 79 | 26 | 278 | 26 | 39 | 72 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.57 | 0.149 | 0.05 | 0.274 | 0.322 | 0.168 | 0.064 | 0.639 | 0.055 | 0.092 | 0.159 |
| Departure Headway (Hd) | 8.746 | 8.246 | 7.546 | 8.826 | 8.326 | 7.626 | 8.771 | 8.271 | 7.571 | 8.491 | 7.991 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 411 | 432 | 472 | 405 | 430 | 467 | 407 | 434 | 470 | 421 | 447 |
| Service Time | 6.539 | 6.039 | 5.339 | 6.618 | 6.118 | 5.418 | 6.56 | 6.06 | 5.36 | 6.274 | 5.774 |
| HCM Lane V/C Ratio | 0.572 | 0.15 | 0.051 | 0.277 | 0.323 | 0.169 | 0.064 | 0.641 | 0.055 | 0.093 | 0.161 |
| HCM Control Delay | 22.6 | 12.5 | 10.7 | 14.9 | 15.1 | 12 | 12.2 | 24.7 | 10.8 | 12.1 | 12.3 |
| HCM Lane LOS | C | B | B | B | C | B | B | C | B | B | B |
| HCM 95th-tile Q | 3.4 | 0.5 | 0.2 | 1.1 | 1.4 | 0.6 | 0.2 | 4.3 | 0.2 | 0.3 | 0.6 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 36 | 66 | 331 |
| Future Vol, veh/h | 0 | 36 | 66 | 331 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 39 | 72 | 360 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |
| :--- | ---: |
| Approach | NB |
| Opposing Approach | 3 |
| Opposing Lanes | WB |
| Conflicting Approach Left | 3 |
| Conflicting Lanes Left | EB |
| Conflicting Approach Right | 3 |
| Conflicting Lanes Right | 23.8 |
| HCM Control Delay | C |
| HCM LOS |  |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 0 | 61 | 5 | 130 | 191 | 3 | 3 | 0 | 124 | 7 | 0 | 1 |
| Future Vol, veh/h | 0 | 61 | 5 | 130 | 191 | 3 | 3 | 0 | 124 | 7 | 0 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 200 | - | 150 | 400 | - | 150 | 200 | - | - | 200 | - |  |
| Veh in Median Storage, \# | \# - | 0 |  |  | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |  | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 66 | 5 | 141 | 208 | 3 | 3 | 0 | 135 | 8 | 0 | 1 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.2 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 3 | 259 | 17 | 43 | 627 | 7 | 19 | 0 |  | 4 | 0 | 7 |
| Future Vol, veh/h | 3 | 259 | 17 | 43 | 627 | 7 | 19 | 0 | 103 | 4 | 0 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop |  | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | ne | - |  | None | - |  | None |
| Storage Length | - | - |  | - | - | - |  | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 282 | 18 | 47 | 682 | 8 | 21 | 0 | 112 | 4 | 0 | 8 |


| Major/Minor | Major1 |  |  | Major2 |  | Minor1 |  |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 689 | 0 | 0 | 300 | 0 | 0 |  | 1080 | 1080 | 291 | 1132 | 1086 | 685 |
| Stage 1 | - | - | - | - | - | - |  | 297 | 297 |  | 779 | 779 |  |
| Stage 2 | - | - | - | - | - | - |  | 783 | 783 | - | 353 | 307 |  |
| Critical Hdwy | 4.12 | - | - | 4.12 | - |  |  | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  | 6.12 | 5.52 | - | 6.12 | 5.52 |  |
| Critical Hdwy Stg 2 | - | - | - |  | - | - |  | 6.12 | 5.52 |  | 6.12 | 5.52 |  |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - |  | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 |
| Pot Cap-1 Maneuver | 905 | - | - | 1261 | - | - |  | 196 | 218 | 748 | 180 | 216 | 448 |
| Stage 1 | - | - | - |  | - | - |  | 712 | 668 |  | 389 | 406 |  |
| Stage 2 | - | - | - | - | - |  |  | 387 | 404 | - | 664 | 661 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 905 | - | - | 1261 | - | - |  | 183 | 204 | 748 | 146 | 202 | 448 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  | 183 | 204 | - | 146 | 202 |  |
| Stage 1 | - | - | - |  |  |  |  | 709 | 665 |  | 387 | 382 |  |
| Stage 2 | - | - | - | - | - |  |  | 358 | 380 |  | 562 | 658 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 0.1 |  |  | 0.5 |  |  |  | 14.6 |  |  | 19.8 |  |  |
| HCM LOS |  |  |  |  |  |  |  | B |  |  | C |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major MvmNBLn1 EBL EBT EBR WBL WBT WBFSBLn1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 505 | 05 | - | - 1261 | - | - | 256 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.263 |  | - | -0.037 | - |  | 0.047 |  |  |  |  |  |  |
| HCM Control Delay (s) | 14.6 | 9 | 0 | 8 | 0 |  | - 19.8 |  |  |  |  |  |  |
| HCM Lane LOS | B | A | A | A | A |  | C |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 1 | 0 | - | - 0.1 | - |  | - 0.1 |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 16.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS C |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 16 | 222 | 4 | 0 | 22 | 587 | 49 | 0 | 12 | 0 | 51 |
| Future Vol, veh/h | 0 | 16 | 222 | 4 | 0 | 22 | 587 | 49 | 0 | 12 | 0 | 51 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 17 | 241 | 4 | 0 | 24 | 638 | 53 | 0 | 13 | 0 | 55 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 2 |  |  |  | 1 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 2 |  |  |  | 1 |  |  |
| Conflicting Approach Righ |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 2 |  |  |  | 3 |  |  |  | 2 |  |  |
| HCM Control Delay |  | 16.5 |  |  |  | 17.6 |  |  |  | 10.9 |  |  |

HCM LOS C C B B

| Lane | NBLn1 | NBLn2 | EBLn1WBLn1WBLn2 | SBLn1 | SBLn2 SBLn3 |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, $\%$ | $100 \%$ | $0 \%$ | $7 \%$ | $7 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $0 \%$ | $92 \%$ | $93 \%$ | $86 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $2 \%$ | $0 \%$ | $14 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 12 | 51 | 242 | 316 | 343 | 63 | 0 | 54 |
| LT Vol | 12 | 0 | 16 | 22 | 0 | 63 | 0 | 0 |
| Through Vol | 0 | 0 | 222 | 294 | 294 | 0 | 0 | 0 |
| RT Vol | 0 | 51 | 4 | 0 | 49 | 0 | 0 | 54 |
| Lane Flow Rate | 13 | 55 | 263 | 343 | 372 | 68 | 0 | 59 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.03 | 0.109 | 0.502 | 0.582 | 0.618 | 0.154 | 0 | 0.112 |
| Departure Headway (Hd) | 8.317 | 7.085 | 6.876 | 6.111 | 5.975 | 8.105 | 7.593 | 6.876 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 428 | 502 | 521 | 590 | 603 | 440 | 0 | 518 |
| Service Time | 6.115 | 4.882 | 4.651 | 3.871 | 3.735 | 5.895 | 5.382 | 4.664 |
| HCM Lane V/C Ratio | 0.03 | 0.11 | 0.505 | 0.581 | 0.617 | 0.155 | 0 | 0.114 |
| HCM Control Delay | 11.4 | 10.8 | 16.5 | 17.1 | 18 | 12.4 | 10.4 | 10.5 |
| HCM Lane LOS | B | B | C | C | C | B | N | B |
| HCM 95th-tile Q | 0.1 | 0.4 | 2.8 | 3.7 | 4.2 | 0.5 | 0 | 0.4 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 63 | 0 | 54 |
| Future Vol, veh/h | 0 | 63 | 0 | 54 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 68 | 0 | 59 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 11.5 |
| HCM LOS | B |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 9.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 0 | 204 | 123 | 312 | 552 | 0 | 0 | 0 | 0 | 62 | 0 | 101 |
| Future Vol, veh/h | 0 | 204 | 123 | 312 | 552 | 0 | 0 | 0 | 0 | 62 | 0 | 101 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free |  | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  |  | - |  | one | - |  | None |
| Storage Length | - | - | - | 250 | - | - | - | - |  | 0 |  | 500 |
| Veh in Median Storage, \# | - | 0 |  |  | 0 |  | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 222 | 134 | 339 | 600 | 0 | 0 | 0 | 0 | 67 | 0 | 110 |


| Major/Minor | Major1 | Major2 |  |  |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 600 | 0 | 0 |  | 355 | 0 | 0 |  | 1567 | 1633 | 300 |
| Stage 1 | - | - | - |  | - | - | - |  | 1278 | 1278 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 289 | 355 |  |
| Critical Hdwy | 4.14 | - | - |  | 4.12 | - | - |  | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - |  | - | - | - |  | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - |  |  | - | - |  | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - |  | 2.218 | - | - |  | 3.519 | 4.019 | 3.319 |
| Pot Cap-1 Maneuver | 973 | - | - |  | 1204 | - | - |  | 112 | 101 | 697 |
| Stage 1 | - | - | - |  |  | - | - |  | 226 | 236 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 759 | 629 |  |
| Platoon blocked, \% |  | - | - |  |  | - | - |  |  |  |  |
| Mov Cap-1 Maneuver | 973 | - | - |  | 1204 | - | - |  | 80 | 0 | 697 |
| Mov Cap-2 Maneuver | - | - | - |  | - | - | - |  | 80 | 0 |  |
| Stage 1 | - | - | - |  |  | - |  |  | 162 | 0 |  |
| Stage 2 | - | - | - |  | - | - | - |  | 759 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  |  | SB |  |  |
| HCM Control Delay, s | 0 |  |  |  | 3.3 |  |  |  | 63.9 |  |  |
| HCM LOS |  |  |  |  |  |  |  |  | F |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | t EBL | T | R | WBL | WBT | R | BLnS | BLn2 |  |  |  |
| Capacity (veh/h) | 973 | - |  | 1204 | - | - | 80 | 697 |  |  |  |
| HCM Lane V/C Ratio | - | - |  | 0.282 | - |  | . 842 | . 158 |  |  |  |
| HCM Control Delay (s) | 0 | - | - | 9.2 |  |  | 49.9 | 11.1 |  |  |  |
| HCM Lane LOS | A | - | - | A | - | - | F | B |  |  |  |
| HCM 95th \%tile Q(veh) | 0 | - | - | 1.2 | - | - | 4.3 | 0.6 |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL WBT WBR |  |  | NBL | NBT | NBR | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 38 | 230 | 0 | 0 | 670 | 171 | 189 | 0 | 91 | 0 | 0 | 0 |
| Future Vol, veh/h | 38 | 230 | 0 | 0 | 670 | 171 | 189 | 0 | 91 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | one | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - | - | - | 0 | - | 300 | - | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 |  | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 41 | 250 | 0 | 0 | 728 | 186 | 205 | 0 | 99 | 0 | 0 | 0 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 25.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS D |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 106 | 137 | 75 | 0 | 24 | 290 | 24 | 0 | 225 | 60 | 22 |
| Future Vol, veh/h | 0 | 106 | 137 | 75 | 0 | 24 | 290 | 24 | 0 | 225 | 60 | 22 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 115 | 149 | 82 | 0 | 26 | 315 | 26 | 0 | 245 | 65 | 24 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Right |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 15.3 |  |  |  | 30.4 |  |  |  | 22.5 |  |  |
| HCM LOS |  | C |  |  |  | D |  |  |  | C |  |  |


| Lane | NBLn1 NBLn2 | NBLn3 | EBLn1 | EBLn2 | EBLn3WBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 36 | 66 | 345 |
| Future Vol, veh/h | 0 | 36 | 66 | 345 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 39 | 72 | 375 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 3 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 3 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 3 |
| HCM Control Delay | 29.9 |
| HCM LOS | D |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.2 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 2 | 124 | 12 | 108 | 177 | 10 | 3 | 0 | 117 | 21 | 1 | 6 |
| Future Vol, veh/h | 2 | 124 | 12 | 108 | 177 | 10 | 3 | 0 | 117 | 21 | 1 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | one | - |  | None | - |  | None |
| Storage Length | 200 | - | 150 | 400 | - | 150 | 200 | - | - | 200 |  |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 135 | 13 | 117 | 192 | 11 | 3 | 0 | 127 | 23 | 1 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 3 | 411 | 17 | 43 | 657 | 7 | 19 | 0 |  | 4 | 0 | 7 |
| Future Vol, veh/h | 3 | 411 | 17 | 43 | 657 | 7 | 19 | 0 |  | 4 | 0 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | ne | - |  | None |  |  | None |
| Storage Length | - | - |  | - |  | - | - | - |  |  |  |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 447 | 18 | 47 | 714 | 8 | 21 | 0 | 112 | 4 | 0 | 8 |


| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 722 | 0 | 0 | 465 | 0 | 0 |  | 1278 | 1278 | 456 | 1329 | 1283 | 718 |
| Stage 1 | - | - | - | - | - | - |  | 463 | 463 | - | 811 | 811 |  |
| Stage 2 | - | - | - | - | - | - |  | 815 | 815 | - | 518 | 472 |  |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - |  | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - |  | - |  |  | 6.12 | 5.52 |  | 6.12 | 5.52 |  |
| Critical Hdwy Stg 2 | - | - | - |  | - | - |  | 6.12 | 5.52 |  | 6.12 | 5.52 |  |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - |  | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 |
| Pot Cap-1 Maneuver | 880 | - | - | 1096 | - | - |  | 143 | 166 | 604 | 132 | 165 | 429 |
| Stage 1 | - | - | - | - | - | - |  | 579 | 564 | - | 373 | 393 |  |
| Stage 2 | - | - | - | - | - | - |  | 371 | 391 | - | 541 | 559 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 880 | - | - | 1096 | - | - |  | 132 | 153 | 604 | 101 | 152 | 429 |
| Mov Cap-2 Maneuver | - | - | - | - | - |  |  | 132 | 153 | - | 101 | 152 |  |
| Stage 1 | - | - | - | - | - | - |  | 576 | 561 |  | 371 | 365 |  |
| Stage 2 | - | - | - | - | - | - |  | 338 | 363 | - | 439 | 556 |  |
| Approach | EB |  |  | WB |  |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 0.1 |  |  | 0.5 |  |  |  | 19 |  |  | 24.5 |  |  |
| HCM LOS |  |  |  |  |  |  |  | C |  |  | C |  |  |
| Minor Lane/Major MvmNBLn1 EBL EBT EBR WBL WBT WBREBLn1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 388 | 880 | - | - 1096 | - | - | 197 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.342 | . 004 | - | -0.043 | - |  | 0.061 |  |  |  |  |  |  |
| HCM Control Delay (s) | 19 | 9.1 | 0 | - 8.4 | 0 |  | 24.5 |  |  |  |  |  |  |
| HCM Lane LOS | C | A | A | A | A |  | C |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 1.5 | 0 | - | - 0.1 | - | - | 0.2 |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 46.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS E |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 19 | 256 | 4 | 0 | 31 | 729 | 70 | 0 | 19 | 0 | 148 |
| Future Vol, veh/h | 0 | 19 | 256 | 4 | 0 | 31 | 729 | 70 | 0 | 19 | 0 | 148 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 21 | 278 | 4 | 0 | 34 | 792 | 76 | 0 | 21 | 0 | 161 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 2 |  |  |  | 1 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 2 |  |  |  | 1 |  |  |
| Conflicting Approach Right |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 2 |  |  |  | 3 |  |  |  | 2 |  |  |
| HCM Control Delay |  | 34.7 |  |  |  | 65.1 |  |  |  | 17 |  |  |

HCM LOS D F C

|  | NBLn1 | NBLn2 | EBLn1WBLn1 | Lancn | SBLn1 | SBLn2 | SBLn3 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, $\%$ | $100 \%$ | $0 \%$ | $7 \%$ | $8 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $0 \%$ | $0 \%$ | $92 \%$ | $92 \%$ | $84 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, $\%$ | $0 \%$ | $100 \%$ | $1 \%$ | $0 \%$ | $16 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 19 | 148 | 279 | 396 | 435 | 138 | 0 | 109 |
| LT Vol | 19 | 0 | 19 | 31 | 0 | 138 | 0 | 0 |
| Through Vol | 0 | 0 | 256 | 365 | 365 | 0 | 0 | 0 |
| RT Vol | 0 | 148 | 4 | 0 | 70 | 0 | 0 | 109 |
| Lane Flow Rate | 21 | 161 | 303 | 430 | 472 | 150 | 0 | 118 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.058 | 0.402 | 0.757 | 0.954 | 1 | 0.412 | 0 | 0.284 |
| Departure Headway (Hd) | 10.14 | 8.993 | 8.981 | 7.992 | 7.836 | 9.883 | 9.364 | 8.637 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 355 | 405 | 406 | 456 | 468 | 369 | 0 | 421 |
| Service Time | 7.85 | 6.651 | 6.665 | 5.69 | 5.534 | 7.498 | 6.999 | 6.3 |
| HCM Lane V/C Ratio | 0.059 | 0.398 | 0.746 | 0.943 | 1.009 | 0.407 | 0 | 0.28 |
| HCM Control Delay | 13.5 | 17.5 | 34.7 | 59.8 | 69.9 | 19.2 | 12 | 14.7 |
| HCM Lane LOS | B | C | D | F | F | C | N | B |
| HCM 95th-tile Q | 0.2 | 1.9 | 6.2 | 11.5 | 13.1 | 2 | 0 | 1.2 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 138 | 0 | 109 |
| Future Vol, veh/h | 0 | 138 | 0 | 109 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 150 | 0 | 118 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 17.2 |
| HCM LOS | C |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 58.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 0 | 267 | 174 | 443 | 684 | 0 | 0 | 0 | 0 | 79 | 0 | 119 |
| Future Vol, veh/h | 0 | 267 | 174 | 443 | 684 | 0 | 0 | 0 | 0 | 79 | 0 | 119 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | ne | - |  | None |  |  | None |
| Storage Length | - | - | - | 250 | - | - | - | - |  | 0 |  | 500 |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 |  | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 290 | 189 | 482 | 743 | 0 | 0 | 0 | 0 | 86 | 0 | 129 |


| Major/Minor | Major1 | Major2 |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 743 | 0 | 0 | 479 | 0 | 0 | 2092 | 2186 | 372 |
| Stage 1 | - | - | - | - | - | - | 1707 | 1707 |  |
| Stage 2 | - | - | - | - | - | - | 385 | 479 |  |
| Critical Hdwy | 4.14 | - | - | 4.12 | - | - | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - | 2.218 | - | - | 3.519 | . 019 | . 319 |
| Pot Cap-1 Maneuver | 860 | - | - | 1083 | - | - | - 51 | 45 | 626 |
| Stage 1 | - | - | - | - | - | - | 133 | 146 |  |
| Stage 2 | - | - | - | - | - | - | 687 | 554 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 860 | - | - | 1083 | - | - | - 28 | 0 | 626 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | $\sim 28$ | 0 |  |
| Stage 1 | - | - | - | - | - | - | - 74 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 687 | 0 |  |


| Approach | EB | WB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 4.3 | $\$ 496.5$ |
| HCM LOS |  | $F$ |  |

Minor Lane/Major Mvmt EBL EBT EBR WBL WBT WBFBBLnISBLn2

| Capacity (veh/h) | 860 | - | -1083 | - | - | 28 |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: |
| 626 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | - | - | -0.445 | - | -3.0670 .207 |  |
| HCM Control Delay (s) | 0 | - | - | 11 | - | $\$ 1226$ |
| HCM Lane LOS | A | - | - | B | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | F | B |  |
| H |  | - | -10.3 | 0.8 |  |  |

Notes
~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 20.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 50 | 307 | 0 | 0 | 848 | 238 | 273 | 0 | 136 | 0 | 0 | 0 |
| Future Vol, veh/h | 50 | 307 | 0 | 0 | 848 | 238 | 273 | 0 | 136 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - | - | - | 0 | - | 300 | - | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 54 | 334 | 0 | 0 | 922 | 259 | 297 | 0 | 148 | 0 | 0 |  |



Notes
$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 57.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS F |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 143 | 177 | 101 | 0 | 34 | 366 | 34 | 0 | 360 | 100 | 36 |
| Future Vol, veh/h | 0 | 143 | 177 | 101 | 0 | 34 | 366 | 34 | 0 | 360 | 100 | 36 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 155 | 192 | 110 | 0 | 37 | 398 | 37 | 0 | 391 | 109 | 39 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Righ |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 24 |  |  |  | 72.1 |  |  |  | 65.6 |  |  |
| HCM LOS |  | C |  |  |  | F |  |  |  | F |  |  |


| Lane | NBLn1 | NBLn2 | NBLn3 | BLn1 | EBLn2 | EBLn | VBLn | VBLn | VBLn | SBLn1 | SBLn2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vol Left, \% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% |
| Vol Thru, \% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% |
| Vol Right, \% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% | 100\% | 0\% | 0\% |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 360 | 100 | 36 | 143 | 177 | 101 | 34 | 366 | 34 | 54 | 100 |
| LT Vol | 360 | 0 | 0 | 143 | 0 | 0 | 34 | 0 | 0 | 54 | 0 |
| Through Vol | 0 | 100 | 0 | 0 | 177 | 0 | 0 | 366 | 0 | 0 | 100 |
| RT Vol | 0 | 0 | 36 | 0 | 0 | 101 | 0 | 0 | 34 | 0 | 0 |
| Lane Flow Rate | 391 | 109 | 39 | 155 | 192 | 110 | 37 | 398 | 37 | 59 | 109 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 1 | 0.316 | 0.107 | 0.488 | 0.578 | 0.309 | 0.114 | 1 | 0.102 | 0.178 | 0.315 |
| Departure Headway (Hd) | 10.965 | 10.479 | 9.798 | 11.306 | 10.816 | 10.129 | 11.144 | 10.657 | 9.977 | 10.904 | 10.418 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 333 | 345 | 367 | 320 | 335 | 356 | 323 | 342 | 360 | 330 | 346 |
| Service Time | 8.696 | 8.21 | 7.53 | 9.031 | 8.541 | 7.854 | 8.88 | 8.394 | 7.713 | 8.635 | 8.149 |
| HCM Lane V/C Ratio | 1.174 | 0.316 | 0.106 | 0.484 | 0.573 | 0.309 | 0.115 | 1.164 | 0.103 | 0.179 | 0.315 |
| HCM Control Delay | 84 | 18 | 13.7 | 24.4 | 27.4 | 17.3 | 15.3 | 82.8 | 13.8 | 16 | 17.9 |
| HCM Lane LOS | F | C | B | C | D | C | C | F | B | C | C |
| HCM 95th-tile Q | 11.1 | 1.3 | 0.4 | 2.5 | 3.4 | 1.3 | 0.4 | 11.2 | 0.3 | 0.6 | 1.3 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 54 | 100 | 506 |
| Future Vol, veh/h | 0 | 54 | 100 | 506 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 59 | 109 | 550 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |  |
| :--- | ---: | :--- |
| Approach | NB |  |
| Opposing Approach | 3 |  |
| Opposing Lanes | WB |  |
| Conflicting Approach Left | 3 |  |
| Conflicting Lanes Left | EB |  |
| Conflicting Approach Right | 3 |  |
| Conflicting Lanes Right | 64.4 |  |
| HCM Control Delay | F |  |
| HCM LOS |  |  |
|  |  |  |
| Lane |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT |  | EBR | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 2 | 135 | 12 | 150 | 223 | 10 | 3 | 0 | 128 | 21 | 1 | 6 |
| Future Vol, veh/h | 2 | 135 | 12 | 150 | 223 | 10 | 3 | 0 | 128 | 21 | 1 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | one | - |  | None | - |  | None |
| Storage Length | 200 | - | 150 | 400 | - | 150 | 200 | - | - | 200 | - |  |
| Veh in Median Storage, \# | - | 0 |  |  | 0 | - | - | 0 |  | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 147 | 13 | 163 | 242 | 11 | 3 | 0 | 139 | 23 | 1 | 7 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 3 | 432 | 17 | 43 | 743 | 7 | 19 | 0 |  | 4 | 0 |  |
| Future Vol, veh/h | 3 | 432 | 17 | 43 | 743 | 7 | 19 | 0 | 103 | 4 | 0 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free |  | Free | Free |  | Stop | Stop |  | Stop | Stop |  |
| RT Channelized | - |  | None | - |  |  | - |  | None |  |  | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - |  |  |
| Veh in Median Storage, \# | - | 0 | - |  | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 470 | 18 | 47 | 808 | 8 | 21 | 0 | 112 | 4 | 0 |  |




| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Traffic Vol, veh/h | 0 | 20 | 275 | 5 | 0 | 31 | 806 | 70 | 0 | 24 | 0 | 148 |
| Future Vol, veh/h | 0 | 20 | 275 | 5 | 0 | 31 | 806 | 70 | 0 | 24 | 0 | 148 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 22 | 299 | 5 | 0 | 34 | 876 | 76 | 0 | 26 | 0 | 161 |
| Number of Lanes | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 1 | 0 |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Opposing Approach | WB | EB | SB |
| Opposing Lanes | 2 | 1 | 3 |
| Conflicting Approach Left | SB | NB | EB |
| Conflicting Lanes Left | 3 | 2 | 1 |
| Conflicting Approach Right | NB | SB | WB |
| Conflicting Lanes Right | 2 | 3 | 2 |
| HCM Control Delay | 41.3 | 71 | 17.3 |
| HCM LOS | E | F | C |


| Lane | NBLn1 | NBLn2 | EBLn1WBLn1WBLn2 | SBLn1 | SBLn2 | SBLn3 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $100 \%$ | $0 \%$ | $7 \%$ | $7 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $0 \%$ |
| Vol Thru, \% | $0 \%$ | $0 \%$ | $92 \%$ | $93 \%$ | $85 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $2 \%$ | $0 \%$ | $15 \%$ | $0 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 24 | 148 | 300 | 434 | 473 | 138 | 0 | 113 |
| LT Vol | 24 | 0 | 20 | 31 | 0 | 138 | 0 | 0 |
| Through Vol | 0 | 0 | 275 | 403 | 403 | 0 | 0 | 0 |
| RT Vol | 0 | 148 | 5 | 0 | 70 | 0 | 0 | 113 |
| Lane Flow Rate | 26 | 161 | 326 | 472 | 514 | 150 | 0 | 123 |
| Geometry Grp | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| Degree of Util (X) | 0.074 | 0.405 | 0.816 | 1 | 1 | 0.414 | 0 | 0.298 |
| Departure Headway (Hd) | 10.268 | 9.068 | 9.007 | 8.066 | 7.923 | 9.925 | 9.425 | 8.725 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 349 | 397 | 401 | 448 | 458 | 363 | 0 | 411 |
| Service Time | 8.027 | 6.828 | 6.757 | 5.844 | 5.701 | 7.678 | 7.178 | 6.479 |
| HCM Lane V/C Ratio | 0.074 | 0.406 | 0.813 | 1.054 | 1.122 | 0.413 | 0 | 0.299 |
| HCM Control Delay | 13.9 | 17.9 | 41.3 | 71.4 | 70.7 | 19.5 | 12.2 | 15.2 |
| HCM Lane LOS | B | C | E | F | F | C | N | C |
| HCM 95th-tile Q | 0.2 | 1.9 | 7.4 | 12.9 | 13 | 2 | 0 | 1.2 |


| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 138 | 0 | 113 |
| Future Vol, veh/h | 0 | 138 | 0 | 113 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 150 | 0 | 123 |
| Number of Lanes | 0 | 1 | 1 | 1 |


| Approach | SB |
| :--- | ---: |
| Opposing Approach | NB |
| Opposing Lanes | 2 |
| Conflicting Approach Left | WB |
| Conflicting Lanes Left | 2 |
| Conflicting Approach Right | EB |
| Conflicting Lanes Right | 1 |
| HCM Control Delay | 17.6 |
| HCM LOS | C |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 67 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 0 | 284 |  | 443 | 754 | 0 | 0 | 0 | 0 | 79 | 0 | 126 |
| Future Vol, veh/h | 0 | 284 | 176 | 443 | 754 | 0 | 0 | 0 | 0 | 79 | 0 | 126 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | ree | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  |  | - |  | None | - |  | None |
| Storage Length | - | - |  | 250 | - | - |  |  | - | 0 | - | 500 |
| Veh in Median Storage, \# |  | 0 |  | - | 0 | - |  | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 309 | 191 | 482 | 820 | 0 | 0 | 0 | 0 | 86 | 0 |  |


| Major/Minor | Major1 | Major2 |  |  |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 820 | 0 | 0 | 500 | 0 | 0 | 2187 | 2283 | 410 |
| Stage 1 | - | - | - | - | - | - | 1783 | 1783 |  |
| Stage 2 | - | - | - | - | - | - | 404 | 500 |  |
| Critical Hdwy | 4.14 | - | - | 4.12 | - | - | 6.63 | 6.53 | 6.93 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.83 | 5.53 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.43 | 5.53 |  |
| Follow-up Hdwy | 2.22 | - | - | 2.218 | - | - | 3.519 | . 019 | . 319 |
| Pot Cap-1 Maneuver | 805 | - | - | 1064 | - | - | -44 | 39 | 592 |
| Stage 1 | - | - | - | - | - | - | 120 | 133 |  |
| Stage 2 | - | - | - | - | - | - | 673 | 542 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 805 | - | - | 1064 | - | - | - 24 | 0 | 592 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | $\sim 24$ | 0 |  |
| Stage 1 | - | - | - | - | - | - | -66 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 673 | 0 |  |


|  | EB | WB | SB |
| :--- | :---: | :---: | ---: |
| Approach $C o n t r o l ~ D e l a y, ~ s ~$ | 0 | 4.1 | \$584.2 |
| HCM LOS |  |  | F |

Minor Lane/Major Mvmt EBL EBT EBR WBL WBT WBFBBLnisBLn2

| Capacity (veh/h) | 805 | - | -1064 | - | - | 24 |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: |
| 592 |  |  |  |  |  |  |
| HCM Lane V/C Ratio | - | - | -0.453 | - | -3.5780 .231 |  |
| HCM Control Delay (s) | 0 | - | -11.1 | - | $\$ 1495.3$ | 12.9 |
| HCM Lane LOS | A | - | - | B | - | - |
| HCM | B |  |  |  |  |  |
| 95th \%tile Q(veh) | 0 | - | - | 2.4 | - | -10.7 |

Notes
~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 27.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL | NBT NBR |  | SBL | SBT SBR |  |
| Traffic Vol, veh/h | 53 | 321 | 0 | 0 | 906 | 238 | 280 | 0 | 136 | 0 | 0 | 0 |
| Future Vol, veh/h | 53 | 321 | 0 | 0 | 906 | 238 | 280 | 0 | 136 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - |  | None | - |  | None | - |  | None | - |  | None |
| Storage Length | 100 | - | - | - | - | - | 0 | - | 300 | - | - |  |
| Veh in Median Storage, \# | - | 0 |  | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 58 | 349 | 0 | 0 | 985 | 259 | 304 | 0 | 148 | 0 | 0 |  |



Notes
~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh 58.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS F |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
| Traffic Vol, veh/h | 0 | 146 | 186 | 103 | 0 | 34 | 400 | 34 | 0 | 369 | 100 | 36 |
| Future Vol, veh/h | 0 | 146 | 186 | 103 | 0 | 34 | 400 | 34 | 0 | 369 | 100 | 36 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 159 | 202 | 112 | 0 | 37 | 435 | 37 | 0 | 401 | 109 | 39 |
| Number of Lanes | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 |
| Approach EB WB NB |  |  |  |  |  |  |  |  |  |  |  |  |
| Opposing Approach |  | WB |  |  |  | EB |  |  |  | SB |  |  |
| Opposing Lanes |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Left |  | SB |  |  |  | NB |  |  |  | EB |  |  |
| Conflicting Lanes Left |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| Conflicting Approach Righ |  | NB |  |  |  | SB |  |  |  | WB |  |  |
| Conflicting Lanes Right |  | 3 |  |  |  | 3 |  |  |  | 3 |  |  |
| HCM Control Delay |  | 24.6 |  |  |  | 73 |  |  |  | 66.1 |  |  |
| HCM LOS |  | C |  |  |  | F |  |  |  | F |  |  |



| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh |  |  |  |  |
| Intersection LOS |  |  |  |  |
| Movement | SBU | SBL | SBT | SBR |
| Traffic Vol, veh/h | 0 | 54 | 100 | 520 |
| Future Vol, veh/h | 0 | 54 | 100 | 520 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 59 | 109 | 565 |
| Number of Lanes | 0 | 1 | 1 | 1 |


|  | SB |
| :--- | ---: |
| Approach | NB |
| Opposing Approach | 3 |
| Opposing Lanes | WB |
| Conflicting Approach Left | 3 |
| Conflictin Lanes Left | EB |
| Conflictin Approach Right | 3 |
| Conflicting Lanes Right | 64.9 |
| HCM Control Delay | F |
| HCM LOS |  |
|  |  |
| Lane |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT EBR |  |  | WBL WBT WBR |  |  | NBL NBT NBR |  |  | SBL SBT SBR |  |  |
| Traffic Vol, veh/h | 2 | 135 | 12 | 150 | 223 | 10 | 3 | 0 |  | 21 | 1 | 6 |
| Future Vol, veh/h | 2 | 135 | 12 | 150 | 223 | 10 | 3 | 0 | 128 | 21 | 1 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free |  | Free | Free | Free | Stop | Stop |  | Stop | Stop |  |
| RT Channelized | - |  | None | - |  | one | - |  | None | - |  | None |
| Storage Length | 200 | - | 150 | 400 | - | 150 | 200 | - | - | 200 | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 147 | 13 | 163 | 242 | 11 | 3 | 0 | 139 | 23 | 1 |  |


| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 242 | 0 | 0 | 147 | 0 | 0 | 723 | 719 | 147 | 789 | 719 | 242 |
| Stage 1 | - | - | - | - | - | - | 151 | 151 | - | 568 | 568 |  |
| Stage 2 | - | - | - | - | - | - | 572 | 568 | - | 221 | 151 | - |
| Critical Hdwy | 4.12 | - | - | 4.12 | - |  | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | - |  | 6.12 | 5.52 |  | 6.12 | 5.52 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - |  | 6.12 | 5.52 |  | 6.12 | 5.52 |  |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - | 3.518 | . 018 | . 318 | 3.518 | . 018 | . 318 |
| Pot Cap-1 Maneuver | 1324 | - | - | 1435 | - | - | 342 | 354 | 900 | 308 | 354 | 797 |
| Stage 1 | - | - | - | - | - | - | 851 | 772 | - | 508 | 506 |  |
| Stage 2 | - | - | - | - | - |  | 505 | 506 | - | 781 | 772 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1324 | - | - | 1435 | - | - | 309 | 313 | 900 | 237 | 313 | 797 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 309 | 313 | - | 237 | 313 |  |
| Stage 1 | - | - | - | - | - | - | 850 | 771 | - | 507 | 449 | - |
| Stage 2 | - | - | - | - | - | - | 443 | 449 | - | 659 | 771 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.1 | 3.1 | 9.9 |
| HCM LOS |  | A | 19 |
|  |  |  | C |

Minor Lane/Major MvmNBLnNBLn2 EBL EBT EBR WBL WBT WBFBBLnISBLn2

| Capacity (veh/h) | 309 | 900 | 1324 | - | -1435 | - | -237 | 653 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- | ---: | ---: | ---: |
| HCM Lane V/C Ratio | 0.011 | 0.155 | 0.002 | - | -0.114 | - | -0.096 | 0.012 |  |
| HCM Control Delay (s) | 16.8 | 9.7 | 7.7 | - | - | 7.8 | - | -21.8 | 10.6 |
| HCM Lane LOS | C | A | A | - | - | A | - | - | C | B


|  | 4 |  |  |  |  |  | 4 | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Volume (veh/h) | 3 | 432 | 17 | 43 | 743 | 7 | 19 | 0 | 103 | 4 | 0 | 7 |
| Future Volume (veh/h) | 3 | 432 | 17 | 43 | 743 | 7 | 19 | 0 | 103 | 4 | 0 | 7 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1750 | 1863 | 1750 | 1750 | 1863 | 1750 | 1750 | 1863 | 1750 | 1750 | 1863 | 1750 |
| Adj Flow Rate, veh/h | 3 | 470 | 18 | 47 | 808 | 8 | 21 | 0 | 112 | 4 | 0 | 8 |
| Adj No. of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | , | 2 | 2 | 2 |
| Cap, veh/h | 41 | 919 | 35 | 75 | 885 | 9 | 115 | 29 | 522 | 226 | 25 | 394 |
| Arrive On Green | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.39 | 0.00 | 0.39 | 0.39 | 0.00 | 0.39 |
| Sat Flow, veh/h | 2 | 1779 | 68 | 63 | 1714 | 17 | 175 | 73 | 1323 | 437 | 63 | 998 |
| Grp Volume(v), veh/h | 491 | 0 | 0 | 863 | 0 | 0 | 133 | 0 | 0 | 12 | 0 | 0 |
| Grp Sat Flow(s), veh/h/ln | 1849 | 0 | 0 | 1793 | 0 | 0 | 1572 | 0 | 0 | 1497 | 0 | 0 |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.0 | 24.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 15.7 | 0.0 | 0.0 | 40.1 | 0.0 | 0.0 | 4.9 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |
| Prop In Lane | 0.01 |  | 0.04 | 0.05 |  | 0.01 | 0.16 |  | 0.84 | 0.33 |  | 0.67 |
| Lane Grp Cap(c), veh/h | 995 | 0 | 0 | 968 | 0 | 0 | 666 | 0 | 0 | 644 | 0 | 0 |
| V/C Ratio(X) | 0.49 | 0.00 | 0.00 | 0.89 | 0.00 | 0.00 | 0.20 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 1107 | 0 | 0 | 1076 | 0 | 0 | 666 | 0 | 0 | 644 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 14.3 | 0.0 | 0.0 | 20.0 | 0.0 | 0.0 | 18.0 | 0.0 | 0.0 | 16.6 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.4 | 0.0 | 0.0 | 8.9 | 0.0 | 0.0 | 0.7 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ | In 8.0 | 0.0 | 0.0 | 22.0 | 0.0 | 0.0 | 2.3 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 |
| LnGrp Delay(d),s/veh | 14.7 | 0.0 | 0.0 | 28.8 | 0.0 | 0.0 | 18.6 | 0.0 | 0.0 | 16.7 | 0.0 | 0.0 |
| LnGrp LOS | B |  |  | C |  |  | B |  |  | B |  |  |
| Approach Vol, veh/h |  | 491 |  |  | 863 |  |  | 133 |  |  | 12 |  |
| Approach Delay, s/veh |  | 14.7 |  |  | 28.8 |  |  | 18.6 |  |  | 16.7 |  |
| Approach LOS |  | B |  |  | C |  |  | B |  |  | B |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs |  | 2 |  | 4 |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), |  | 39.5 |  | 50.5 |  | 39.5 |  | 50.5 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | 4.0 |  | 4.0 |  | 4.0 |  | 4.0 |  |  |  |  |
| Max Green Setting (Gmax | x), s | 30.0 |  | 52.0 |  | 30.0 |  | 52.0 |  |  |  |  |
| Max Q Clear Time (g_c+1) | 1), s | 6.9 |  | 17.7 |  | 2.4 |  | 42.1 |  |  |  |  |
| Green Ext Time (p_c), s |  | 0.5 |  | 6.9 |  | 0.5 |  | 4.4 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl DelayHCM 2010 LOS |  |  | 23.2 |  |  |  |  |  |  |  |  |  |
|  |  |  | C |  |  |  |  |  |  |  |  |  |





|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

## HCS ANALYSIS

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $282 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $531 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 | 1.1 |  |  |
| PCE for RVs, ER |  | 1.0 | 1.0 |  |
|  |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.977 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate,(note-2) vi | 314 | pc/h | 581 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.1 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | 50.0 | $\mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $86.2 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.18 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
306.5

Effective speed factor, St
24.00

Bicycle LOS Score, BLOS
4.79

Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | ss 2 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $208 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $515 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.1 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | 50.7 | $\mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $87.5 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | A |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.13 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  |  | veh/h |
| Directional Capacity | 1700 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $50.7 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
A
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl A
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
226.1
24.00
4.79
3.25

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $208 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $512 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.1 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $50.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $87.5 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.14 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
226.1
24.00
4.79
3.23

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: AM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR $41 \mathrm{NB} / \mathrm{N} 191 / 2$ Ave |
| Jurisdiction: | Kings County |
| Analysis Year: | 2020 |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC 0.0 mph 0.0 mph
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 155 | pcphpl | 402 |  |  |$\quad$ pcphpl

## Direction 1 2

Flow rate, vp 155 pcphpl 402 pcphpl
Free-flow speed, FFS $55.0 \quad \mathrm{mph} 55.0 \mathrm{mph}$

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

$\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 152.2 | 392.4 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.72 | 3.20 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: AM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: 2020 |  |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  |
| :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |
| Trucks and buses PCE, ET | 1.5 | 1.5 |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |
| Flow rate, vp 128 | pcphpl | 405 pcphpl |
| RESULTS |  |  |


|  | Direction | 1 | 2 |  |
| :--- | :--- | :--- | :--- | :--- |
| Flow rate, vp | 128 | pcphpl | 405 | pcphpl |
| Free-flow speed, FFS |  | 55.0 | mph | 55.0 | mph

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$
Level of service, LOS A A
Density, D $2.3 \quad \mathrm{pc} / \mathrm{mi} / \ln 7.4 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
Bicycle Level of Service $\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 125.0 | 395.7 |
| Effective width of outside lane | ne, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.62 | 3.20 |
| Bicycle LOS C | C | C |

Overall results are not computed when free-flow speed is less than 45 mph .

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 531 veh/h
Opposing direction volume, Vo $282 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.4 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.994 | 0.977 |  |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate,(note-2) vi | 581 | $\mathrm{pc} / \mathrm{h}$ | 314 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.5 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.4 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.34 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
577.2
24.00
4.79
3.71

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | ss 2 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $515 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $208 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.5 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.994 |  | 0.971 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 563 | $\mathrm{pc} / \mathrm{h}$ | 233 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
|  |  |  |
| Adjustment for no-passing zones, fnp | $1.7 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | 50.1 | $\mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $86.5 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.33 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS | 0 | veh/h |  |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $50.1 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl A
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
559.8
24.00
4.79
3.69

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $512 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $208 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.7 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $50.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $86.5 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.33 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1651 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1651 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
556.5
24.00
4.79

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 301 veh/h
Opposing direction volume, Vo $608 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.977 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 335 | pc/h | 665 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \mathrm{mi} / \mathrm{h}$

Adjustment for no-passing zones, fnp
Average travel speed, ATSd
Percent Free Flow Speed, PFFS
$0.9 \mathrm{mi} / \mathrm{h}$
$49.4 \mathrm{mi} / \mathrm{h}$
85.1 \%

Percent Time-Spent-Following


Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.20 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, Lt 0.0 mi
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $49.4 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
B

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 229 veh/h
Opposing direction volume, Vo $601 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |
| :--- | :---: |
| Adjustment for no-passing zones, fnp | $0.9 \mathrm{mi} / \mathrm{h}$ |
| Average travel speed, ATSd | $50.0 \mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | 86.3 m |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.15 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |


| Passing Lane Analysis |
| :---: |
| Total length of analysis segment, Lt 0.0 mi |
| Length of two-lane highway upstream of the passing lane, Lu - mi |
| Length of passing lane including tapers, Lpl - mi |
| Average travel speed, ATSd (from above) $\quad 50.0 \mathrm{mi} / \mathrm{h}$ |
| Percent time-spent-following, PTSFd (from above) 39.8 |
| Level of service, LOSd (from above) B |
| Average Travel Speed with Passing Lane |
| Downstream length of two-lane highway within effective length of passing lane for average travel speed, Lde - mi |
| Length of two-lane highway downstream of effective length of the passing lane for average travel speed, Ld - mi |
| Adj. factor for the effect of passing lane on average speed, fpl |
| Average travel speed including passing lane, ATSpl |
| Percent free flow speed including passing lane, PFFSpl 0.0 \% |

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
4.79
3.28

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 229 veh/h
Opposing direction volume, Vo $598 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.5 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) fHV | 0.971 |  | 0.994 |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 256 | $\mathrm{pc} / \mathrm{h}$ | 654 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |
| :--- | :---: |
| Adjustment for no-passing zones, fnp | $0.9 \mathrm{mi} / \mathrm{h}$ |
| Average travel speed, ATSd | $50.0 \mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | 86.3 m |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.15 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
4.79

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: | R\&S Civil |
| Date: | 12/18/2020 |
| Analysis Period: AM |  |
| Highway: | Bush Street |
| From/To: | SR 41 NB/N 19 1/2 Ave |
| Jurisdiction: | Kings County |
| Analysis Year: 2020+Project <br> Project ID: Community College Expansion |  |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph

| Number of lanes | 2 |  | 2 |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 163 | pcphpl | 433 |  |  |$\quad$| pcphpl |  |  |
| :--- | :--- | :--- |
|  |  |  |
|  |  |  |
|  |  | RESULTS |

## Direction 1 2

Flow rate, vp 163 pcphpl 433 pcphpl
Free-flow speed, FFS 55.0 mph 55.0 mph

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

| Level of service, LOS | A |  |  |  | A <br> Density, D | 3.0 | $\mathrm{pc} / \mathrm{mi} / \mathrm{ln} 7.9$ | $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: |

$\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 159.8 | 423.4 |
| Effective width of outside lane | ne, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.75 | 3.24 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: | R\&S Civil |
| Date: | 12/18/2020 |
| Analysis Period: AM |  |
| Highway: | Bush Street |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: | 2020+Project |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  |
| :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |
| Trucks and buses PCE, ET | 1.5 | 1.5 |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |
| Flow rate, vp 137 | pcphpl | 444 pcphpl |
|  |  | RESULTS |

## Direction 1 2

Flow rate, vp 137 pcphpl 444 pcphpl
Free-flow speed, FFS $55.0 \quad \mathrm{mph} 55.0 \mathrm{mph}$

Avg. passenger-car travel speed, S $55.0 \mathrm{mph} \quad 55.0 \mathrm{mph}$
Level of service, LOS A

Density, D $2.5 \quad \mathrm{pc} / \mathrm{mi} / \ln 8.1 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
$\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 134.2 | 433.7 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.66 | 3.25 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

Phone:
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E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highway c | $s 3$ |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment lengt | 0.0 | mi | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles | S | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 | \% |
| Up/down |  |  | Access point density |  | mi |

Analysis direction volume, Vd $608 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $301 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $48.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $84.1 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.39 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
660.9

Effective speed factor, St
Bicycle LOS Score, BLOS
4.79

Bicycle LOS
D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $601 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $229 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.5 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.994 |  | 0.971 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 657 | $\mathrm{pc} / \mathrm{h}$ | 256 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.3 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.0 \%$ |  |


| Percent Time-Spent-Following__ |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Direction | Analysis(d) | Opposing (o) |  |  |
| PCE for trucks, ET | 1.0 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 1.000 | 0.994 |  |  |
| Grade adjustment factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 653 | $\mathrm{pc} / \mathrm{h}$ | 250 | $\mathrm{pc} / \mathrm{h}$ |
| Base percent time-spent-following,(note-4) | BPTSFd | 55.6 | $\%$ |  |
| Adjustment for no-passing zones, fnp | 20.9 |  |  |  |
| Percent time-spent-following, PTSFd | 70.7 | $\%$ |  |  |

Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.39 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
653.3
24.00
4.79

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 598 veh/h
Opposing direction volume, Vo $229 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.3 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.0 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.38 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
650.0
24.00
4.79

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $308 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $576 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.977 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate,(note-2) vi | 343 | pc/h | 630 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.0 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.5 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.3 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.20 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
334.8

Effective speed factor, St
24.00

Bicycle LOS Score, BLOS
4.79

Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 304 veh/h
Opposing direction volume, Vo $538 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.0 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.8 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.20 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P 3
Flow rate in outside lane, vOL
Effective width of outside lane, We 330.4

Effective speed factor, St
Bicycle LOS Score, BLOS
4.79

Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $221 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $567 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.0 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $50.3 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | 86.7 m |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.15 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We 240.2

Effective speed factor, St
4.79

Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: AM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR $41 \mathrm{NB} / \mathrm{N} 191 / 2$ Ave |
| Jurisdiction: | Kings County |
| Analysis Year: | 2024 |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC 0.0 mph 0.0 mph
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 169 | pcphpl | 447 |  |  |
|  |  |  | pcphpl |  |  |
|  |  |  | RESULTS |  |  |

## Direction 1 2

Flow rate, vp 169 pcphpl 447 pcphpl
Free-flow speed, FFS $55.0 \quad \mathrm{mph} 55.0 \mathrm{mph}$

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

Level of service, LOS
Density, D

A
$3.1 \quad \mathrm{pc} / \mathrm{mi} / \ln 8.1 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
Bicycle Level of Service $\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 165.2 | 436.4 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.76 | 3.25 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: AM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: 2024 |  |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  |
| :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |
| Trucks and buses PCE, ET | 1.5 | 1.5 |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |
| Flow rate, vp 139 | pcphpl | 442 pcphpl |
|  |  | RESULTS |


| Direction | 1 | 2 |  |  |
| :--- | :--- | :--- | :---: | :---: |
| Flow rate, vp | 139 | pcphpl |  |  | 442 | pcphpl |
| :---: |
| Free-flow speed, FFS |

Avg. passenger-car travel speed, S $55.0 \mathrm{mph} \quad 55.0 \mathrm{mph}$
Level of service, LOS A

Density, D $\quad 2.5 \quad \mathrm{pc} / \mathrm{mi} / \ln 8.0 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 136.4 | 431.5 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.66 | 3.25 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 576 veh/h
Opposing direction volume, Vo $308 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.4 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.994 |  | 0.977 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 630 | $\mathrm{pc} / \mathrm{h}$ | 343 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 |  |
| :--- | :---: | :---: |
| $\mathrm{mi} / \mathrm{h}$ |  |  |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.0 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $84.5 \%$ |  |


| Percent Time-Spent-Following__ |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Direction | Analysis(d) | Opposing (o) |  |  |
| PCE for trucks, ET | 1.0 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 1.000 | 0.994 |  |  |
| Grade adjustment factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 626 | $\mathrm{pc} / \mathrm{h}$ | 337 | $\mathrm{pc} / \mathrm{h}$ |
| Base percent time-spent-following,(note-4) | BPTSFd | 55.2 | $\%$ |  |
| Adjustment for no-passing zones, fnp | 23.3 |  |  |  |
| Percent time-spent-following, PTSFd | 70.3 | $\%$ |  |  |

Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.37 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
626.1
24.00
4.79
3.75

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highway c | $s 3$ |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment lengt | 0.0 | mi | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles | S | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 | \% |
| Up/down |  |  | Access point density |  | mi |

Analysis direction volume, Vd 538 veh/h
Opposing direction volume, Vo $304 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.3 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.1 \%$ |  |


| Percent Time-Spent-Following__ |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Direction | Analysis(d) | Opposing (o) |  |  |
| PCE for trucks, ET | 1.0 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 1.000 | 0.994 |  |  |
| Grade adjustment factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 585 | $\mathrm{pc} / \mathrm{h}$ | 332 | $\mathrm{pc} / \mathrm{h}$ |
| Base percent time-spent-following,(note-4) | BPTSFd | 53.2 | $\%$ |  |
| Adjustment for no-passing zones, fnp | 24.6 |  |  |  |
| Percent time-spent-following, PTSFd | 68.9 | $\%$ |  |  |

Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.35 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
584.8
24.00
4.79

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $567 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $221 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.5 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) fHV | 0.994 |  | 0.971 |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 620 | $\mathrm{pc} / \mathrm{h}$ | 247 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \quad \mathrm{mi} / \mathrm{h}$

Adjustment for no-passing zones, fnp
Average travel speed, ATSd
Percent Free Flow Speed, PFFS
$1.7 \mathrm{mi} / \mathrm{h}$
$49.6 \mathrm{mi} / \mathrm{h}$
85.6 \%

Percent Time-Spent-Following $\qquad$

| Direction | Analysis(d) |  | Opposing (o) |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.0 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 1.000 |  | 0.994 |  |
| Grade adjustment factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 616 | $\mathrm{pc} / \mathrm{h}$ | 242 | $\mathrm{pc} / \mathrm{h}$ |
| Base percent time-spent-following,(note-4) | BPTSFd | 53.8 | $\%$ |  |
| Adjustment for no-passing zones, fnp | 21.7 |  |  |  |
| Percent time-spent-following, PTSFd | 69.4 | $\%$ |  |  |

Level of Service and Other Performance Measures $\qquad$


Passing Lane Analysis $\qquad$
Total length of analysis segment, Lt 0.0 mi
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $49.6 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
B
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 327 veh/h
Opposing direction volume, Vo $653 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.3 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.982 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 362 | pc/h | 714 | pc/h |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \quad \mathrm{mi} / \mathrm{h}$

Adjustment for no-passing zones, fnp
Average travel speed, ATSd
Percent Free Flow Speed, PFFS
$0.8 \mathrm{mi} / \mathrm{h}$
$48.9 \mathrm{mi} / \mathrm{h}$
84.3 \%

Percent Time-Spent-Following


Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.21 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $48.9 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
B
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
355.4
24.00
4.79
3.46

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highway c | $s 3$ |  | Peak hour factor, P | 0.88 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment lengt | 0.0 | m | Truck crawl speed | 0. |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 | \% |
| Up/down |  |  | Access point density |  | mi |

Analysis direction volume, Vd 279 veh/h
Opposing direction volume, Vo $653 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \quad \mathrm{mi} / \mathrm{h}$

Adjustment for no-passing zones, fnp
Average travel speed, ATSd
Percent Free Flow Speed, PFFS
$0.7 \mathrm{mi} / \mathrm{h}$
$49.0 \mathrm{mi} / \mathrm{h}$
84.5 \%

Percent Time-Spent-Following

| Percent |  |  |  | Time-Spent-Following___ |
| :--- | :---: | :---: | :---: | :--- |
|  |  |  |  |  |
| Direction | Analysis(d) | Opposing (o) |  |  |
| PCE for trucks, ET | 1.1 | 1.0 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 0.994 | 1.000 |  |  |
| Grade adjustment factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 319 | $\mathrm{pc} / \mathrm{h}$ | 742 | $\mathrm{pc} / \mathrm{h}$ |
| Base percent time-spent-following,(note-4) | BPTSFd | 42.0 | $\%$ |  |
| Adjustment for no-passing zones, fnp | 19.7 |  |  |  |
| Percent time-spent-following, PTSFd | 47.9 | $\%$ |  |  |

Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.19 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $49.0 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
B
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
317.0
24.00
4.79
3.40

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $242 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $653 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.977 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate,(note-2) vi | 269 | pc/h | 714 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \mathrm{mi} / \mathrm{h}$

| Adjustment for no-passing zones, fnp | $0.8 \mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Average travel speed, ATSd | $49.6 \mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $85.5 \%$ |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.16 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
263.0
4.79
3.31

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: | R\&S Civil |
| Date: | 12/18/2020 |
| Analysis Period: AM |  |
| Highway: | Bush Street |
| From/To: | SR 41 NB/N 19 1/2 Ave |
| Jurisdiction: | Kings County |
| Analysis Year: 2024+Project <br> Project ID: Community College Expansion |  |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes 2 | 2 |  |
| :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |
| Trucks and buses PCE, ET | 1.5 | 1.5 |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |
| Flow rate, vp 177 | pcphpl | 479 pcphpl |
|  |  | RESULTS |


|  | Direction | 1 | 2 |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Flow rate, vp | 177 | pcphpl | 479 |  |  | pcphpl

Avg. passenger-car travel speed, S $55.0 \mathrm{mph} \quad 55.0 \mathrm{mph}$

| Level of service, LOS |  |  |  |
| :--- | :--- | ---: | :--- |
| A |  |  |  |
| Density, D | 3.2 | $\mathrm{pc} / \mathrm{mi} / \ln 8.7$ | $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |

$\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 172.8 | 467.4 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.79 | 3.29 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: | R\&S Civil |
| Date: | 12/18/2020 |
| Analysis Period: AM |  |
| Highway: | Bush Street |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: | 2024+Project |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 149 | pcphpl | 481 |  |  |
|  |  |  | pcphpl |  |  |
|  |  |  | RESULTS |  |  |

## Direction $1 \quad 2$

Flow rate, vp 149 pcphpl 481 pcphpl
Free-flow speed, FFS $55.0 \quad \mathrm{mph} 55.0 \mathrm{mph}$

Avg. passenger-car travel speed, S $55.0 \mathrm{mph} \quad 55.0 \mathrm{mph}$

$\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 145.7 | 469.6 |
| Effective width of outside lane | ne, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.70 | 3.29 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $653 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $327 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.3 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.994 |  | 0.982 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 714 | pc/h | 362 | pc/h |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \quad \mathrm{mi} / \mathrm{h}$
Adjustment for no-passing zones, fnp
Average travel speed, ATSd
Percent Free Flow Speed, PFFS
$1.4 \mathrm{mi} / \mathrm{h}$
$48.2 \mathrm{mi} / \mathrm{h}$
$83.1 \mathrm{\%}$

Percent Time-Spent-Following $\qquad$

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.0 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 1.000 | 0.994 |  |  |
| Grade adjustment factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 710 | $\mathrm{pc} / \mathrm{h}$ | 358 | $\mathrm{pc} / \mathrm{h}$ |
| Base percent time-spent-following,(note-4) | BPTSFd | 59.9 | $\%$ |  |
| Adjustment for no-passing zones, fnp | 21.1 |  |  |  |
| Percent time-spent-following, PTSFd | 73.9 | $\%$ |  |  |

Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.42 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |  |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $48.2 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
709.8
24.00
4.79
3.81

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.88 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $653 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $279 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.4 |  |  |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) fHV | 0.994 |  | 0.977 |  |  |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |  |  |
| Directional flow rate,(note-2) vi | 747 | pc/h | 325 | $\mathrm{pc} / \mathrm{h}$ |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $48.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $83.1 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |
| :--- | :---: | :--- | :--- | :--- |
| Volume to capacity ratio, v/c | 0.44 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above) C
$48.2 \mathrm{mi} / \mathrm{h}$
75.8

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
742.0
24.00

Effective speed factor, St
4.79

Bicycle LOS Score, BLOS
Bicycle LOS
D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $653 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $242 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $48.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $84.1 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.42 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
709.8

Effective speed factor, St
24.00

Bicycle LOS Score, BLOS
4.79

Bicycle LOS
D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $441 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $803 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $0.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $46.9 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $80.9 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.29 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1700 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  |  | veh/h |
| Directional Capacity | 1700 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $46.9 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
479.3
24.00
4.79
3.61

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $431 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $683 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.2 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.988 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 474 | pc/h | 747 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $0.7 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $47.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $82.5 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.28 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above)
$47.8 \mathrm{mi} / \mathrm{h}$
61.1

C
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
468.5
24.00
4.79
3.60

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 279 veh/h
Opposing direction volume, Vo $857 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $0.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $47.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $82.4 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.18 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1700 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  |  | veh/h |
| Directional Capacity | 1700 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)
Level of service, LOSd (from above)
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
303.3

Effective speed factor, St
24.00

Bicycle LOS Score, BLOS
4.79

Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: AM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR $41 \mathrm{NB} / \mathrm{N} 191 / 2$ Ave |
| Jurisdiction: | Kings County |
| Analysis Year: | 2040 |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC 0.0 mph 0.0 mph
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes 2 | 2 |  |
| :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |
| Trucks and buses PCE, ET | 1.5 | 1.5 |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |
| Flow rate, vp 234 | pcphpl | 686 pcphpl |
|  |  | RESULTS |

## Direction $1 \quad 2$

Flow rate, vp 234 pcphpl 686 pcphpl
Free-flow speed, FFS $55.0 \quad \mathrm{mph} 55.0 \mathrm{mph}$

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$
Level of service, LOS A B
Density, D $4.3 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln} 12.5 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
Bicycle Level of Service $\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | - 228.8 | 669.6 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.93 | 3.47 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: AM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: | 2040 |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 196 | pcphpl | 624 |  |  |

$\qquad$

## Direction $1 \quad 2$

Flow rate, vp 196 pcphpl 624 pcphpl
Free-flow speed, FFS $55.0 \quad \mathrm{mph} 55.0 \mathrm{mph}$

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$
Level of service, LOS A B
Density, D $\quad 3.6 \mathrm{pc} / \mathrm{mi} / \ln 11.3 \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
Bicycle Level of Service $\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 191.3 | 609.2 |
| Effective width of outside lane, | ne, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.84 | 3.42 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $803 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $441 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.2 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $46.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $79.7 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.51 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1680 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |  |
| Directional Capacity | 1680 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above)
$46.2 \mathrm{mi} / \mathrm{h}$ 80.3

C
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
872.8
4.79
3.92

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $683 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo veh/h
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.994 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 747 | pc/h | 747 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \quad \mathrm{mi} / \mathrm{h}$

Adjustment for no-passing zones, fnp
Average travel speed, ATSd
Percent Free Flow Speed, PFFS
$0.7 \mathrm{mi} / \mathrm{h}$
$45.7 \mathrm{mi} / \mathrm{h}$
78.8 \%

Percent Time-Spent-Following $\qquad$

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.0 | 1.0 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 1.000 |  |  |  |
| Grade adjustment factor,(note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate,(note-2) vi | 742 | $\mathrm{pc} / \mathrm{h}$ | 742 | $\mathrm{pc} / \mathrm{h}$ |
| Base percent time-spent-following,(note-4) | BPTSFd | 67.1 | $\%$ |  |
| Adjustment for no-passing zones, fnp | 19.1 |  |  |  |
| Percent time-spent-following, PTSFd | 76.7 | $\%$ |  |  |

Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.44 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above) C
$45.7 \mathrm{mi} / \mathrm{h}$
76.7

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
742.4
24.00

Effective speed factor, St
4.79

Bicycle LOS Score, BLOS
Bicycle LOS
D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highway class | ass 3 |  | Peak hour factor, | 0.92 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 |  |  |
| ne width | 12.0 | ft | \% Trucks crawling |  |  |  |
| Segment leng | 0.0 |  | Truck crawl speed |  |  |  |
| Terrain type | Specific Grade \% Recreational vehicles 4 \% |  |  |  |  |  |
| Grade: Length | 0.25 |  | \% No-passing zo |  |  |  |
| Up/down | 3.0 | \% | Access point density | 8 |  |  |

Analysis direction volume, Vd 857 veh/h
Opposing direction volume, Vo $279 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.4 |  |  |
| PCE for RVs, ER |  | 1.0 | 1.0 |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.994 |  | 0.977 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 937 | pc/h | 311 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $46.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | 80.7 m |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.55 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1373 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1648 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1373 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $46.8 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 460 veh/h
Opposing direction volume, Vo $880 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.2 | 1.0 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.988 |  |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.000 |  |  |
| Directional flow rate,(note-2) vi | 506 | $\mathrm{pc} / \mathrm{h}$ | 957 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $0.6 \mathrm{mi} / \mathrm{h}$ |
| Average travel speed, ATSd | $46.1 \mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $79.5 \%$ |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.30 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1700 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  |  | veh/h |
| Directional Capacity | 1700 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above)
$46.1 \mathrm{mi} / \mathrm{h}$
Level of service, LOSd (from above) C62.1

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
500.0
24.00
4.79
3.64

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

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Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $452 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $769 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $0.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $47.1 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $81.1 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.29 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)
Level of service, LOSd (from above)
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

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Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highway class | ass 3 |  | Peak hour factor, | 0.92 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 |  |  |
| ne width | 12.0 | ft | \% Trucks crawling |  |  |  |
| Segment leng | 0.0 |  | Truck crawl speed |  |  |  |
| Terrain type | Specific Grade \% Recreational vehicles 4 \% |  |  |  |  |  |
| Grade: Length | 0.25 |  | \% No-passing zo |  |  |  |
| Up/down | 3.0 | \% | Access point density | 8 |  |  |

Analysis direction volume, Vd 300 veh/h
Opposing direction volume, Vo $943 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $0.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $46.4 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $80.0 \mathrm{\%}$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.23 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1564 |  |  |  |  |  | veh/h |
| Directional Capacity | 1690 | veh $/ \mathrm{h}$ |  |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi
$46.4 \mathrm{mi} / \mathrm{h}$
Level of service, LOSd (from above)
C

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
326.1
24.00
4.79
3.42

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: AM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 NB/N 19 1/2 Ave |
| Jurisdiction: | Kings County |
| Analysis Year: | 2040+Project |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes 2 | 2 |  |
| :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |
| Trucks and buses PCE, ET | 1.5 | 1.5 |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |
| Flow rate, vp 242 | pcphpl | 718 pcphpl |
|  |  | RESULTS |


|  | Direction | 1 | 2 |  |  |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| Flow rate, vp | 242 | pcphpl | 718 |  |  |  |  | pcphpl

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

Level of service, LOS
Density, D

A
$4.4 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln} 13.1 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
Bicycle Level of Service $\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 236.4 | 700.5 |
| Effective width of outside lane, | ne, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.94 | 3.49 |
| Bicycle LOS C | C | C |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: | R\&S Civil |
| Date: | 12/18/2020 |
| Analysis Period: AM |  |
| Highway: | Bush Street |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: | 2040+Project |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes 2 | 2 |  |
| :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |
| Trucks and buses PCE, ET | 1.5 | 1.5 |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |
| Flow rate, vp 208 | pcphpl | 663 pcphpl |
|  |  | RESULTS |


|  | Direction | 1 | 2 |  |
| :--- | :--- | :--- | :--- | :--- |
| Flow rate, vp | 208 | pcphpl | 663 | pcphpl |
| Free-flow speed, FFS |  | 55.0 | mph | 55.0 | mph

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$
Level of service, LOS A B
Density, D $\quad 3.8 \mathrm{pc} / \mathrm{mi} / \mathrm{ln} 12.1 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
Bicycle Level of Service $\qquad$


Overall results are not computed when free-flow speed is less than 45 mph .

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Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 880 veh/h
Opposing direction volume, Vo $460 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.2 \mathrm{mi} / \mathrm{h}$ |
| Average travel speed, ATSd | $45.5 \mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $78.4 \%$ |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.56 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1680 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1680 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above) C
$45.5 \mathrm{mi} / \mathrm{h}$
82.3

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
956.5
24.00
4.79
3.96

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 769 veh/h
Opposing direction volume, Vo veh/h
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.1 |  |  |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.994 |  | 0.994 |  |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |  |  |
| Directional flow rate,(note-2) vi | 841 | pc/h | 841 | $\mathrm{pc} / \mathrm{h}$ |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $0.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $44.4 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $76.5 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.49 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above) C
$44.4 \mathrm{mi} / \mathrm{h}$
79.7

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
835.9
24.00
4.79
3.90

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period AM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highway class | ass 3 |  | Peak hour factor, | 0.92 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 |  |  |
| ne width | 12.0 | ft | \% Trucks crawling |  |  |  |
| Segment leng | 0.0 |  | Truck crawl speed |  |  |  |
| Terrain type | Specific Grade \% Recreational vehicles 4 \% |  |  |  |  |  |
| Grade: Length | 0.25 |  | \% No-passing zo |  |  |  |
| Up/down | 3.0 | \% | Access point density | 8 |  |  |

Analysis direction volume, Vd $943 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $300 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 |  |  |  |  |  | 1.4 |  |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) fHV | 0.994 |  | 0.977 |  |  |  |  |  |  |  |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |  |  |  |  |  |  |
| Directional flow rate,(note-2) vi | 1031 | pc/h | 334 | $\mathrm{pc} / \mathrm{h}$ |  |  |  |  |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |
| Average travel speed, ATSd | $45.9 \mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $79.2 \%$ |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.61 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1390 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1644 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1390 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $45.9 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking
0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
1025.0
4.79
4.00

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 344 veh/h
Opposing direction volume, Vo $292 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.3 | 1.4 |  |  |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.982 |  | 0.977 |  |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |  |  |
| Directional flow rate,(note-2) vi | 381 | $\mathrm{pc} / \mathrm{h}$ | 325 | $\mathrm{pc} / \mathrm{h}$ |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |
| Average travel speed, ATSd | $51.0 \mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $88.0 \%$ |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.22 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS 3
373.9
24.00
4.79

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highway c | $s 3$ |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment lengt | 0.0 | mi | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles | S | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 | \% |
| Up/down |  |  | Access point density |  | mi |

Analysis direction volume, Vd $264 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $512 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.1 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $50.3 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | 86.7 m |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.17 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We 287.0
24.00

Effective speed factor, St
4.79

Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 264 veh/h
Opposing direction volume, Vo $222 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 |  |  |  |  | 1.5 |  |
| PCE for RVs, ER |  | 1.0 | 1.0 |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.977 |  | 0.971 |  |  |  |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |  |  |  |
| Directional flow rate,(note-2) vi | 294 | pc/h | 249 | $\mathrm{pc} / \mathrm{h}$ |  |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $52.1 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $89.9 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.17 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1651 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1651 | $\mathrm{veh} / \mathrm{h}$ |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl

- mi

Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)
$52.1 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
B

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We 287.0
24.00

Effective speed factor, St
4.79

Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: PM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 NB/N 19 1/2 Ave |
| Jurisdiction: Kings County |  |
| Analysis Year: 2020 |  |
| Project ID: $\quad$ Community College Expansion |  |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC 0.0 mph 0.0 mph
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 0.976  <br> pcphpl 188 pcphpl <br> Flow rate, vp   <br>    <br>   RESULTS |  |  |  |  |


| Direction | 1 | 2 |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Flow rate, vp | 297 | pcphpl | 188 | pcphpl |
| Free-flow speed, FFS |  | mph |  | 0 mp |

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

$\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 290.2 | 183.7 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 3.05 | 2.82 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: PM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: 2020 |  |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph

| Number of lanes | 2 |  | 2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 189 | pcphpl | 197 |  |  |

$\qquad$
Direction $1 \quad 2$
Flow rate, vp 189 pcphpl 197 pcphpl
Free-flow speed, FFS $55.0 \quad \mathrm{mph} 55.0 \mathrm{mph}$

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$
Level of service, LOS A A
Density, D $3.4 \quad \mathrm{pc} / \mathrm{mi} / \ln 3.6 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
Bicycle Level of Service $\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 185.3 | 192.9 |
| Effective width of outside lane | ne, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.82 | 2.84 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 292 veh/h
Opposing direction volume, Vo $344 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 |  |  |  |  | 1.3 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.977 |  | 0.982 |  |  |  |  |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |  |  |  |  |
| Directional flow rate,(note-2) vi | 325 | pc/h | 381 | $\mathrm{pc} / \mathrm{h}$ |  |  |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.4 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | 51.1 | $\mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $88.1 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.19 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |  |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
317.4
24.00
4.79
3.40

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $512 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $264 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.9 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.33 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
556.5
24.00
4.79

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $222 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $264 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.5 | 1.4 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.971 | 0.977 |  |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate,(note-2) vi | 249 | $\mathrm{pc} / \mathrm{h}$ | 294 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $52.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $90.0 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.15 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
241.3
24.00
4.79

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 378 veh/h
Opposing direction volume, Vo $335 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.4 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $50.5 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $87.0 \%$ |  |


|  | Percent | Time-Spent-Following__ |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Direction | Analysis(d) | Opposing (o) |  |  |
| PCE for trucks, ET | 1.0 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 1.000 | 0.994 |  |  |
| Grade adjustment factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 411 | $\mathrm{pc} / \mathrm{h}$ | 366 | $\mathrm{pc} / \mathrm{h}$ |
| Base percent time-spent-following,(note-4) | BPTSFd | 43.4 | $\%$ |  |
| Adjustment for no-passing zones, fnp | 32.8 |  |  |  |
| Percent time-spent-following, PTSFd | 60.7 | $\%$ |  |  |

Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.25 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highway c | lass 1 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment lengt | 0.0 | mi | Truck crawl speed | 0. |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 | \% |
| Up/down |  |  | Access point density |  | mi |

Analysis direction volume, Vd $302 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $560 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 | 1.1 |  |  |
| PCE for RVs, ER |  | 1.0 | 1.0 |  |
|  |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.977 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate,(note-2) vi | 336 | pc/h | 612 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.0 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.7 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.6 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.20 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above) C
$49.7 \mathrm{mi} / \mathrm{h}$
49.1

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
328.3
24.00
4.79

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $302 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $270 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 | 1.4 |  |  |
| PCE for RVs, ER |  | 1.0 | 1.0 |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.977 |  | 0.977 |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate,(note-2) vi | 336 | pc/h | 300 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $51.5 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $88.8 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.20 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
328.3
24.00
4.79

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: PM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 NB/N 19 1/2 Ave |
| Jurisdiction: | Kings County |
| Analysis Year: | 2020+Project |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes 2 | 2 |  |
| :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |
| Trucks and buses PCE, ET | 1.5 | 1.5 |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |
| Flow rate, vp 311 | pcphpl | 206 pcphpl |
| RESULTS |  |  |


| Direction | 1 | 2 |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Flow rate, vp | 311 | pcphpl |  | pcphpl |
| Free-flow speed, FFS |  | mph |  | 0 mp |

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

Level of service, LOS
Density, D

A
$5.7 \mathrm{pc} / \mathrm{mi} / \ln 3.7 \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
Bicycle Level of Service $\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 304.3 | 201.1 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 3.07 | 2.86 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: | R\&S Civil |
| Date: | $12 / 18 / 2020$ |
| Analysis Period: PM |  |
| Highway: | Bush Street |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: | 2020+Project |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured FFS or BFFS 55.0 mph 55.0 mph
Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph
VOLUME


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 207 | pcphpl | 219 |  |  |$\quad$| pcphpl |  |  |
| :--- | :--- | :--- |
|  |  |  |
|  |  |  |
|  |  | RESULTS |


|  | Direction | 1 | 2 |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Flow rate, vp | 207 | pcphpl | 219 |  |  | pcphpl

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

| Level of service, LOS |  | A | A <br> Density, D |
| :--- | :--- | ---: | :--- |
|  | 3.8 | $\mathrm{pc} / \mathrm{mi} / \mathrm{ln} 4.0$ | $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |

$\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 202.2 | 214.1 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.86 | 2.89 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $335 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $378 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.3 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $50.5 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $87.2 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.22 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
364.1
24.00
4.79

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | ass 1 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 560 veh/h
Opposing direction volume, Vo $302 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.4 |  |  |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) fHV | 0.994 |  | 0.977 |  |  |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |  |  |
| Directional flow rate,(note-2) vi | 612 | pc/h | 336 | $\mathrm{pc} / \mathrm{h}$ |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.2 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $84.8 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | D |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.36 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2020+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 270 veh/h
Opposing direction volume, Vo $302 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $51.6 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $88.9 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.18 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We 293.5
24.00

Effective speed factor, St
4.79

Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 376 veh/h
Opposing direction volume, Vo $317 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.4 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $50.6 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $87.2 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.24 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We 408.7

Effective speed factor, St
24.00

Bicycle LOS Score, BLOS
4.79

Bicycle LOS
D
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 304 veh/h
Opposing direction volume, Vo $538 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.0 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.8 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.20 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P 3
Flow rate in outside lane, vOL
Effective width of outside lane, We 330.4

Effective speed factor, St
Bicycle LOS Score, BLOS
4.79

Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 279 veh/h
Opposing direction volume, Vo $245 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.6 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $51.9 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $89.4 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.18 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
303.3

Effective speed factor, St
24.00

Bicycle LOS Score, BLOS
4.79

Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: PM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR $41 \mathrm{NB} / \mathrm{N} 191 / 2$ Ave |
| Jurisdiction: | Kings County |
| Analysis Year: | 2024 |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC 0.0 mph 0.0 mph
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes 2 | 2 |  |
| :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |
| Trucks and buses PCE, ET | 1.5 | 1.5 |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |
| Flow rate, vp 323 | pcphpl | 208 pcphpl |
|  |  | RESULTS |


| Direction | 1 | 2 |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Flow rate, vp | 323 | pcphpl |  | pcphpl |
| Free-flow speed, FFS |  | mph |  | 0 mp |

Avg. passenger-car travel speed, S $55.0 \mathrm{mph} \quad 55.0 \mathrm{mph}$

$\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 315.2 | 203.8 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 3.09 | 2.87 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: PM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: 2024 |  |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 207 | pcphpl | 215 |  |  |

$\qquad$

|  | Direction | 1 | 2 |  |
| :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |
| Flow rate, vp | 207 | pcphpl | 215 | pcphpl |
| Free-flow speed, FFS |  | 55.0 | mph | 55.0 | mph

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

| Level of service, LOS |  | A | A <br> Density, D |
| :--- | :--- | ---: | :--- |
|  | 3.8 | $\mathrm{pc} / \mathrm{mi} / \mathrm{ln} 3.9$ | $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |

$\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 202.2 | 210.3 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.86 | 2.88 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 317 veh/h
Opposing direction volume, Vo $376 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 |  |  |  |  | 1.3 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.977 | 0.982 |  |  |  |  |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |  |  |  |  |
| Directional flow rate,(note-2) vi | 353 | pc/h | 416 | $\mathrm{pc} / \mathrm{h}$ |  |  |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
|  |  |  |
| Adjustment for no-passing zones, fnp | $1.3 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | 50.7 | $\mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $87.4 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.21 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |  |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $\quad 12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $538 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $304 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.3 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.1 \%$ |  |


| Percent Time-Spent-Following__ |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Direction | Analysis(d) | Opposing (o) |  |  |
| PCE for trucks, ET | 1.0 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 1.000 | 0.994 |  |  |
| Grade adjustment factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 585 | $\mathrm{pc} / \mathrm{h}$ | 332 | $\mathrm{pc} / \mathrm{h}$ |
| Base percent time-spent-following,(note-4) | BPTSFd | 53.2 | $\%$ |  |
| Adjustment for no-passing zones, fnp | 24.6 |  |  |  |
| Percent time-spent-following, PTSFd | 68.9 | $\%$ |  |  |

Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.35 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
584.8
24.00
4.79

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $245 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $279 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $51.9 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $89.6 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.16 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
266.3
24.00
4.79
3.32

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 410 veh/h
Opposing direction volume, Vo $360 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.3 |  |  |  |  |  | 1.3 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.982 | 0.982 |  |  |  |  |  |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |  |  |  |  |  |
| Directional flow rate,(note-2) vi | 454 | $\mathrm{pc} / \mathrm{h}$ | 398 | $\mathrm{pc} / \mathrm{h}$ |  |  |  |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.4 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $50.0 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $86.2 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.27 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |  |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
445.7
4.79
3.58

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $342 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $586 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \mathrm{mi} / \mathrm{h}$

Adjustment for no-passing zones, fnp
Average travel speed, ATSd
Percent Free Flow Speed, PFFS
$0.9 \mathrm{mi} / \mathrm{h}$
$49.2 \mathrm{mi} / \mathrm{h}$
84.8 \%

Percent Time-Spent-Following


Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.22 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, Lt 0.0 mi
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $49.2 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
B

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 317 veh/h
Opposing direction volume, Vo 293 veh/h
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 | 1.4 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) fHV | 0.977 | 0.977 |  |  |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate,(note-2) vi | 353 | $\mathrm{pc} / \mathrm{h}$ | 326 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.5 \mathrm{mi} / \mathrm{h}$ |
| Average travel speed, ATSd | $51.2 \mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $88.3 \%$ |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.21 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: PM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 NB/N 19 1/2 Ave |
| Jurisdiction: | Kings County |
| Analysis Year: | 2024+Project |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured FFS or BFFS 55.0 mph 55.0 mph
Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph
VOLUME $\qquad$

|  |  | Direction 1 |
| :---: | :---: | :---: |
|  |  | Volume, V 606 vph 407 vph |
|  |  | Peak-hour factor, PHF 0.92 0.92 |
|  |  | Peak 15-minute volume, v15 165 111 |
|  |  | Trucks and buses $50 \%$ \% |
|  |  | Recreational vehicles 0 \% 0 \% |
|  |  | Terrain type Level Level |
|  |  | Grade 0.00 \% 0.00 \% |
|  |  | Segment length 0.00 mi 0.00 mi |


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 337 | pcphpl | 226 |  |  |

$\qquad$

| Direction | 1 | 2 |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Flow rate, vp | 337 | pcphpl | 226 | pcphpl |
| Free-flow speed, FFS |  | mph |  | mp |

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

Level of service, LOS
Density, D

A
$6.1 \quad \mathrm{pc} / \mathrm{mi} / \ln 4.1 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
Bicycle Level of Service $\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 329.3 | 221.2 |
| Effective width of outside lane | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 3.11 | 2.91 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: | R\&S Civil |
| Date: | $12 / 18 / 2020$ |
| Analysis Period: PM |  |
| Highway: | Bush Street |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: | 2024+Project |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 224 | pcphpl | 237 |  |  |
|  |  |  | pcphpl |  |  |

$\qquad$

| Direction | 1 | 2 |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Flow rate, vp | 224 | pcphpl |  | pcphpl |
| Free-flow speed, FFS |  | mph |  | mp |

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

Level of service, LOS
Density, D

A
$4.1 \quad \mathrm{pc} / \mathrm{mi} / \ln 4.3 \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
Bicycle Level of Service $\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 219.0 | 231.5 |
| Effective width of outside lane, | ne, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 2.90 | 2.93 |
| Bicycle LOS C | C | C |

Overall results are not computed when free-flow speed is less than 45 mph .

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 360 veh/h
Opposing direction volume, Vo $410 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.3 |  |  |  |  |  | 1.3 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.982 | 0.982 |  |  |  |  |  |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |  |  |  |  |  |
| Directional flow rate,(note-2) vi | 398 | $\mathrm{pc} / \mathrm{h}$ | 454 | $\mathrm{pc} / \mathrm{h}$ |  |  |  |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.3 \mathrm{mi} / \mathrm{h}$ |
| Average travel speed, ATSd | $50.1 \mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $86.4 \%$ |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.23 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl

- mi

Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)
$50.1 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
B
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
391.3
24.00
4.79
3.51

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $586 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $342 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.4 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $48.7 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $83.9 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.38 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
637.0
24.00
4.79
3.76

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2024+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 293 veh/h
Opposing direction volume, Vo $317 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.4 | 1.4 |  |  |
| PCE for RVs, ER | 1.0 |  | 1.0 |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.977 |  | 0.977 |
| Grade adj. factor,(note-1) fg | 1.00 |  | 1.00 |  |
| Directional flow rate,(note-2) vi | 326 | pc/h | 353 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.4 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $51.3 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $88.4 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.19 |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |
| Capacity from ATS, CdATS |  | 1661 | veh $/ \mathrm{h}$ |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |
| Directional Capacity | 1661 | $\mathrm{veh} / \mathrm{h}$ |  |  |



Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
318.5
24.00
4.79
3.41

C

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $538 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $443 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \quad \mathrm{mi} / \mathrm{h}$

Adjustment for no-passing zones, fnp
Average travel speed, ATSd
Percent Free Flow Speed, PFFS
$1.2 \mathrm{mi} / \mathrm{h}$
$48.4 \mathrm{mi} / \mathrm{h}$
83.5 \%

Percent Time-Spent-Following


Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.35 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1680 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1680 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above) B
$48.4 \mathrm{mi} / \mathrm{h}$

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
584.8
24.00
4.79

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $597 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $657 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.994 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 653 | $\mathrm{pc} / \mathrm{h}$ | 718 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \quad \mathrm{mi} / \mathrm{h}$

| Adjustment for no-passing zones, fnp | $0.7 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Average travel speed, ATSd | $46.6 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $80.4 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.38 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl - mi
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)
Level of service, LOSd (from above)
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
648.9

Effective speed factor, St
Bicycle LOS Score, BLOS
4.79

Bicycle LOS
D
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

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Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 353 veh/h
Opposing direction volume, Vo $369 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.3 | 1.3 |  |  |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.982 | 0.982 |  |  |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |  |  |
| Directional flow rate,(note-2) vi | 391 | $\mathrm{pc} / \mathrm{h}$ | 408 | $\mathrm{pc} / \mathrm{h}$ |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.3 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $50.5 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $87.0 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.23 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We 383.7

Effective speed factor, St
24.00

Bicycle LOS Score, BLOS
4.79

Bicycle LOS
D
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: PM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 NB/N 19 1/2 Ave |
| Jurisdiction: Kings County |  |
| Analysis Year: 2040 |  |
| Project ID: $\quad$ Community College Expansion |  |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC 0.0 mph 0.0 mph
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 447 | pcphpl | 318 |  |  |

$\longrightarrow$ RESULTS___

| Direction | 1 | 2 |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Flow rate, vp | 447 | pcphpl |  | pcphpl |
| Free-flow speed, FFS |  | mph |  | mp |

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$

Level of service, LOS
Density, D

A
$8.1 \mathrm{pc} / \mathrm{mi} / \ln 5.8 \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$

Bicycle Level of Service $\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 436.4 | 310.3 |
| Effective width of outside lane, | e, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 3.25 | 3.08 |
| Bicycle LOS C | C |  |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: PM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: 2040 |  |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 294 | pcphpl | 307 |  |  |


| RESULTS |
| :---: |
| Direction $1 \quad 2$ |
| Flow rate, vp 294 pcphpl 307 pcphpl |
| Free-flow speed, FFS 55.0 mph 55.0 mph |
| Avg. passenger-car travel speed, S 55.0 mph 55.0 mph |
| Level of service, LOS A A |
| Density, D $\quad 5.3 \mathrm{pc} / \mathrm{mi} / \mathrm{ln} 5.6 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |
| Bicycle Level of Service |
| Posted speed limit, $\mathrm{Sp} \quad 55$ |
| Percent of segment with occupied |
| on-highway parking 00 |
| Pavement rating, P ( 3 |
| Flow rate in outside lane, vOL 287.0 300.0 |
| Effective width of outside lane, We 24.0024 .00 |
| Effective speed factor, $\mathrm{St} \quad 4.79$ 4.79 |
| Bicycle LOS Score, BLOS 3.04 3.06 |
| Bicycle LOS C C |

Overall results are not computed when free-flow speed is less than 45 mph .

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Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $443 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $538 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.2 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.988 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 487 | pc/h | 588 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$
Free-flow speed, FFSd $\quad 58.0 \quad \mathrm{mi} / \mathrm{h}$
Adjustment for no-passing zones, fnp
Average travel speed, ATSd
Percent Free Flow Speed, PFFS
$1.0 \mathrm{mi} / \mathrm{h}$
$48.6 \mathrm{mi} / \mathrm{h}$
$83.8 \%$

Percent Time-Spent-Following


Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.29 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P 3
Flow rate in outside lane, vOL
Effective width of outside lane, We 481.5

Effective speed factor, St
24.00

Bicycle LOS Score, BLOS
4.79

Bicycle LOS
D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

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Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $657 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo 597 veh/h
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $0.9 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $46.5 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $80.1 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.42 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above) C
$46.5 \mathrm{mi} / \mathrm{h}$
75.0

Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
714.1
24.00
4.79
3.82

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040 |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $369 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $353 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.3 |  |  |  |  | 1.3 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |  |  |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.982 |  | 0.982 |  |  |  |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |  |  |  |  |
| Directional flow rate,(note-2) vi | 408 | pc/h | 391 | $\mathrm{pc} / \mathrm{h}$ |  |  |  |  |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.4 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $50.4 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $86.9 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.24 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1690 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |  |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
401.1
24.00
4.79
3.52

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $572 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $486 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction Analy | Analysis(d) | Opposing (o) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.2 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | note-5) fHV | 0.994 |  | 0.988 |
| Grade adj. factor,(note-1) fg | $\mathrm{fg} \quad 1.00$ |  | 1.00 |  |
| Directional flow rate,(note-2) vi | -2) vi 625 | $\mathrm{pc} / \mathrm{h}$ | 535 | $5 \mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.1 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $47.9 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $82.5 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.37 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1680 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |  |
| Directional Capacity | 1680 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, Lu - mi
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)
Level of service, LOSd (from above)
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
621.7
24.00
4.79

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $635 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $705 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.1 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.994 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 694 | pc/h | 771 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |
| :--- | :---: |
| Adjustment for no-passing zones, fnp | $0.6 \mathrm{mi} / \mathrm{h}$ |
| Average travel speed, ATSd | $46.0 \mathrm{mi} / \mathrm{h}$ |
| Percent Free Flow Speed, PFFS | $79.3 \%$ |


| Percent Time-Spent-Following__ |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Direction | Analysis(d) | Opposing (o) |  |  |
| PCE for trucks, ET | 1.0 | 1.0 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adjustment factor, fHV | 1.000 | 1.000 |  |  |
| Grade adjustment factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 690 | $\mathrm{pc} / \mathrm{h}$ | 766 | $\mathrm{pc} / \mathrm{h}$ |
| Base percent time-spent-following,(note-4) | BPTSFd | 64.5 | $\%$ |  |
| Adjustment for no-passing zones, fnp | 19.1 |  |  |  |
| Percent time-spent-following, PTSFd | 73.6 | $\%$ |  |  |

Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.41 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh/h |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above)
$46.0 \mathrm{mi} / \mathrm{h}$
Level of service, LOSd (from above) C
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
690.2

Effective speed factor, St
24.00

Bicycle LOS Score, BLOS
4.79

Bicycle LOS
D
Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 391 veh/h
Opposing direction volume, Vo $414 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.3 | 1.3 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.982 | 0.982 |  |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 433 | $\mathrm{pc} / \mathrm{h}$ | 458 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM - mi/h
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.3 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.9 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.25 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
425.0
24.00
4.79
3.55

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: PM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 NB/N 19 1/2 Ave |
| Jurisdiction: | Kings County |
| Analysis Year: | 2040+Project |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured FFS or BFFS 55.0 mph 55.0 mph
Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \quad \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph
VOLUME $\qquad$


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 461 | pcphpl | 335 |  |  |

$\qquad$
Direction 1 2
Flow rate, vp 461 pcphpl 335 pcphpl
Free-flow speed, FFS 55.0 mph 55.0 mph

Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$
Level of service, LOS
Density, D $8.4 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln} 6.1 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 450.5 | 327.7 |
| Effective width of outside lane | ne, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 3.27 | 3.11 |
| Bicycle LOS C | C | C |

Overall results are not computed when free-flow speed is less than 45 mph .

OPERATIONAL ANALYSIS

| Analyst: | Shalisha Hodson |
| :--- | :--- |
| Agency/Co: $\quad$ R\&S Civil |  |
| Date: $\quad 12 / 18 / 2020$ |  |
| Analysis Period: PM |  |
| Highway: $\quad$ Bush Street |  |
| From/To: | SR 41 SB/SR 41 NB |
| Jurisdiction: | Kings County |
| Analysis Year: | 2040+Project |
| Project ID: | Community College Expansion |

FREE-FLOW SPEED
Direction 1

| Lane width | 12.0 | ft | 12.0 | ft |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Lateral clearance: |  |  |  |  |  |
| $\quad$ Right edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Left edge | 6.0 | ft | 6.0 | ft |  |
| $\quad$ Total lateral clearance | 12.0 | ft | 12.0 | ft |  |
| Access points per mile | 0 |  | 0 |  |  |

Median type
Free-flow speed: Measured Measured
FFS or BFFS 55.0 mph 55.0 mph

Lane width adjustment, FLW $\quad 0.0 \quad \mathrm{mph} 0.0 \mathrm{mph}$
Lateral clearance adjustment, FLC $\quad 0.0$ mph $0.0 \quad \mathrm{mph}$
Median type adjustment, FM $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \quad \mathrm{mph}$
Access points adjustment, FA $\quad 0.0 \quad \mathrm{mph} \quad 0.0 \mathrm{mph}$
Free-flow speed 55.0 mph 55.0 mph


| Number of lanes | 2 |  | 2 |  |  |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Driver population adjustment, fP | 1.00 | 1.00 |  |  |  |
| Trucks and buses PCE, ET | 1.5 | 1.5 |  |  |  |
| Recreational vehicles PCE, ER | 1.2 | 1.2 |  |  |  |
| Heavy vehicle adjustment, fHV | 0.976 | 0.976 |  |  |  |
| Flow rate, vp | 311 | pcphpl | 329 |  |  |

$\qquad$
Direction $1 \quad 2$
Flow rate, vp 311 pcphpl 329 pcphpl
Free-flow speed, FFS $55.0 \quad \mathrm{mph} 55.0 \mathrm{mph}$
Avg. passenger-car travel speed, S $55.0 \quad \mathrm{mph} \quad 55.0 \mathrm{mph}$
Level of service, LOS
A
A
Density, D $\quad 5.7 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln} 6.0 \quad \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$
$\qquad$

| Posted speed limit, Sp | 55 | 55 |
| :---: | :---: | :---: |
| Percent of segment with occupied |  |  |
| on-highway parking | 0 | 0 |
| Pavement rating, P | 3 | 3 |
| Flow rate in outside lane, vOL | L 303.8 | 321.2 |
| Effective width of outside lane, | ne, We 24.00 | 24.00 |
| Effective speed factor, St | 4.79 | 4.79 |
| Bicycle LOS Score, BLOS | 3.07 | 3.10 |
| Bicycle LOS C | C | C |

Overall results are not computed when free-flow speed is less than 45 mph .

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Belle Haven Dr/SR 41 |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 486 veh/h
Opposing direction volume, Vo $572 \mathrm{veh} / \mathrm{h}$
Average Travel Speed

| Direction | Analysis(d) | Opposing (o) |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PCE for trucks, ET | 1.2 | 1.1 |  |  |
| PCE for RVs, ER | 1.0 | 1.0 |  |  |
| Heavy-vehicle adj. factor,(note-5) | fHV | 0.988 |  | 0.994 |
| Grade adj. factor,(note-1) fg | 1.00 | 1.00 |  |  |
| Directional flow rate,(note-2) vi | 535 | pc/h | 625 | $\mathrm{pc} / \mathrm{h}$ |

Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.0 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $48.0 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $82.8 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.31 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)

- mi

Percent time-spent-following, PTSFd (from above) $48.0 \mathrm{mi} / \mathrm{h}$

Level of service, LOSd (from above)
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane $\qquad$

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS

3
528.3
24.00
4.79
3.66

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | 12/14/2020 |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | College Ave/Semas Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd $705 \mathrm{veh} / \mathrm{h}$
Opposing direction volume, Vo $635 \mathrm{veh} / \mathrm{h}$
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | 58.0 | $\mathrm{mi} / \mathrm{h}$ |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $0.8 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $45.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $79.0 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | C |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.45 |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |
| Capacity from ATS, CdATS |  | 1690 | veh $/ \mathrm{h}$ |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | veh/h |
| Directional Capacity | 1690 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |

Passing Lane Analysis $\qquad$
Total length of analysis segment, $\mathrm{Lt} \quad 0.0 \mathrm{mi}$
Length of two-lane highway upstream of the passing lane, $\mathrm{Lu}-\mathrm{mi}$
Length of passing lane including tapers, Lpl
Average travel speed, ATSd (from above)
Percent time-spent-following, PTSFd (from above)

- mi

Level of service, LOSd (from above)
$45.8 \mathrm{mi} / \mathrm{h}$
Level of service, LOSd (from above) C
Average Travel Speed with Passing Lane $\qquad$
Downstream length of two-lane highway within effective
length of passing lane for average travel speed, Lde - mi
Length of two-lane highway downstream of effective
length of the passing lane for average travel speed, Ld - mi
Adj. factor for the effect of passing lane
on average speed, fpl
Average travel speed including passing lane, ATSpl
Percent free flow speed including passing lane, PFFSpl $0.0 \quad \%$
Percent Time-Spent-Following with Passing Lane

Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0
Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
766.3
24.00

Effective speed factor, St
4.79

Bicycle LOS Score, BLOS
3.85

Bicycle LOS
D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

Phone:
Fax:
E-Mail:
Directional Two-Lane Highway Segment Analysis

| Analyst | Shalisha Hodson |
| :--- | :---: |
| Agency/Co. | R\&S Civil |
| Date Performed | $12 / 14 / 2020$ |
| Analysis Time Period PM |  |
| Highway | Bush Street |
| From/To | Semas Dr/Belle Haven Dr |
| Jurisdiction | Kings County |
| Analysis Year | 2040+Project |
| Description Community College Expansion |  |

Input Data $\qquad$

| Highw | s 3 |  | Peak hour factor, P | 0.92 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shoulder width | 6.0 | ft | \% Trucks and buses | 6 | \% |
| Lane width | 12.0 | ft | \% Trucks crawling | 0.0 | \% |
| Segment leng | 0.0 | m | Truck crawl speed | 0.0 |  |
| Terrain type | Level |  | \% Recreational vehicles |  | \% |
| Grade: Length |  | mi | \% No-passing zones | 20 |  |
| Up/down |  | \% | Access point density |  | mi |

Analysis direction volume, Vd 414 veh/h
Opposing direction volume, Vo 391 veh/h
Average Travel Speed


Free-Flow Speed from Field Measurement:
Field measured speed,(note-3) S FM $\quad-\quad \mathrm{mi} / \mathrm{h}$
Observed total demand,(note-3) V - veh/h
Estimated Free-Flow Speed:
Base free-flow speed,(note-3) BFFS $\quad 60.0 \mathrm{mi} / \mathrm{h}$
Adj. for lane and shoulder width,(note-3) fLS $0.0 \mathrm{mi} / \mathrm{h}$
Adj. for access point density,(note-3) fA $2.0 \mathrm{mi} / \mathrm{h}$

| Free-flow speed, FFSd | $58.0 \mathrm{mi} / \mathrm{h}$ |  |
| :--- | :---: | :---: |
| Adjustment for no-passing zones, fnp | $1.3 \mathrm{mi} / \mathrm{h}$ |  |
| Average travel speed, ATSd | $49.8 \mathrm{mi} / \mathrm{h}$ |  |
| Percent Free Flow Speed, PFFS | $85.8 \%$ |  |



Level of Service and Other Performance Measures $\qquad$

| Level of service, LOS | B |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume to capacity ratio, v/c | 0.27 |  |  |  |  |  |  |
| Peak 15-min vehicle-miles of travel, VMT15 | 0 | veh-mi |  |  |  |  |  |
| Peak-hour vehicle-miles of travel, VMT60 | 0 | veh-mi |  |  |  |  |  |
| Peak 15-min total travel time, TT15 | 0.0 | veh-h |  |  |  |  |  |
| Capacity from ATS, CdATS |  | 1669 | veh $/ \mathrm{h}$ |  |  |  |  |
| Capacity from PTSF, CdPTSF | 1700 |  |  |  |  | $\mathrm{veh} / \mathrm{h}$ |  |
| Directional Capacity | 1669 | $\mathrm{veh} / \mathrm{h}$ |  |  |  |  |  |



Downstream length of two-lane highway within effective length
of passing lane for percent time-spent-following, Lde - mi
Length of two-lane highway downstream of effective length of
the passing lane for percent time-spent-following, Ld - mi
Adj. factor for the effect of passing lane
on percent time-spent-following, fpl
Percent time-spent-following
including passing lane, PTSFpl - $\%$
Level of Service and Other Performance Measures with Passing Lane $\qquad$
Level of service including passing lane, LOSpl E
Peak 15-min total travel time, TT15 - veh-h
Bicycle Level of Service $\qquad$
Posted speed limit, Sp 55
Percent of segment with occupied on-highway parking 0

Pavement rating, P
Flow rate in outside lane, vOL
Effective width of outside lane, We
Effective speed factor, St
Bicycle LOS Score, BLOS
Bicycle LOS
450.0
4.79
3.58

D

Notes:

1. Note that the adjustment factor for level terrain is 1.00 , as level terrain is one of the base conditions. For the purpose of grade adjustment, specific dewngrade segments are treated as level terrain.
2. If vi (vd or vo ) $>=1,700 \mathrm{pc} / \mathrm{h}$, terminate analysis-the LOS is F.
3. For the analysis direction only and for $v>200 \mathrm{veh} / \mathrm{h}$.
4. For the analysis direction only.
5. Use alternative Exhibit 15-14 if some trucks operate at crawl speeds on a specific downgrade.

## QUEUE LENGTH ANALYSIS

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | WB | SB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | L | L | R |
| Maximum Queue (ft) | 66 | 50 | 39 |
| Average Queue (ft) | 20 | 10 | 14 |
| 95th Queue (ft) | 47 | 32 | 33 |
| Link Distance (ft) | 1122 |  |  |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (ft) | 250 |  | 500 |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | R |
| Maximum Queue (ft) | 51 | 18 | 72 | 116 |
| Average Queue (ft) | 11 | 1 | 42 | 47 |
| 95th Queue (ft) | 36 | 6 | 64 | 78 |
| Link Distance (ft) |  | 540 | 1327 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 300 |
| Storage Bay Dist (ft) | 100 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Network Summary
Network wide Queuing Penalty: 0

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :---: | :---: | :---: | :---: | :---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 51 | 68 | 30 | 58 |
| Average Queue (ft) | 2 | 21 | 10 | 20 |
| 95th Queue (ft) | 17 | 46 | 30 | 39 |
| Link Distance (ft) | 397 |  | 1172 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  | 250 |  | 500 |
| Storage BIk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | NB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | L | L | R |
| Maximum Queue (ft) | 49 | 74 | 72 |
| Average Queue (ft) | 13 | 38 | 45 |
| 95th Queue (ft) | 36 | 61 | 70 |
| Link Distance (ft) |  | 1210 |  |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  | 300 |
| Storage Bay Dist (ft) | 100 |  |  |
| Storage Blk Time (\%) |  |  |  |

Network Summary
Network wide Queuing Penalty: 0

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 20 | 47 | 50 | 48 |
| Average Queue (ft) | 1 | 19 | 14 | 18 |
| 95th Queue (ft) | 7 | 41 | 36 | 36 |
| Link Distance (ft) | 547 |  | 977 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | R |
| Maximum Queue (ft) | 28 | 21 | 96 | 119 |
| Average Queue (ft) | 9 | 1 | 42 | 58 |
| 95th Queue (ft) | 30 | 10 | 74 | 98 |
| Link Distance (ft) |  | 494 | 1242 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) | 100 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Network Summary
Network wide Queuing Penalty: 0

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 20 | 66 | 28 | 47 |
| Average Queue (ft) | 2 | 23 | 9 | 21 |
| 95th Queue (ft) | 11 | 46 | 27 | 37 |
| Link Distance (ft) | 407 |  | 896 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | NB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | L | L | R |
| Maximum Queue (ft) | 68 | 114 | 114 |
| Average Queue (ft) | 16 | 47 | 55 |
| 95th Queue (ft) | 44 | 84 | 90 |
| Link Distance (ft) |  | 874 |  |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  | 300 |
| Storage Bay Dist (ft) | 100 |  |  |
| Storage Blk Time (\%) |  |  |  |

Network Summary
Network wide Queuing Penalty: 0

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 21 | 68 | 48 | 60 |
| Average Queue (ft) | 4 | 35 | 17 | 19 |
| 95th Queue (ft) | 17 | 61 | 39 | 38 |
| Link Distance (ft) | 435 |  | 1130 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | NB | NB |
| :---: | :---: | :---: | :---: |
| Directions Served | L | L | R |
| Maximum Queue (ft) | 53 | 183 | 272 |
| Average Queue (ft) | 23 | 99 | 130 |
| 95th Queue (ft) | 48 | 182 | 218 |
| Link Distance (ft) |  | 1211 |  |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (ft) | 100 |  | 300 |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Network Summary |  |  |  |
| Network wide Queuing Penalty: 0 |  |  |  |

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 21 | 86 | 25 | 70 |
| Average Queue (ft) | 3 | 34 | 9 | 23 |
| 95th Queue (ft) | 16 | 60 | 28 | 44 |
| Link Distance (ft) | 840 |  | 1230 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | NB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | L | L | R |
| Maximum Queue (ft) | 51 | 353 | 325 |
| Average Queue (ft) | 16 | 90 | 126 |
| 95th Queue (ft) | 43 | 198 | 246 |
| Link Distance (ft) |  | 1525 |  |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  | 300 |
| Storage Bay Dist (ft) | 100 |  | 1 |
| Storage Blk Time (\%) |  |  | 2 |

Network Summary
Network wide Queuing Penalty: 2

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 22 | 68 | 93 | 72 |
| Average Queue (ft) | 1 | 34 | 36 | 26 |
| 95th Queue (ft) | 10 | 57 | 66 | 49 |
| Link Distance (ft) | 424 |  | 1349 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  | 250 |  | 500 |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | NB | NB |  |
| :--- | ---: | ---: | ---: | :---: |
| Directions Served | L | L | R |  |
| Maximum Queue (ft) | 27 | 112 | 49 |  |
| Average Queue (ft) | 11 | 48 | 26 |  |
| 95th Queue (ft) | 31 | 89 | 44 |  |
| Link Distance (ft) | 1149 |  |  |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) | 100 |  | 300 |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
|  |  |  |  |  |
| Network Summary |  |  |  |  |
| Network wide Queuing Penalty: 0 |  |  |  |  |

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 28 | 177 | 94 | 59 |
| Average Queue (ft) | 2 | 40 | 28 | 27 |
| 95th Queue (ft) | 14 | 92 | 58 | 41 |
| Link Distance (ft) | 425 |  | 1007 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | R |
| Maximum Queue (ft) | 50 | 19 | 94 | 66 |
| Average Queue (ft) | 18 | 2 | 58 | 29 |
| 95th Queue (ft) | 41 | 11 | 88 | 44 |
| Link Distance (ft) |  | 438 | 1083 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 300 |
| Storage Bay Dist (ft) | 100 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Network Summary
Network wide Queuing Penalty: 0

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 38 | 93 | 74 | 53 |
| Average Queue (ft) | 3 | 41 | 28 | 26 |
| 95th Queue (ft) | 16 | 77 | 55 | 45 |
| Link Distance (ft) | 398 |  | 1173 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | NB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | L | L | R |
| Maximum Queue (ft) | 27 | 115 | 53 |
| Average Queue (ft) | 12 | 58 | 29 |
| 95th Queue (ft) | 33 | 94 | 41 |
| Link Distance (ft) | 1186 |  |  |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (ft) | 100 |  | 300 |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
|  |  |  |  |
| Network Summary |  |  |  |
| Network wide Queuing Penalty: 0 |  |  |  |

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 21 | 90 | 74 | 58 |
| Average Queue (ft) | 3 | 40 | 36 | 29 |
| 95th Queue (ft) | 14 | 70 | 71 | 43 |
| Link Distance (ft) | 507 |  | 870 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | R |
| Maximum Queue (ft) | 46 | 46 | 225 | 52 |
| Average Queue (ft) | 12 | 2 | 88 | 32 |
| 95th Queue (ft) | 35 | 15 | 175 | 47 |
| Link Distance (ft) |  | 562 | 854 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 300 |
| Storage Bay Dist (ft) | 100 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |

Network Summary
Network wide Queuing Penalty: 0

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 34 | 164 | 184 | 54 |
| Average Queue (ft) | 8 | 69 | 64 | 30 |
| 95th Queue (ft) | 26 | 126 | 139 | 54 |
| Link Distance (ft) | 699 |  | 955 |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | TR | L | R |
| Maximum Queue (ft) | 50 | 21 | 48 | 454 | 325 |
| Average Queue (ft) | 18 | 1 | 2 | 410 | 325 |
| 95th Queue (ft) | 42 | 7 | 18 | 429 | 325 |
| Link Distance (ft) |  | 687 | 687 | 391 |  |
| Upstream Blk Time (\%) |  |  |  | 96 |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |
| Storage Bay Dist (ft) | 100 |  |  | 96 | 300 |
| Storage Blk Time (\%) |  |  |  | 130 | 1 |

Network Summary
Network wide Queuing Penalty: 131

Intersection: 4: SR 41 SB Ramps \& Bush St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | L | R |
| Maximum Queue (ft) | 33 | 156 | 133 | 87 |
| Average Queue (ft) | 6 | 75 | 49 | 34 |
| 95th Queue (ft) | 23 | 132 | 98 | 58 |
| Link Distance (ft) | 408 | 1028 |  |  |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: SR 41 NB Ramps \& Bush St

| Movement | EB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | R |
| Maximum Queue (ft) | 49 | 19 | 414 | 325 |
| Average Queue (ft) | 22 | 3 | 393 | 284 |
| 95th Queue (ft) | 46 | 14 | 411 | 456 |
| Link Distance (ft) |  | 507 | 375 |  |
| Upstream Blk Time (\%) |  |  | 90 |  |
| Queuing Penalty (veh) |  |  | 0 |  |
| Storage Bay Dist (ft) | 100 |  |  | 300 |
| Storage Blk Time (\%) |  |  | 94 | 0 |
| Queuing Penalty (veh) |  |  | 128 | 1 |

Network Summary
Network wide Queuing Penalty: 129

## VEHICLE TURNING MOVEMENT COUNTS

## Metro Traffic Data Inc.

310 N. Irwin Street - Suite 20
Hanford, CA 93230

## Turning Movement Report

Prepared For:
ND Engineering 6807 Leameadow Dallas, TX 75248

| LOCATION | Bush St @ College Ave |
| ---: | :---: |
|  | Kings |
| COLLECTION DATE | Wednesday, August 29, 2018 |


| LATITUDE | 36.2945 |
| ---: | :---: |
| LONGITUDE | -119.8216 |
| WEATHER | Clear |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 7:00 AM - 7:15 AM | 1 | 0 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 19 | 19 | 0 | 1 |
| 7:15 AM - 7:30 AM | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 50 | 39 | 0 | 2 |
| 7:30 AM - 7:45 AM | 2 | 0 | 42 | 2 | 0 | 0 | 0 | 0 | 0 | 13 | 1 | 0 | 75 | 47 | 0 | 2 |
| 7:45 AM - 8:00 AM | 2 | 0 | 94 | 1 | 0 | 0 | 0 | 0 | 0 | 10 | 1 | 1 | 107 | 114 | 0 | 0 |
| 8:00 AM - 8:15 AM | 2 | 0 | 24 | 4 | 0 | 0 | 0 | 0 | 0 | 9 | 2 | 0 | 40 | 40 | 0 | 3 |
| 8:15 AM - 8:30 AM | 2 | 0 | 17 | 1 | 0 | 0 | 0 | 0 | 0 | 13 | 2 | 0 | 30 | 17 | 0 | 2 |
| 8:30 AM - 8:45 AM | 3 | 0 | 31 | 2 | 0 | 0 | 0 | 0 | 0 | 11 | 2 | 0 | 69 | 65 | 0 | 3 |
| 8:45 AM - 9:00 AM | 6 | 0 | 32 | 2 | 0 | 0 | 0 | 0 | 0 | 33 | 4 | 0 | 66 | 141 | 0 | 1 |
| TOTAL | 18 | 0 | 257 | 13 | 0 | 0 | 0 | 0 | 0 | 100 | 12 | 1 | 456 | 482 | 0 | 14 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 4:00 PM - 4:15 PM | 1 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 2 | 0 | 13 | 25 | 0 | 1 |
| 4:15 PM - 4:30 PM | 0 | 0 | 14 | 1 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 0 | 17 | 12 | 0 | 1 |
| 4:30 PM - 4:45 PM | 2 | 0 | 32 | 2 | 0 | 0 | 0 | 0 | 0 | 18 | 3 | 0 | 24 | 11 | 0 | 2 |
| 4:45 PM - 5:00 PM | 3 | 0 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 46 | 0 | 0 | 29 | 57 | 0 | 1 |
| 5:00 PM - 5:15 PM | 0 | 0 | 41 | 2 | 0 | 0 | 0 | 0 | 0 | 44 | 2 | 0 | 18 | 27 | 0 | 2 |
| 5:15 PM - 5:30 PM | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 0 | 20 | 34 | 0 | 0 |
| 5:30 PM - 5:45 PM | 0 | 0 | 18 | 2 | 0 | 0 | 0 | 0 | 0 | 37 | 1 | 0 | 17 | 20 | 0 | 2 |
| 5:45 PM - 6:00 PM | 2 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 1 | 0 | 9 | 24 | 0 | 0 |
| TOTAL | 8 | 0 | 202 | 7 | 0 | 0 | 0 | 0 | 0 | 228 | 9 | 0 | 147 | 210 | 0 | 9 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEAK HOUR | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 7:15 AM - 8:15 AM | 6 | 0 | 168 | 7 | 0 | 0 | 0 | 0 | 0 | 40 | 4 | 1 | 272 | 240 | 0 | 7 |
| 4:45 PM - 5:45 PM | 3 | 0 | 104 | 4 | 0 | 0 | 0 | 0 | 0 | 150 | 3 | 0 | 84 | 138 | 0 | 5 |



## Metro Traffic Data Inc.

310 N. Irwin Street - Suite 20
Hanford, CA 93230

## Turning Movement Report

Prepared For:
ND Engineering 6807 Leameadow Dallas, TX 75248

| LOCATION | Bush St @ Belle Haven Dr |
| ---: | :---: |
| COUNTY | Kings |
| COLLECTION DATE | Wednesday, August 29, 2018 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 7:00 AM - 7:15 AM | 0 | 0 | 5 | 1 | 17 | 0 | 3 | 2 | 3 | 9 | 0 | 1 | 0 | 41 | 12 | 3 |
| 7:15 AM - 7:30 AM | 1 | 0 | 8 | 0 | 13 | 0 | 7 | 3 | 0 | 20 | 0 | 0 | 6 | 89 | 11 | 6 |
| 7:30 AM - 7:45 AM | 1 | 0 | 11 | 1 | 16 | 0 | 9 | 3 | 4 | 54 | 0 | 2 | 5 | 122 | 12 | 3 |
| 7:45 AM - 8:00 AM | 2 | 0 | 17 | 0 | 15 | 0 | 19 | 2 | 9 | 87 | 2 | 1 | 5 | 202 | 10 | 3 |
| 8:00 AM - 8:15 AM | 0 | 0 | 3 | 1 | 8 | 0 | 4 | 2 | 0 | 30 | 0 | 4 | 4 | 53 | 12 | 2 |
| 8:15 AM - 8:30 AM | 0 | 0 | 9 | 0 | 9 | 1 | 2 | 5 | 0 | 31 | 1 | 2 | 3 | 48 | 7 | 5 |
| 8:30 AM - 8:45 AM | 2 | 0 | 6 | 0 | 4 | 0 | 4 | 1 | 0 | 43 | 0 | 2 | 3 | 147 | 11 | 4 |
| 8:45 AM - 9:00 AM | 2 | 1 | 3 | 0 | 10 | 0 | 16 | 3 | 0 | 60 | 2 | 1 | 4 | 182 | 14 | 7 |
| TOTAL | 8 | 1 | 62 | 3 | 92 | 1 | 64 | 21 | 16 | 334 | 5 | 13 | 30 | 884 | 89 | 33 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 4:00 PM - 4:15 PM | 0 | 0 | 5 | 0 | 14 | 1 | 0 | 2 | 0 | 46 | 1 | 1 | 8 | 30 | 5 | 2 |
| 4:15 PM - 4:30 PM | 0 | 0 | 6 | 0 | 19 | 0 | 2 | 5 | 1 | 35 | 0 | 0 | 9 | 28 | 7 | 2 |
| 4:30 PM - 4:45 PM | 0 | 0 | 5 | 0 | 20 | 0 | 3 | 1 | 0 | 54 | 0 | 2 | 12 | 43 | 11 | 6 |
| 4:45 PM - 5:00 PM | 1 | 0 | 8 | 0 | 15 | 0 | 2 | 2 | 1 | 81 | 0 | 0 | 6 | 76 | 9 | 5 |
| 5:00 PM - 5:15 PM | 0 | 0 | 8 | 0 | 6 | 0 | 3 | 1 | 3 | 73 | 0 | 2 | 12 | 45 | 13 | 5 |
| 5:15 PM - 5:30 PM | 1 | 0 | 5 | 1 | 17 | 0 | 5 | 5 | 2 | 30 | 1 | 0 | 13 | 47 | 9 | 2 |
| 5:30 PM - 5:45 PM | 0 | 1 | 8 | 0 | 17 | 2 | 0 | 5 | 1 | 60 | 0 | 2 | 9 | 36 | 15 | 8 |
| 5:45 PM - 6:00 PM | 0 | 0 | 4 | 0 | 7 | 1 | 0 | 0 | 1 | 39 | 0 | 0 | 12 | 26 | 9 | 0 |
| TOTAL | 2 | 1 | 49 | 1 | 115 | 4 | 15 | 21 | 9 | 418 | 2 | 7 | 81 | 331 | 78 | 30 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEAK HOUR | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 7:15 AM - 8:15 AM | 4 | 0 | 39 | 2 | 52 | 0 | 39 | 10 | 13 | 191 | 2 | 7 | 20 | 466 | 45 | 14 |
| 4:45 PM - 5:45 PM | 2 | 1 | 29 | 1 | 55 | 2 | 10 | 13 | 7 | 244 | 1 | 4 | 40 | 204 | 46 | 20 |



## Metro Traffic Data Inc.

310 N. Irwin Street - Suite 20
Hanford, CA 93230

## Turning Movement Report

Prepared For:
ND Engineering 6807 Leameadow Dallas, TX 75248

| LOCATION | Bush St @ SR-41 SB Ramps |
| ---: | :---: |
| COUNTY | Kings |
| COLLECTION DATE | Wednesday, August 29, 2018 |


| LATITUDE | 36.2964 |
| ---: | :---: |
| LONGITUDE | -119.8116 |
| WEATHER | Clear |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 7:00 AM - 7:15 AM | 0 | 0 | 0 | 0 | 16 | 0 | 13 | 3 | 0 | 14 | 14 | 5 | 81 | 48 | 0 | 4 |
| 7:15 AM - 7:30 AM | 0 | 0 | 0 | 0 | 14 | 0 | 10 | 2 | 0 | 20 | 20 | 2 | 88 | 100 | 0 | 8 |
| 7:30 AM - 7:45 AM | 0 | 0 | 0 | 0 | 18 | 0 | 31 | 1 | 0 | 64 | 23 | 6 | 71 | 113 | 0 | 4 |
| 7:45 AM - 8:00 AM | 0 | 0 | 0 | 0 | 11 | 0 | 33 | 1 | 0 | 67 | 49 | 2 | 46 | 178 | 0 | 4 |
| 8:00 AM - 8:15 AM | 0 | 0 | 0 | 0 | 10 | 0 | 15 | 0 | 0 | 28 | 12 | 7 | 30 | 53 | 0 | 2 |
| 8:15 AM - 8:30 AM | 0 | 0 | 0 | 0 | 10 | 0 | 7 | 2 | 0 | 31 | 18 | 6 | 23 | 57 | 0 | 8 |
| 8:30 AM - 8:45 AM | 0 | 0 | 0 | 0 | 12 | 0 | 29 | 2 | 0 | 41 | 13 | 3 | 22 | 138 | 0 | 7 |
| 8:45 AM - 9:00 AM | 0 | 0 | 0 | 0 | 19 | 0 | 37 | 3 | 0 | 50 | 27 | 4 | 26 | 163 | 0 | 9 |
| TOTAL | 0 | 0 | 0 | 0 | 110 | 0 | 175 | 14 | 0 | 315 | 176 | 35 | 387 | 850 | 0 | 46 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 4:00 PM - 4:15 PM | 0 | 0 | 0 | 0 | 27 | 0 | 8 | 0 | 0 | 44 | 18 | 3 | 24 | 43 | 0 | 3 |
| 4:15 PM - 4:30 PM | 0 | 0 | 0 | 0 | 30 | 0 | 10 | 0 | 0 | 38 | 22 | 4 | 20 | 34 | 0 | 2 |
| 4:30 PM - 4:45 PM | 0 | 0 | 0 | 0 | 35 | 0 | 12 | 1 | 0 | 52 | 27 | 3 | 20 | 55 | 0 | 6 |
| 4:45 PM - 5:00 PM | 0 | 0 | 0 | 0 | 25 | 0 | 15 | 0 | 0 | 68 | 35 | 2 | 21 | 78 | 0 | 6 |
| 5:00 PM - 5:15 PM | 0 | 0 | 0 | 0 | 27 | 0 | 8 | 0 | 0 | 73 | 29 | 5 | 15 | 56 | 0 | 5 |
| 5:15 PM - 5:30 PM | 0 | 0 | 0 | 0 | 27 | 0 | 13 | 1 | 0 | 34 | 17 | 7 | 40 | 58 | 0 | 4 |
| 5:30 PM - 5:45 PM | 0 | 0 | 0 | 0 | 35 | 0 | 4 | 2 | 0 | 50 | 37 | 6 | 29 | 58 | 0 | 7 |
| 5:45 PM - 6:00 PM | 0 | 0 | 0 | 0 | 27 | 0 | 10 | 0 | 0 | 37 | 14 | 0 | 19 | 35 | 0 | 2 |
| TOTAL | 0 | 0 | 0 | 0 | 233 | 0 | 80 | 4 | 0 | 396 | 199 | 30 | 188 | 417 |  | 35 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEAK HOUR | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 7:00 AM - 8:00 AM | 0 | 0 | 0 | 0 | 59 | 0 | 87 | 7 | 0 | 165 | 106 | 15 | 286 | 439 | 0 | 20 |
| 4:45 PM - 5:45 PM | 0 | 0 | 0 | 0 | 114 | 0 | 40 | 3 | 0 | 225 | 118 | 20 | 105 | 250 | 0 | 22 |



## Metro Traffic Data Inc.

310 N. Irwin Street - Suite 20
Hanford, CA 93230

## Turning Movement Report

Prepared For:
ND Engineering 6807 Leameadow Dallas, TX 75248

| LOCATION | Bush St @ SR-41 NB Ramps |
| ---: | :---: |
| COUNTY | Kings |
| COLLECTION DATE | Wednesday, August 29, 2018 |

COLLECTION DATE $\qquad$

| LATITUDE | 36.2966 |
| ---: | :---: |
| LONGITUDE | -119.8099 |
| WEATHER | Clear | NEATHER $\qquad$


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 7:00 AM - 7:15 AM | 24 | 0 | 11 | 3 | 0 | 0 | 0 | 0 | 1 | 31 | 0 | 2 | 0 | 109 | 32 | 3 |
| 7:15 AM - 7:30 AM | 48 | 2 | 16 | 5 | 0 | 0 | 0 | 0 | 3 | 28 | 0 | 1 | 0 | 129 | 51 | 4 |
| 7:30 AM - 7:45 AM | 41 | 0 | 22 | 2 | 0 | 0 | 0 | 0 | 15 | 55 | 0 | 2 | 0 | 138 | 42 | 5 |
| 7:45 AM - 8:00 AM | 50 | 0 | 33 | 3 | 0 | 0 | 0 | 0 | 12 | 80 | 0 | 4 | 0 | 185 | 33 | 4 |
| 8:00 AM - 8:15 AM | 24 | 0 | 27 | 1 | 0 | 0 | 0 | 0 | 7 | 33 | 0 | 2 | 0 | 74 | 23 | 4 |
| 8:15 AM - 8:30 AM | 24 | 0 | 20 | 4 | 0 | 0 | 0 | 0 | 8 | 31 | 0 | 4 | 0 | 50 | 25 | 4 |
| 8:30 AM - 8:45 AM | 55 | 0 | 16 | 3 | 0 | 0 | 0 | 0 | 6 | 46 | 0 | 2 | 0 | 90 | 12 | 4 |
| 8:45 AM - 9:00 AM | 64 | 0 | 16 | 4 | 0 | 0 | 0 | 0 | 14 | 54 | 0 | 3 | 0 | 135 | 11 | 5 |
| TOTAL | 330 | 2 | 161 | 25 | 0 | 0 | 0 | 0 | 66 | 358 | 0 | 20 | 0 | 910 | 229 | 33 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 4:00 PM - 4:15 PM | 15 | 0 | 47 | 2 | 0 | 0 | 0 | 0 | 11 | 63 | 0 | 1 | 0 | 50 | 31 | 3 |
| 4:15 PM - 4:30 PM | 14 | 0 | 17 | 2 | 0 | 0 | 0 | 0 | 6 | 50 | 0 | 1 | 0 | 41 | 30 | 2 |
| 4:30 PM - 4:45 PM | 24 | 0 | 61 | 7 | 0 | 0 | 0 | 0 | 12 | 74 | 0 | 3 | 0 | 42 | 21 | 2 |
| 4:45 PM - 5:00 PM | 35 | 0 | 62 | 6 | 0 | 0 | 0 | 0 | 11 | 86 | 0 | 2 | 0 | 63 | 27 | 2 |
| 5:00 PM - 5:15 PM | 27 | 1 | 69 | 1 | 0 | 0 | 0 | 0 | 16 | 85 | 0 | 1 | 0 | 51 | 24 | 6 |
| 5:15 PM - 5:30 PM | 24 | 0 | 54 | 2 | 0 | 0 | 0 | 0 | 5 | 61 | 0 | 4 | 0 | 69 | 19 | 2 |
| 5:30 PM - 5:45 PM | 23 | 0 | 43 | 3 | 0 | 0 | 0 | 0 | 9 | 59 | 0 | 1 | 0 | 57 | 27 | 4 |
| 5:45 PM - 6:00 PM | 19 | 0 | 40 | 2 | 0 | 0 | 0 | 0 | 5 | 68 | 0 | 2 | 0 | 51 | 18 | 1 |
| TOTAL | 181 | 1 | 393 | 25 | 0 | 0 | 0 | 0 | 75 | 546 | 0 | 15 | 0 | 424 | 197 | 22 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEAK HOUR | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 7:00 AM - 8:00 AM | 163 | 2 | 82 | 13 | 0 | 0 | 0 | 0 | 31 | 194 | 0 | 9 | 0 | 561 | 158 | 16 |
| 4:30 PM - 5:30 PM | 110 | 1 | 246 | 16 | 0 | 0 | 0 | 0 | 44 | 306 | 0 | 10 | 0 | 225 | 91 | 12 |



## Metro Traffic Data Inc.

310 N. Irwin Street - Suite 20
Hanford, CA 93230

## Turning Movement Report

Prepared For:
ND Engineering 6807 Leameadow Dallas, TX 75248

| LOCATION | Bush St @ 19 1/2 Ave |
| ---: | :---: |
| COUNTY | Kings |
| COLLECTION DATE | Wednesday, August 29, 2018 |


| LATITUDE | 36.2983 |
| ---: | :---: |
| LONGITUDE | -119.8078 |
| WEATHER | Clear |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 7:00 AM - 7:15 AM | 29 | 10 | 3 | 0 | 7 | 7 | 69 | 2 | 14 | 15 | 12 | 1 | 4 | 41 | 1 | 3 |
| 7:15 AM - 7:30 AM | 40 | 14 | 7 | 1 | 6 | 10 | 82 | 0 | 14 | 18 | 9 | 2 | 5 | 62 | 7 | 3 |
| 7:30 AM - 7:45 AM | 49 | 10 | 5 | 3 | 13 | 17 | 64 | 2 | 23 | 26 | 22 | 3 | 7 | 65 | 8 | 3 |
| 7:45 AM - 8:00 AM | 70 | 19 | 4 | 3 | 6 | 25 | 79 | 2 | 47 | 63 | 24 | 6 | 6 | 64 | 6 | 1 |
| 8:00 AM - 8:15 AM | 26 | 10 | 4 | 0 | 8 | 16 | 24 | 2 | 26 | 23 | 11 | 3 | 5 | 43 | 8 | 3 |
| 8:15 AM - 8:30 AM | 20 | 11 | 8 | 0 | 3 | 4 | 27 | 2 | 18 | 23 | 10 | 4 | 1 | 26 | 3 | 2 |
| 8:30 AM - 8:45 AM | 26 | 7 | 6 | 1 | 4 | 8 | 43 | 2 | 23 | 24 | 13 | 3 | 6 | 40 | 0 | 2 |
| 8:45 AM - 9:00 AM | 42 | 5 | 5 | 2 | 4 | 5 | 45 | 1 | 20 | 28 | 22 | 4 | 7 | 53 | 1 | 1 |
| TOTAL | 302 | 86 | 42 | 10 | 51 | 92 | 433 | 13 | 185 | 220 | 123 | 26 | 41 | 394 | 34 | 18 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 4:00 PM - 4:15 PM | 16 | 10 | 2 | 0 | 6 | 8 | 22 | 1 | 41 | 47 | 16 | 0 | 7 | 45 | 6 | 3 |
| 4:15 PM - 4:30 PM | 16 | 12 | 5 | 0 | 2 | 9 | 17 | 0 | 47 | 47 | 17 | 1 | 6 | 37 | 5 | 2 |
| 4:30 PM - 4:45 PM | 18 | 9 | 4 | 0 | 4 | 6 | 18 | 1 | 37 | 42 | 30 | 3 | 2 | 27 | 2 | 1 |
| 4:45 PM - 5:00 PM | 20 | 10 | 5 | 1 | 4 | 6 | 29 | 1 | 64 | 60 | 28 | 6 | 3 | 39 | 2 | 1 |
| 5:00 PM - 5:15 PM | 22 | 12 | 4 | 3 | 4 | 16 | 25 | 0 | 63 | 54 | 29 | 1 | 3 | 26 | 5 | 2 |
| 5:15 PM - 5:30 PM | 20 | 18 | 4 | 1 | 3 | 9 | 33 | 0 | 51 | 43 | 28 | 3 | 8 | 35 | 5 | 1 |
| 5:30 PM - 5:45 PM | 18 | 17 | 6 | 0 | 5 | 11 | 31 | 2 | 29 | 42 | 26 | 1 | 4 | 40 | 4 | 2 |
| 5:45 PM - 6:00 PM | 16 | 13 | 4 | 1 | 8 | 12 | 19 | 0 | 44 | 54 | 10 | 2 | 8 | 31 | 5 | 0 |
| TOTAL | 146 | 101 | 34 | 6 | 36 | 77 | 194 | 5 | 376 | 389 | 184 | 17 | 41 | 280 | 34 | 12 |


|  | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEAK HOUR | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks | Left | Thru | Right | Trucks |
| 7:00 AM - 8:00 AM | 188 | 53 | 19 | 7 | 32 | 59 | 294 | 6 | 98 | 122 | 67 | 12 | 22 | 232 | 22 | 10 |
| 4:45 PM - 5:45 PM | 80 | 57 | 19 | 5 | 16 | 42 | 118 | 3 | 207 | 199 | 111 | 11 | 18 | 140 | 16 | 6 |




[^0]:    Note: The State Clearinghouse will assign identification numbers for all new projects. If a SCH number already exists for a project (e.g. Notice of Preparation or previous draft document) please fill in.

[^1]:    ${ }^{1}$ SJVAPCD GAMAQI, Section 8.3.4, Page 85.

[^2]:    Enclosures: Figures 1-4

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[^4]:    ${ }^{1}$ Mitigation shown in Table 8

